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SUBJECT: Milton – Route 28 Corridor Road Diet Feasibility Study from Chickatawbut Road to Reedsdale Road

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HSH PROJECT NO.: 2021055.15

Executive Summary

This memorandum is part of the Massachusetts Department of Transportation's (MassDOT's) ongoing efforts to evaluate alternatives for potential corridor safety and operational improvements along Route 28 just north of Chickatawbut Road to Reedsdale Road. These potential improvements were investigated in response to concerns raised by the public and the Town of Milton.

A road diet was evaluated on Route 28, reducing either northbound or southbound traffic to one lane except at intersections requiring left-turn lanes. The cross-sectional width gained from the road diet may support multiple new transportation uses (such as shared-use path or a center-running left-turn lane with raised medians); however, this study focuses solely on the feasibility of the road diet. The road diet alternatives for Route 28 included:

- Alternative 1 – Northbound Road Diet: narrowing the roadway to one lane northbound and maintaining two southbound travel lanes. The northbound road diet would start approximately 1,350 feet north of the Chickatawbut Road roundabout and end south of Reedsdale Road.
- Alternative 2 – Northbound Road Diet, Version 2: narrowing the roadway to one lane northbound and maintaining two southbound travel lanes. The northbound road diet would start at the Chickatawbut Road roundabout and end south of Reedsdale Road.
- Alternative 3 – Southbound Road Diet: narrowing the roadway to one lane southbound and maintaining two northbound travel lanes. The southbound road diet would start at the Reedsdale Road intersection and end north of the Chickatawbut Road roundabout.



The following study results conclude why a road diet along this Route 28 segment is not feasible in either direction:

- Travel time along the corridor from the Scanlon Drive/Russ Street intersection to Reedsdale Road:
 - Overall corridor travel time improved in the a.m. peak hour but worsened in the p.m. peak hour, except for Alternative 1.
 - Even though the a.m. peak hour saw overall improvement in travel times, the actual improvement was noticeable in only half the corridor, depending on the road diet alternative.
 - Alternative 2 – the corridor experienced congestion in the northbound direction at the roundabout, due to removing one through lane from the roundabout. The remaining portion of the corridor saw the travel time improvement due to reduced traffic and increased speeds.
- Vehicle-hours of Delay along the corridor:
 - Alternative 1 shows an increase in vehicle-hours of delay in both the a.m. and p.m. peak hours, north of Hillside Street.
 - Alternative 2 experiences an increase in vehicle-hours of delay in the a.m. peak hour, south of Chickatawbut Road, and in the p.m. peak hour, north of Hillside Street.
 - Alternative 3 experiences an increase in vehicle-hours of delay in the a.m. peak hour, north of Hillside Street, and in the p.m. peak hour, south of Chickatawbut Road.
- Bus Travel Time:
 - This metric shows that bus travel times experience an increase under Alternative 2 and Alternative 3.
- Corridor Vehicle Speeds:
 - A goal of the road diet is to reduce the speeds along Route 28 to increase safety along the corridor. However, while the portions of the corridor that saw congestion saw a reduction in speeds, the portions that saw less traffic due to the upstream congestion resulted in speed increases.
- Driveway Delay:
 - This metric focused on the driveways and side streets nearest the proposed Chickatawbut Road intersection roundabout. The results determined that the existing conditions see less delay at the driveways than the road diet alternatives during the a.m. peak, except for Alternative 3. During the p.m. peak hour, some



driveways are expected to see less delay under Alternatives 1 and 3, and others are expected to see more delay under all alternatives.

■ Queues:

- Each of the road diet alternatives saw increased queues along the Route 28 corridor, with queues extending well over a mile.
- The most notable impact of queueing was noted at Chickatawbut Road. The two northbound road diet alternatives presented queues like or worse than existing conditions, thus maintaining or worsening the impacts at the I-93 interchange.

A supplemental memorandum focused on driveway delay is provided in **Appendix A**. This memorandum compared the existing conditions against:

- Future No-build (increase in volumes only);
- Future No-build with Roundabout (at Route 28 and Chickatawbut Road);
- Future No-build with Roundabout and Metering (at Route 28 and Chickatawbut Road and metering signals on northbound and southbound approaches to the roundabout);
- Road Diet Alternative 1;
- Road Diet Alternative 2;
- Road Diet Alternative 3; and
- The Route 28 at Chickatawbut Road roundabout without a road diet.

The data presented in that memorandum showed an average delay increase for the side streets and driveways under Alternatives 1 and 2 for all peak hours when compared to No-build conditions, and an average delay decrease under Alternative 3.

Two Road Safety Audits (RSAs) were conducted along Route 28:

- Milton: Reedsdale Road to north of Chickatawbut Road; and
- Quincy/Randolph: south of Chickatawbut Road to north of Scanlon Drive/Russ Street.

The RSAs identified issues like speeding, poor sight distances at unsignalized intersections, and signal timing problems. Proposed countermeasures include short-term fixes (e.g., signal adjustments) and long-term solutions (e.g., medians to restrict left turns). Potential short- and long-term improvements are to be further evaluated and designed separate from the Route 28 at Chickatawbut Road intersection improvement project. The RSA reports are available on MassDOT's RSAs website.



Metering of the Route 28 traffic at the proposed Chickatawbut Road roundabout was also evaluated in a memorandum dated May 2023, which is provided in **Appendix C**. The metering included using specially timed signals to create gaps for driveways and side streets. The analysis presented focused only on the proposed roundabout. The May 2023 memorandum analysis showed some improvement on Chickatawbut Road but lacked insight into the metering's impact on driveways north of the roundabout, prompting further analysis that is presented in this memorandum. The analysis presented in this memorandum indicates that the No-build with Roundabout and Metering scenario results in slightly worse driveway delays than the Future No-build with Roundabout and Alternative 3 scenarios but performs better than all other scenarios.

This memorandum concludes that:

- A road diet is not feasible in either direction, as at least one peak hour would experience heavy congestion on Route 28, leading to traffic diverting to local roads; and
- The Future No-build with Roundabout scenario results in slightly less driveway delay than the Future No-build with Roundabout and Metering scenario. Though the difference is minimal, abutters are concerned about any increase, making the Future No-build with Roundabout, the current MassDOT design, the preferred option.

Therefore, the recommended scenario is no road diet, a roundabout, and Pedestrian Hybrid Beacons (PHBs).



Introduction

The purpose of this memorandum is to present the feasibility of a road diet along the Route 28 Corridor, from Chickatawbut Road to Reedsdale Road in Milton, Massachusetts. The Massachusetts Department of Transportation (MassDOT) tasked **Howard Stein Hudson (HSH)** with this study, as part of the Route 28 at Chickatawbut Road Intersection Improvements Project (PInfo #607342). The need for this study resulted from several comments and concerns made by residents living near the Route 28 at Chickatawbut Road intersection and along Route 28, who believe that the proposed roundabout at the Route 28 and Chickatawbut Road intersection will make it more difficult for them to exit their driveway and enter Route 28. The study limits extend along Route 28 from the intersection of Route 28 and Reedsdale Road to the intersection of Route 28 and Scanlon Drive/Russ Street.

The memorandum will briefly describe the alternatives that were studied, the necessary improvements at certain intersections that will allow the implementation of the road diet, and the results of the study. The results presented in the memorandum will focus on performance metrics such as:

- Travel time along the corridor;
- Vehicle-hours of delay experienced by those driving through the corridor;
- Average vehicular speed and how it changes between alternatives;
- Demand rate or unmet demand at specific points along the corridor;
- Driveway delay; and
- Queues on the Route 28 mainline at specific locations.

The appendices provided include additional traffic information such as the network volumes used in the analysis, VISSIM calibration notes, tabulated data, and capacity analysis results.

Feasibility Study

Alternatives Description

This section will provide a brief description of each alternative studied under this effort. This memorandum and analysis focus on the impact of changing the number of travel lanes along the corridor. The alternatives which reduce the number of lanes on Route 28 would allow for roadway space to be reallocated to separate bicycle accommodations. However, the alternatives include



providing an exclusive left-turn lane at select intersections, and those locations would require further investigation for bicycle connectivity through them.

EXISTING AND FUTURE NO-BUILD CONDITIONS

Under the existing conditions, Route 28 and its intersections remain as they are today, without any changes to signals, number of lanes, etc. This means that the existing signal at the Route 28 and Chickatawbut Road intersection is still in place. Under the future No-build conditions, the only thing that changes are the corridor volumes, which are increased by a 10-year horizon (2023 to 2033).

NO-BUILD WITH ROUNDABOUT

This alternative analyzes the Route 28 corridor with the proposed roundabout at the Route 28 and Chickatawbut Road intersection. The roundabout will be modeled as depicted currently in the latest design plans under MassDOT Project #607342, including the Pedestrian Hybrid Beacons (PHBs) on the Route 28 legs of the roundabout.

NO-BUILD WITH ROUNDABOUT AND METERING

This alternative evaluates the Route 28 corridor with a proposed roundabout at Route 28 and Chickatawbut Road. Instead of PHBs on Route 28, 20-second metering signals will be used to create longer gaps for Chickatawbut Road and nearby driveways to enter. The 20 second duration was selected after testing 10-, 15-, and 20-second intervals to ensure safe gaps and smooth roundabout flow.

ALTERNATIVE 1 – NORTHBOUND ROAD DIET

Alternative 1 studied the feasibility of a northbound road diet, which would reduce the northbound direction to one travel lane and maintain two southbound travel lanes. The lane reduction on Route 28 northbound is proposed 880 feet north of the proposed roundabout at Route 28 and Chickatawbut Road to better accommodate the anticipated queue on Route 28 northbound at the merge point without creating gridlock through the roundabout. Specific intersection improvements needed to allow the implementation of this alternative would include:

- Route 28 at Reedsdale Road:
 - Intersection lane use remains unchanged, except for the westbound approach which is proposed to provide one exclusive left-turn lane and a shared through/right-turn lane;
 - Provide markings and signs to better inform intended lane use throughout the intersection;
 - Narrow the south leg of the intersection (Route 28 northbound) to three 11-foot-wide travel lanes;



- Modify signal equipment to provide a Flashing Yellow Left Arrow (FYLA) for Reedsdale Road westbound; and
- Modify timings and coordinate signal with the signal at Reed Street/Access Road.
- Route 28 at Reed Street/Access Road:
 - Open Route 28 northbound to two lanes and mark the inside northbound lane as an exclusive left-turn lane. Remaining intersection lane assignments remain unchanged; and
 - Provide protected left-turn phasing and coordinate with signals at Reedsdale Road and Hillside Street.
- Route 28 at Hallen Avenue:
 - Open Route 28 northbound to two lanes and mark the inside northbound lane as an exclusive left-turn lane. Remaining intersection lane assignments remain unchanged
- Route 28 at Hillside Street:
 - Open Route 28 northbound to two lanes and mark the inside northbound lane as an exclusive left-turn lane. Allow U-turns from this lane to assist residents residing on the northbound side of Route 28 to change direction from northbound to southbound and avoid turning left from their driveways (current concern). Remaining intersection lane assignments remain unchanged; and
 - Provide protected left-turn phase and coordinate with Reed Street/Access Road signal.
- Route 28 Northbound through I-93 Interchange:
 - Provide markings between inner loop ramps to delineate an auxiliary lane for weaving vehicles;
 - Provide markings and signs for a Yield Condition for the I-93 Southbound Off-Ramp; and
 - Improve the merge area to the north of the I-93 Southbound Off-Ramp by better delineating the two Route 28 northbound travel lanes and the start of the merge area (signs and markings).

Figure 1 presents the corridor proposed conditions graphically.

ALTERNATIVE 2 – NORTHBOUND ROAD DIET V2

The second alternative still looks into the northbound road diet, however, rather than merging the two northbound lanes north of Chickatawbut Road, this alternative proposes that the Route 28 northbound approach at Chickatawbut Road be revised to one left-turn/thru lane and one right-turn-



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only lane so that only a single northbound lane departs the roundabout. All other improvements mentioned under Alternative 1 would be the same. **Figure 2** presents the proposed conditions graphically.



Figure 1. *Route 28 Corridor Northbound Road Diet – Alternative 1*

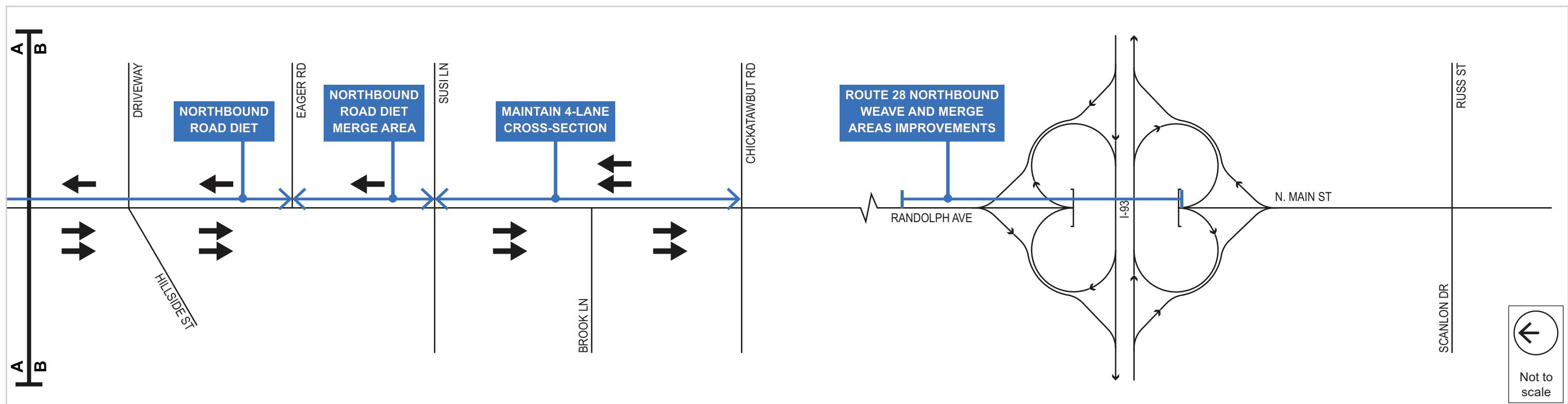
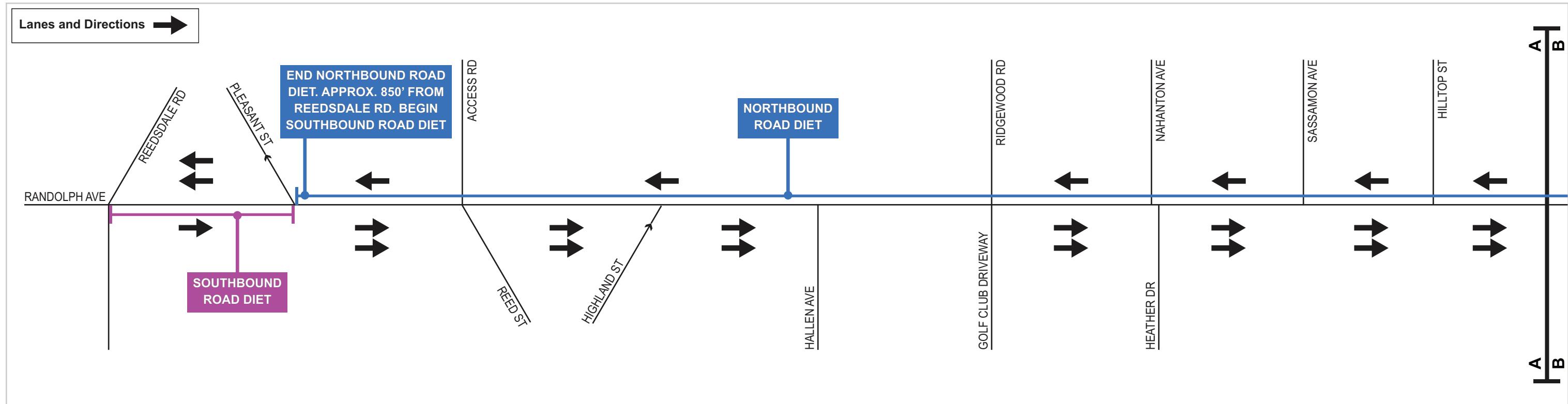
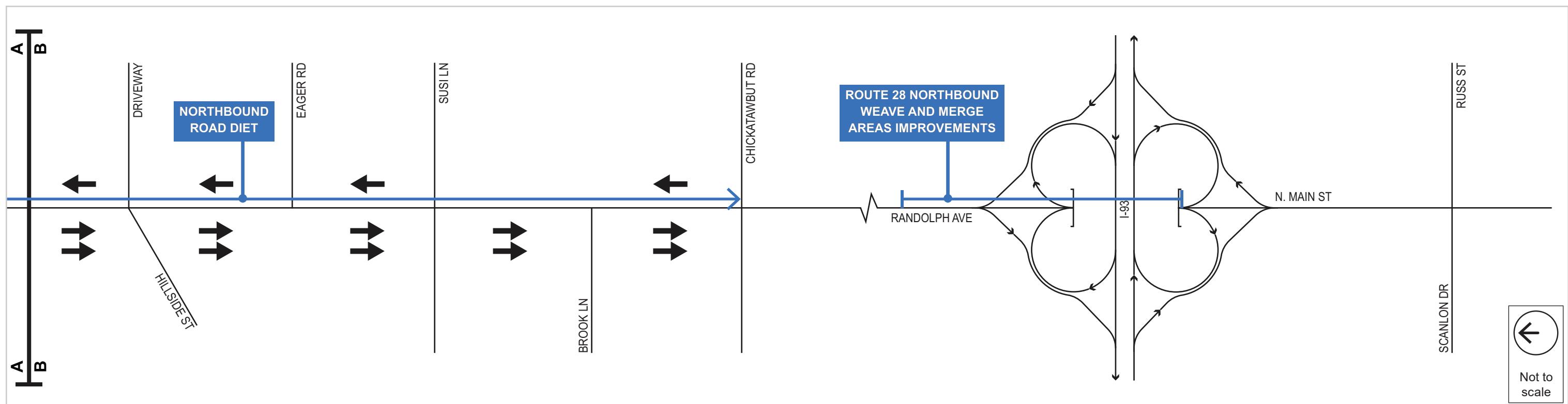
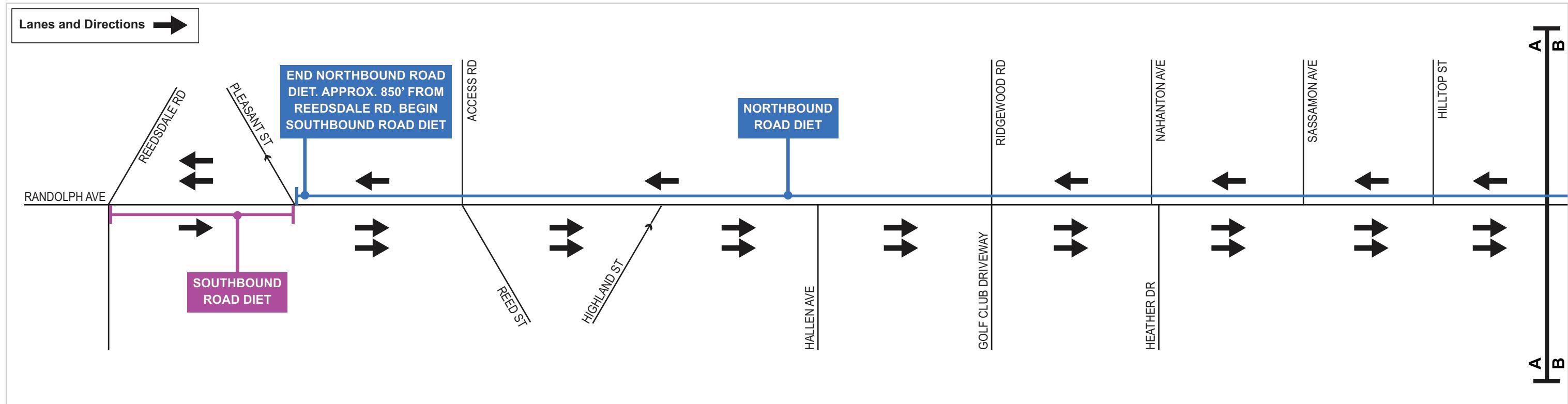




Figure 2. *Route 28 Corridor Northbound Road Diet – Alternative 2*





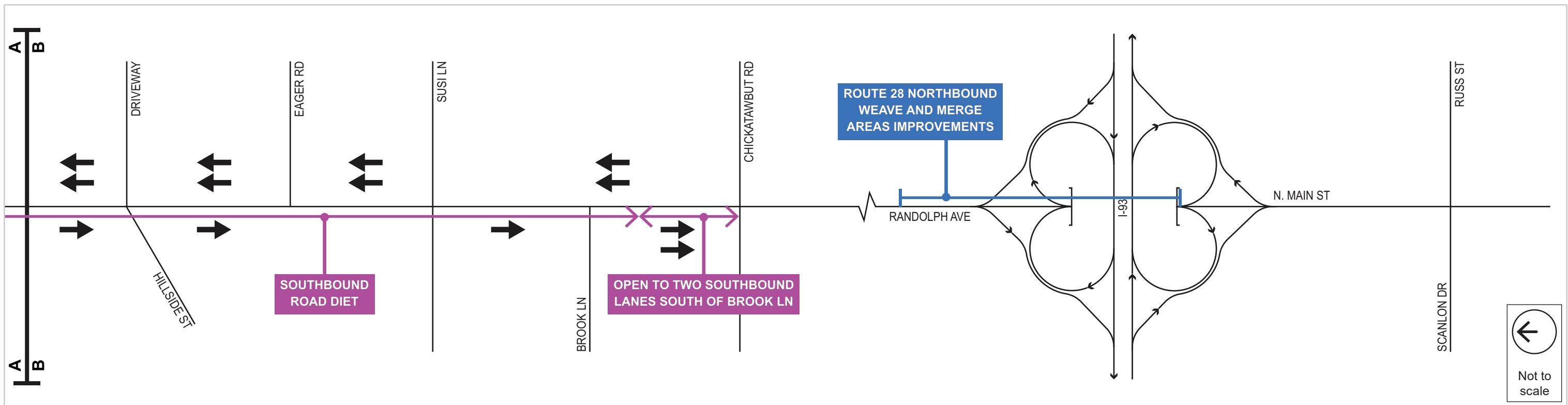
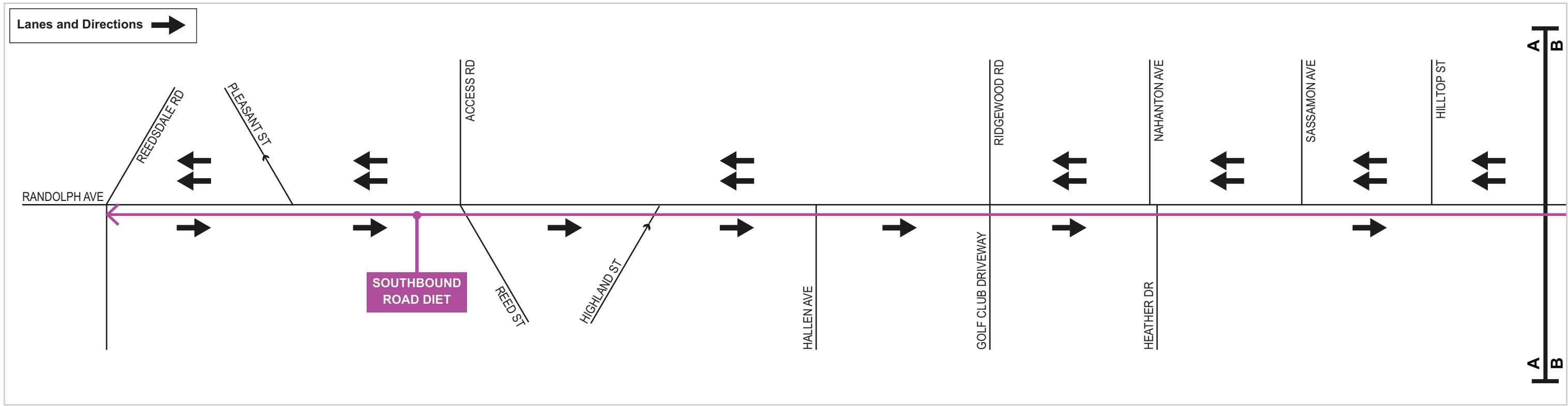
ALTERNATIVE 3 – SOUTHBOUND ROAD DIET

The southbound diet would start immediately to the south of the Route 28 and Reedsdale Road intersection, by providing only one southbound receiving lane that will continue all the way to Chickatawbut Road, where it would open to two lanes at approximately 250 feet to the north of the roundabout. The northbound direction would maintain the two travel lanes throughout the study corridor.

The lane use modifications, as well as the signal modifications, at the Route 28 at Reedsdale Road and Reed Street/Access Road intersections would be similar to the other alternatives. However, this alternative would not provide a U-turn at the Hillside Street intersection for residents on the northbound side of Route 28 to change direction. The Route 28 northbound area through the I-93 Interchange modifications would also be similar to the other alternatives. **Figure 3** presents the proposed improvements graphically.



Figure 3. *Route 28 Corridor Southbound Road Diet – Alternative 3*





Performance Metrics

This section will describe the metrics that data was collected for and compared against No-build conditions, as well as between the alternatives.

Existing (2023) and Future (2033) Conditions volumes and Vissim model calibration notes, as well as roundabout capacity calibration in Vissim notes, can be found in **Appendix B**.

TRAVEL TIME AND VEHICLE-HOURS OF DELAY

This metric measures the total amount of time that Route 28 vehicles are delayed due to congestion along the length of the study corridor. HSH conducted field travel time runs within specific corridor segments at the same time the traffic counts were being collected (September 2023), to calibrate the Vissim models and compare the Alternatives' simulated travel times against. The travel time segments selected were:

- South of Route 28 at Reedsdale Road to north of Route 28 at Chickatawbut Road;
- North of Route 28 at Chickatawbut Road to north of Route 28 at Scanlon Drive/Russ Street; and
- South of Route 28 at Reedsdale Road to north of Route 28 at Scanlon Drive/Russ Street.

The vehicle-hours of delay were calculated as follows:

- ***Existing Conditions:*** Vehicle-hours traveled were determined by multiplying the number of vehicles passing through specific points in the VISSIM model by their travel time between these points.
- ***No-build and Alternatives:*** Using the same method, vehicle-hours traveled were calculated for No-build and alternative scenarios. The difference between No-build and existing vehicle-hours traveled determined the delay under No-build conditions.
- ***Comparing Alternatives:*** The difference between vehicle-hours traveled for each alternative and the No-build scenario indicated the change in vehicle-hours of delay for each alternative.

Figure 4 and **Figure 5** present the travel time (in minutes) and vehicle-hours of delay results of the Vissim modeling for the Existing conditions. The No-build conditions and the three alternatives travel time and vehicle-hours of delay are presented in **Figure 6** through **Figure 9**. Tabulated data for these results can be found in **Appendix B**.



Figure 4. *Travel Time – Existing (2023) Conditions*

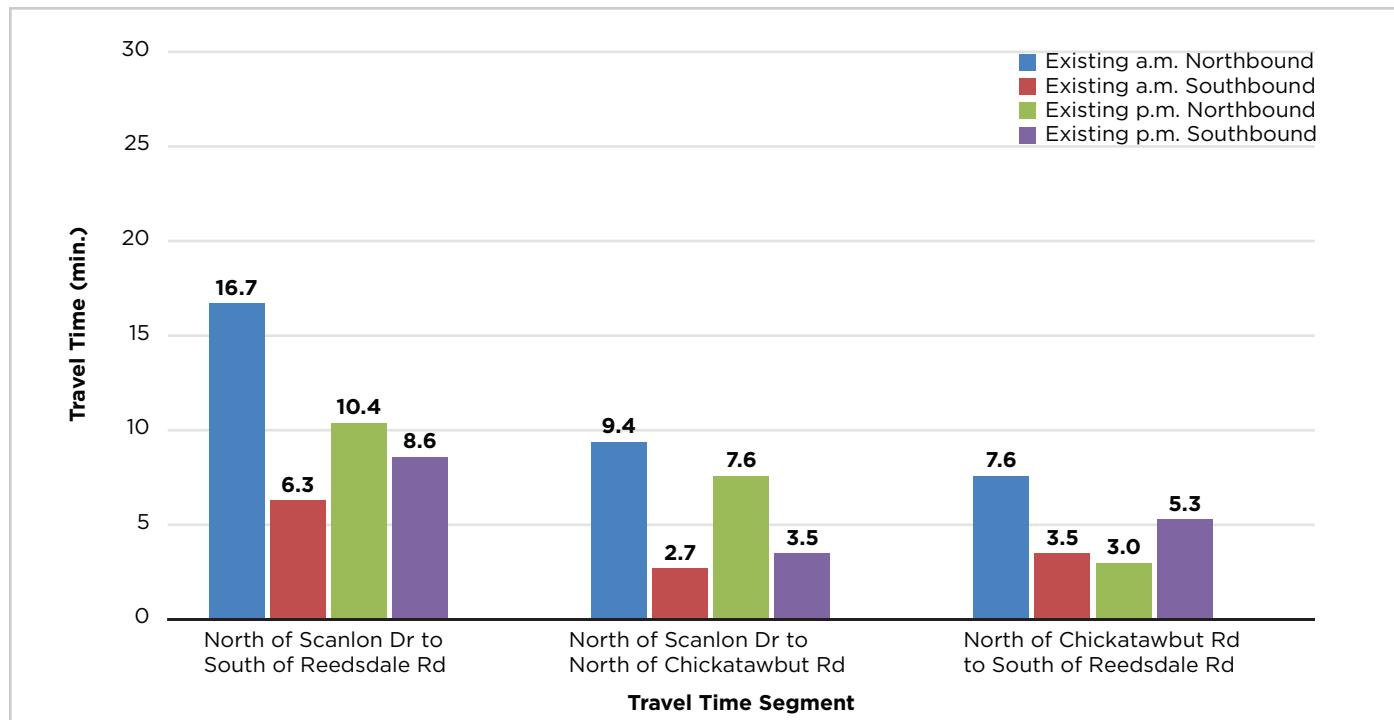


Figure 5. *Vehicle Hours of Delay – Existing (2023) Conditions*

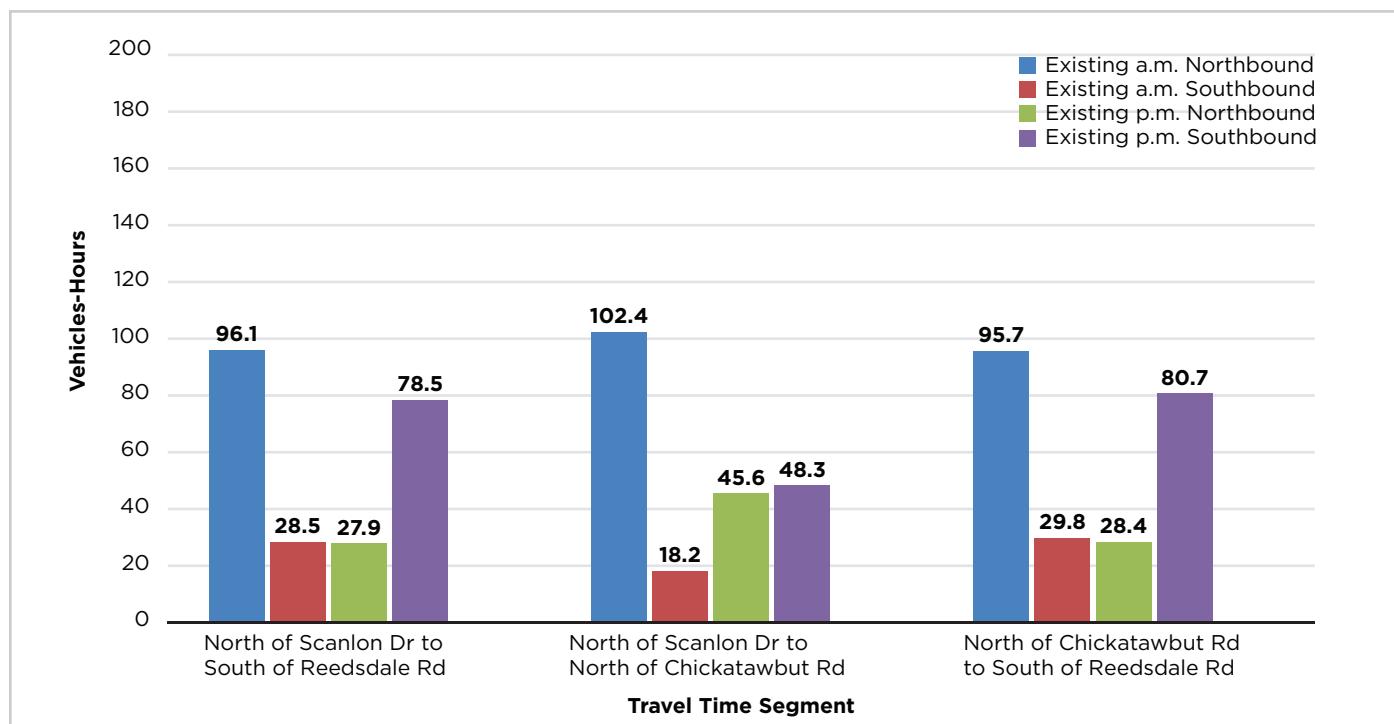




Figure 6. a.m. Peak Travel Time Comparison of Future Alternatives

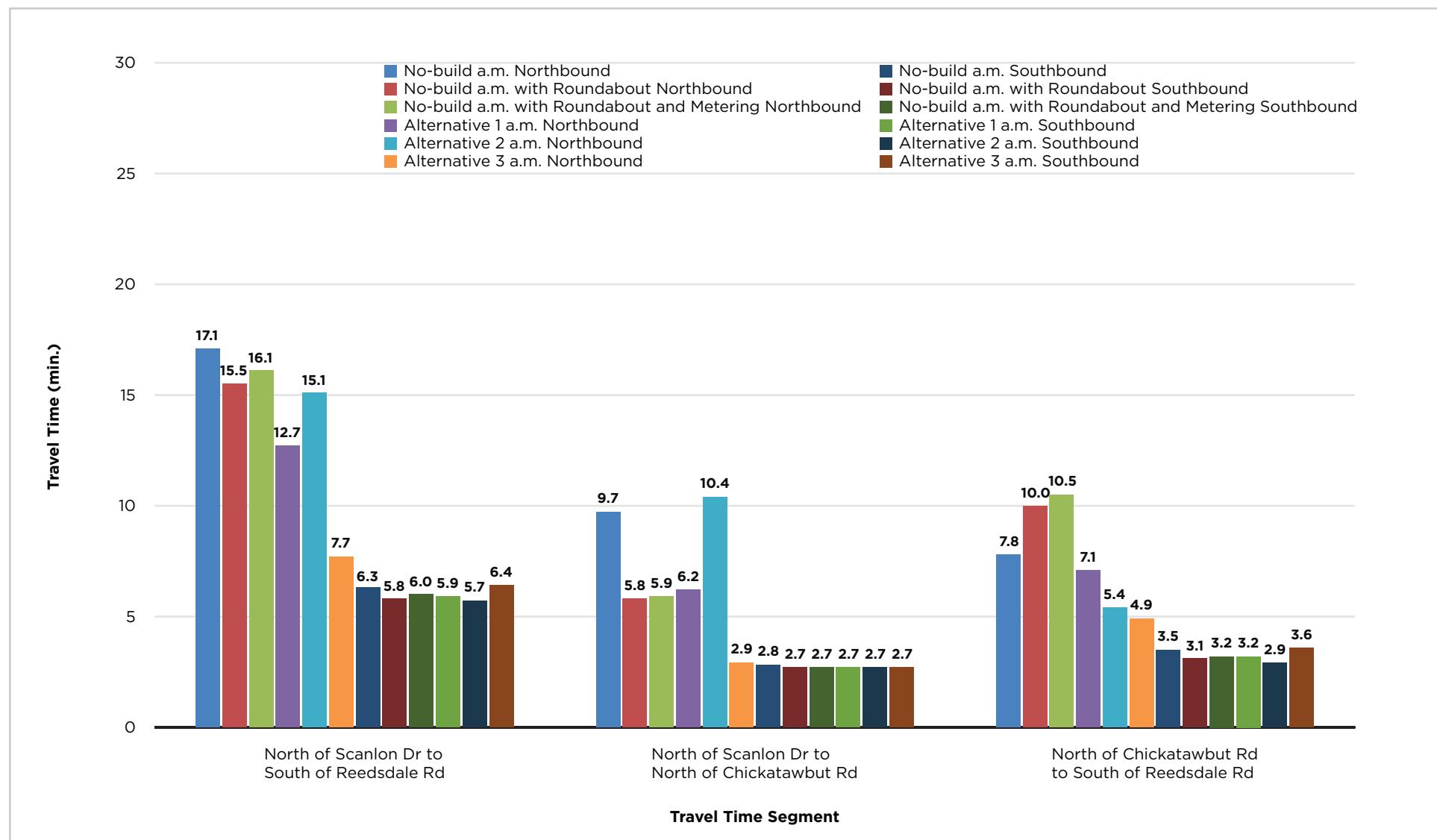




Figure 7. *p.m. Peak Travel Time Comparison of Future Alternatives*

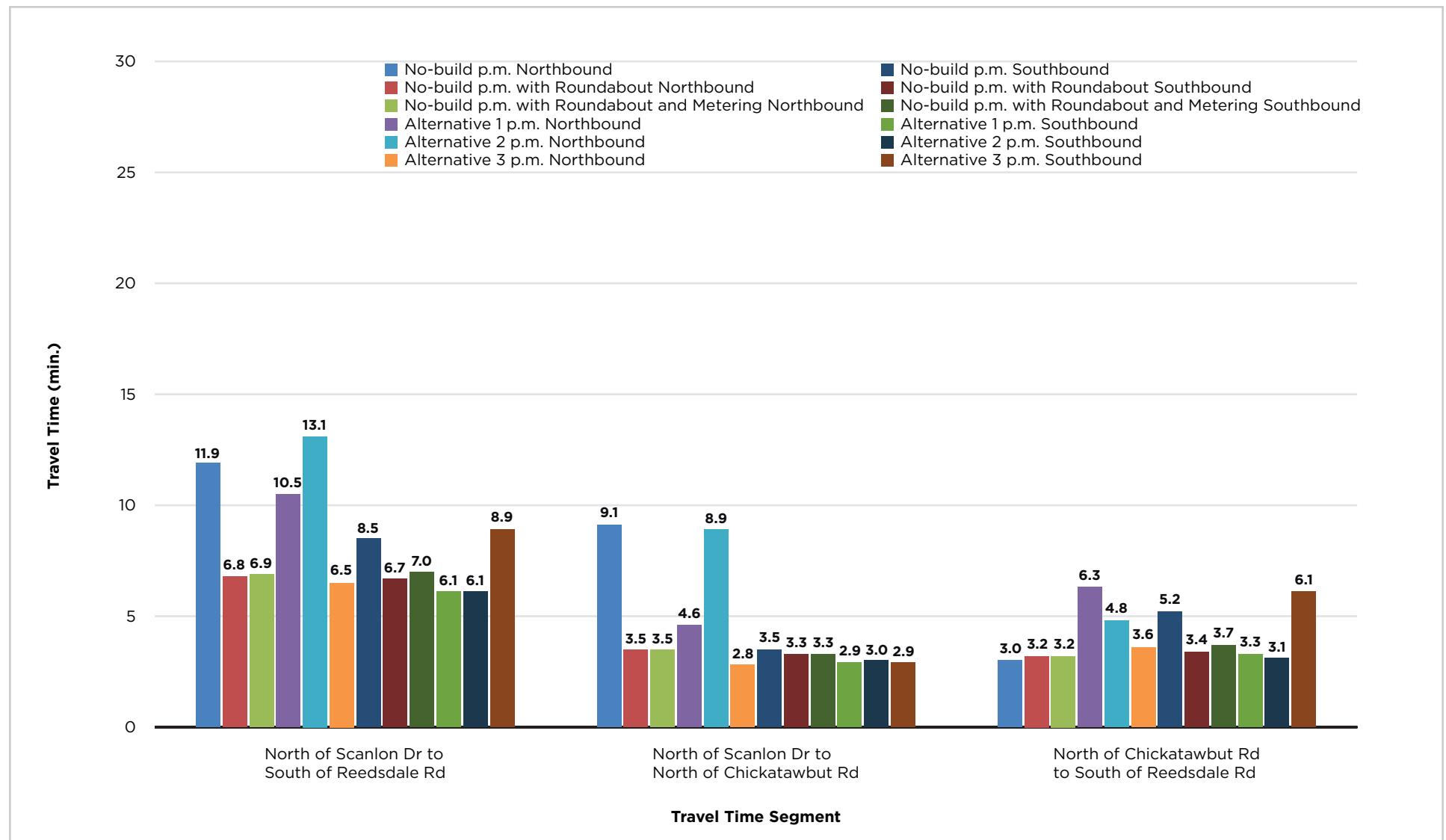




Figure 8. a.m. Peak Vehicle-hours of Delay Comparison of Future Alternatives

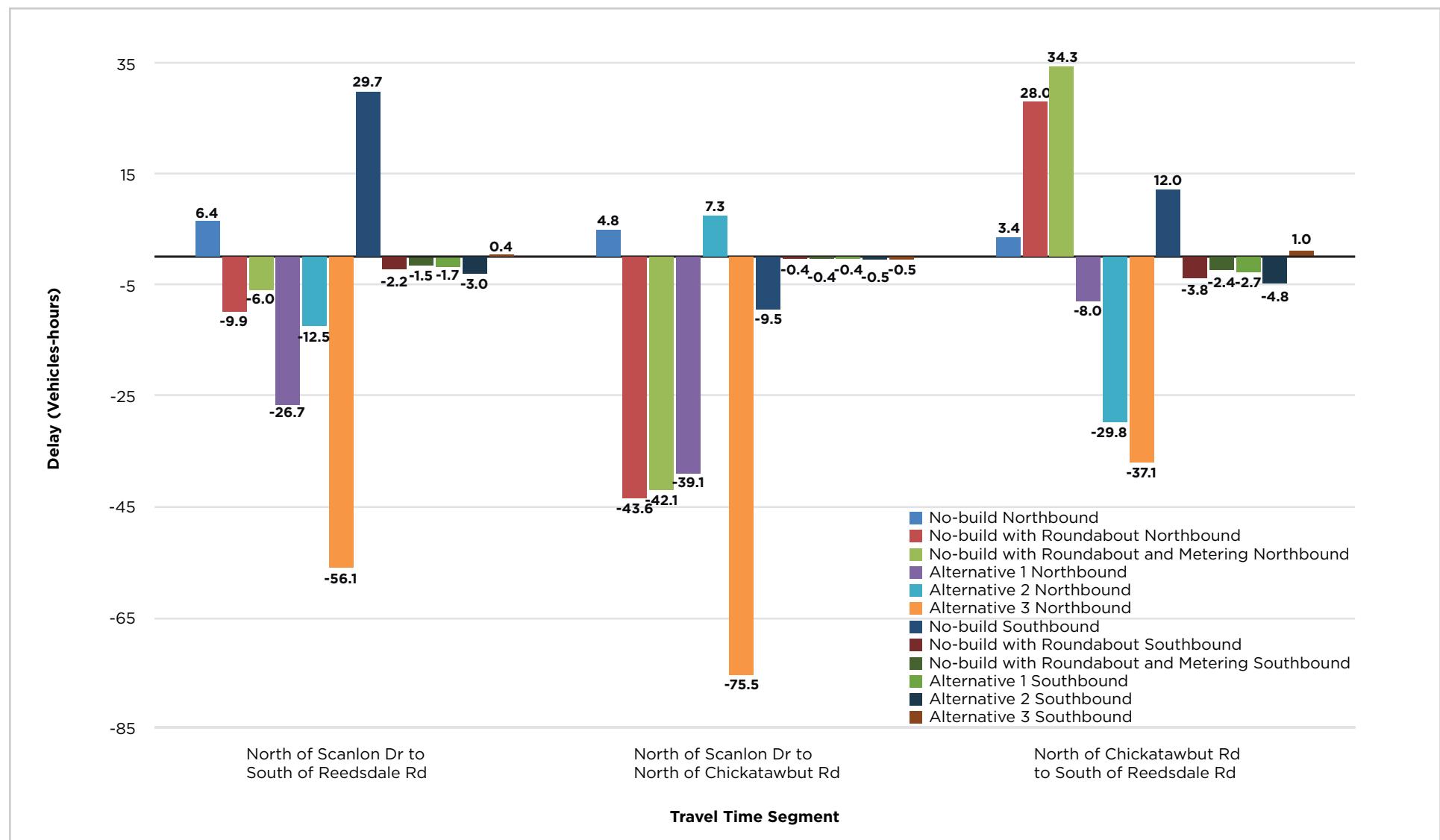
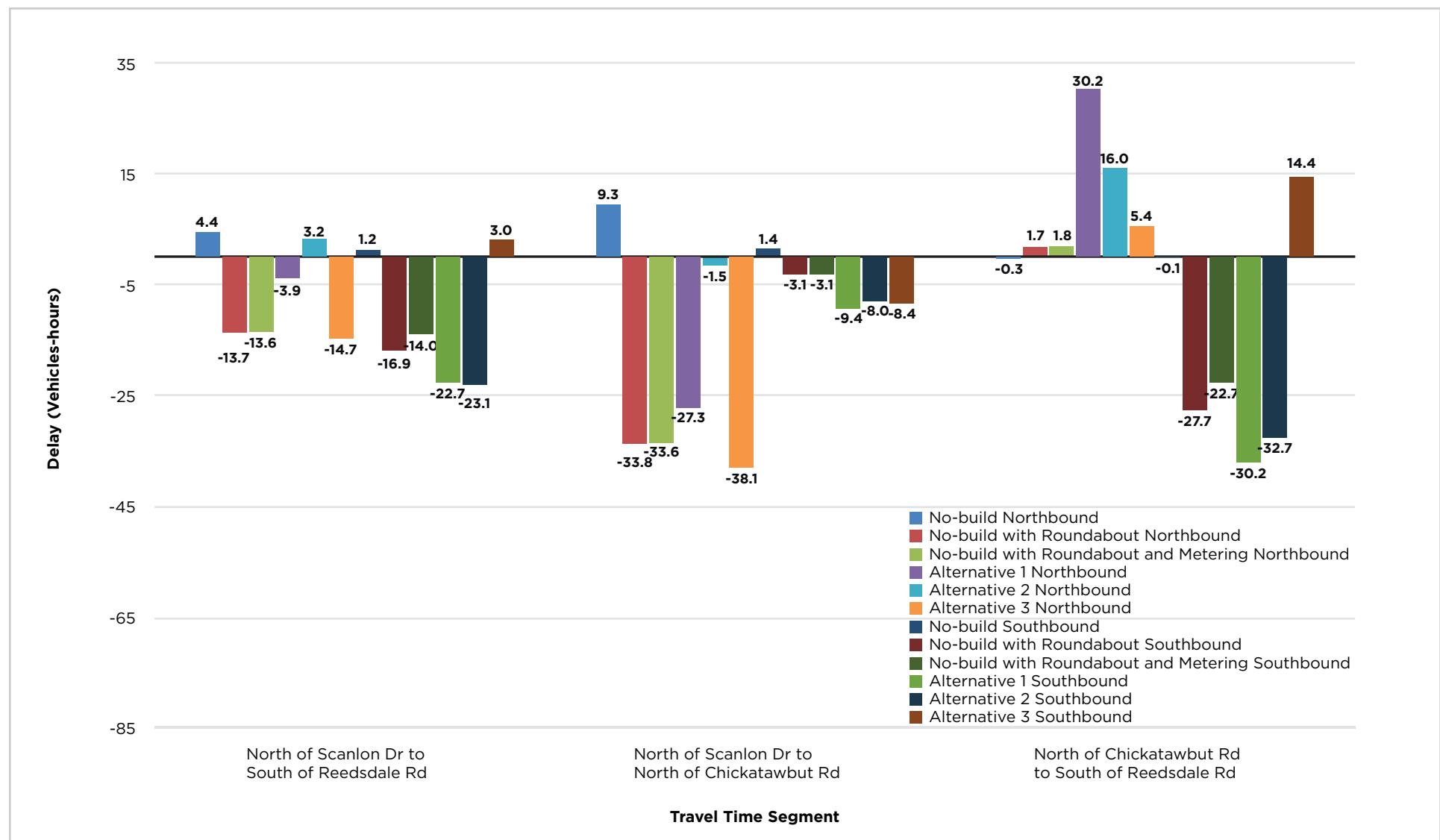




Figure 9. *p.m. Peak Vehicle-hours of Delay Comparison of Future Alternatives*





As can be seen from the charts that compare the future No-build conditions against the northbound and southbound road diet alternatives, when considering the entire corridor travel times and vehicle-hours of delay, Alternative 3 in the northbound direction and Alternative 2 in the southbound direction are expected to see improved travel times and less vehicle-hours of delay during both the a.m. and p.m. peak hours.

When looking at the segment between north of the Scanlon Drive/Russ Street intersection and north of the Chickatawbut Road intersection, and during the a.m. peak hour, Alternative 3 is expected to see improved travel times and less vehicle-hours of delay in both the northbound and southbound directions. During the p.m. peak hour, Alternative 3 in the northbound direction and Alternative 1 in the southbound direction are expected to see improved travel times and less vehicle-hours of delay.

The bus travel times were also collected, as there are buses using Route 28 through the study area; the Massachusetts Bay Transportation Authority (MBTA) bus route #240 and the Brockton Area Transit (BAT), which is a flag-down bus service. Today, these buses stop at the curb to board and alight riders at nine different stops on each side of the study corridor. Under the alternatives, these bus stops are proposed to be pull-out areas, so the stopped buses do not block the large volumes traveling up and down Route 28 within the study area. **Figure 10** shows the existing bus travel times, whereas **Figure 11** and **Figure 12** present the a.m. and p.m. peak hour travel times, respectively, for the No-build conditions and the alternatives.



Figure 10. *Existing (2023) Condition Bus Travel Times - Route 28*

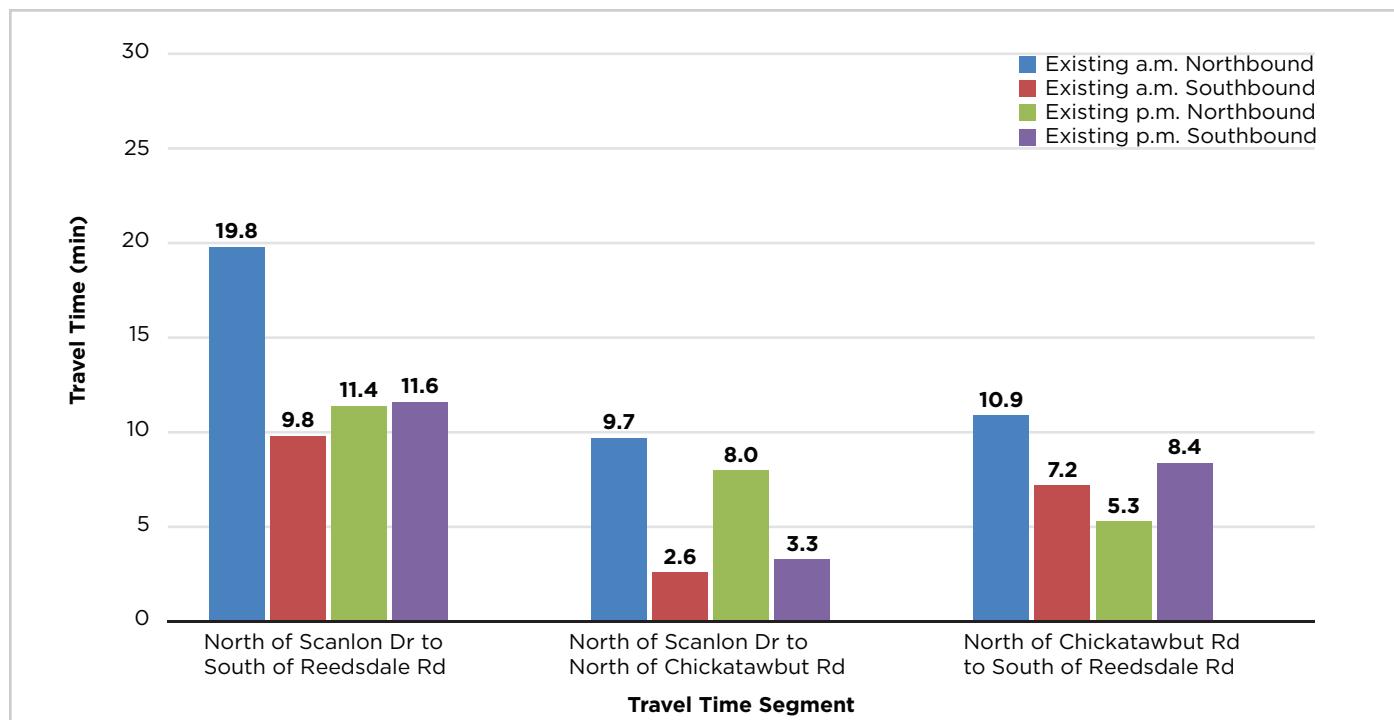




Figure 11. *Comparison of Future Alternatives - a.m. Peak Hour Bus Travel Times*

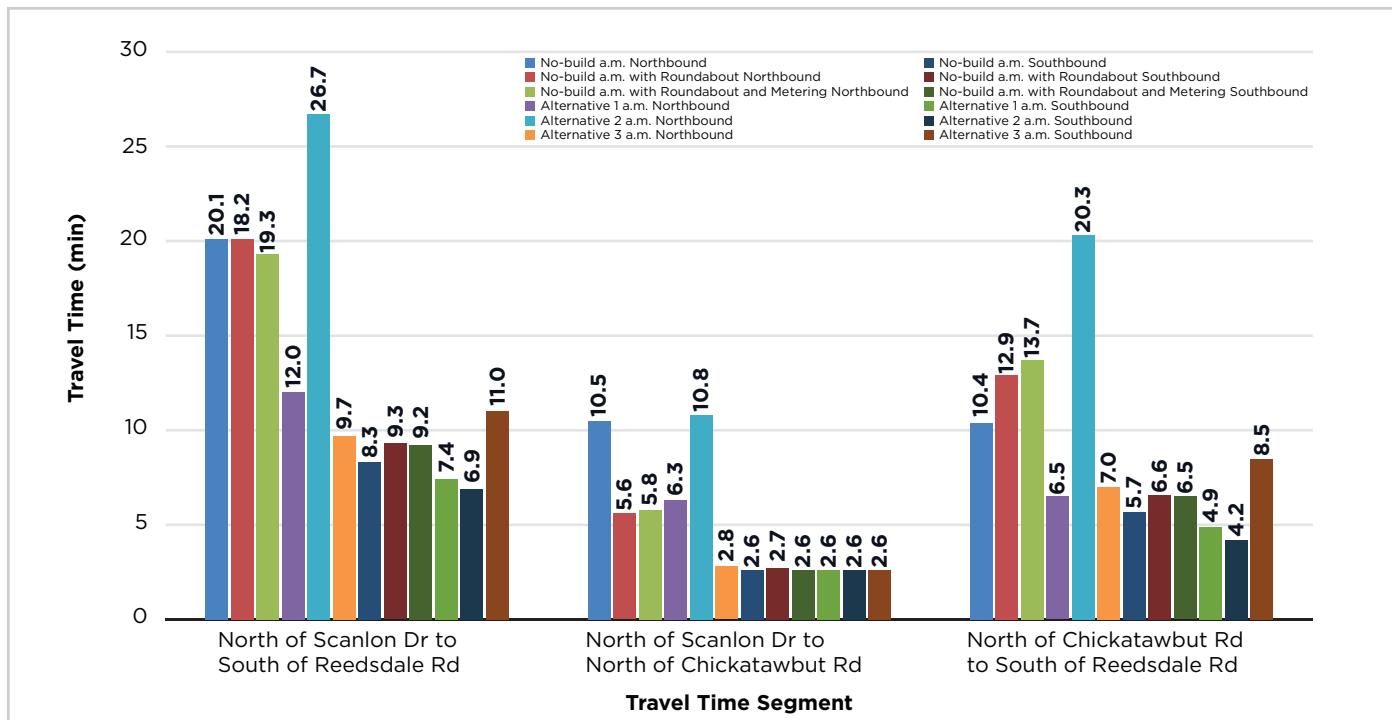
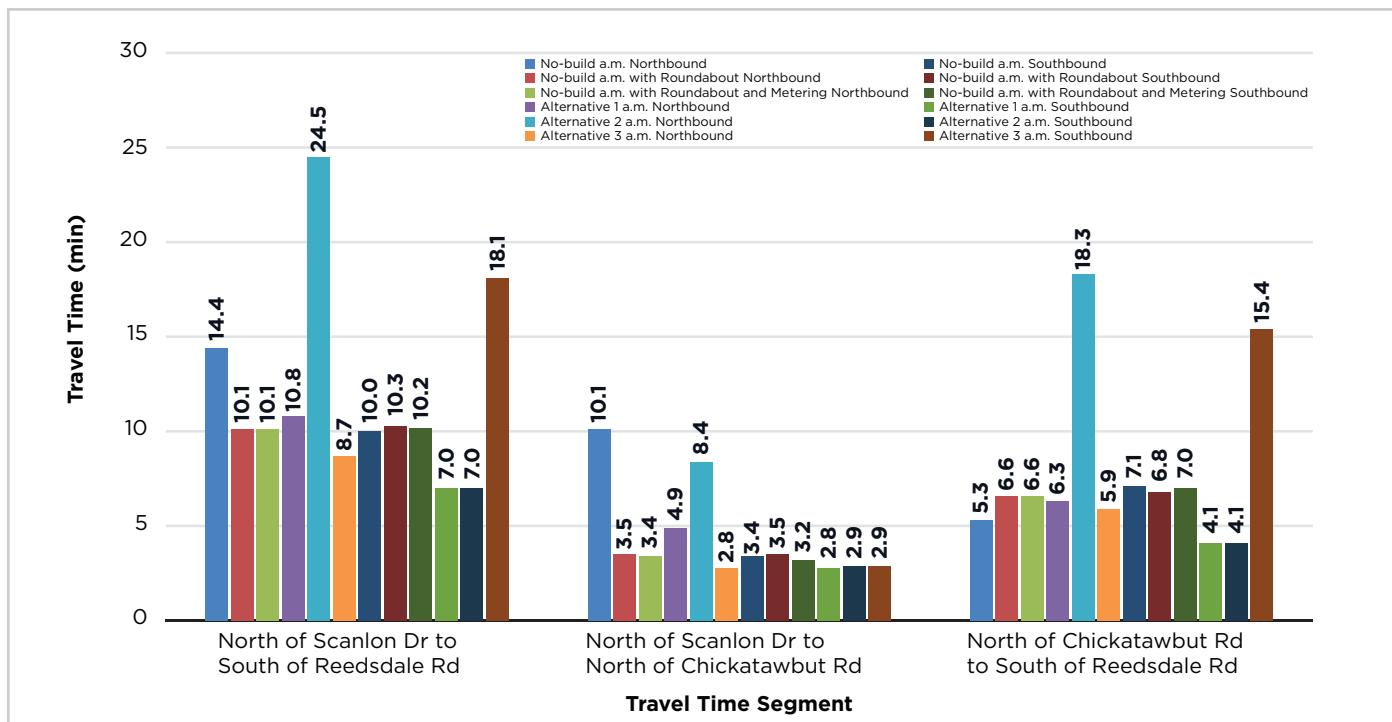


Figure 12. *Comparison of Future Alternatives - p.m. Peak Hour Bus Travel Times*





As can be seen from **Figure 10** through **Figure 12**, and when comparing the alternatives against the No-build travel times, Alternative 2 is expected to increase bus travel times in the northbound direction for both the a.m. and p.m. peak hours, and Alternative 3 is expected to increase bus travel times in the southbound direction for both the a.m. and p.m. peak hours.

AVERAGE VEHICLE SPEEDS

Vehicle speeds along the Route 28 corridor were measured at five different locations in all the models:

- South of Reedsdale Road;
- South of Reed Street/Access Road;
- South of Hillside Street;
- South of Chickatawbut Road; and
- Between the I-93 inner loop ramps.

The changes in average speeds at different locations will point out where there is congestion or free-flow traffic along the corridor depending on the alternative. **Figure 13** and **Figure 14** present the Existing conditions average vehicle speeds for the northbound and southbound directions respectively during the weekday a.m. and p.m. peak hours. **Figure 15** and **Figure 16** provide a comparison between the No-build conditions and the alternatives' average vehicle speeds for the northbound and southbound directions respectively.

Tabulated data for the average vehicle speeds can be found in **Appendix B**.



Figure 13. *Route 28 Northbound Average Speeds, Existing (2023) a.m. & p.m. Peaks*

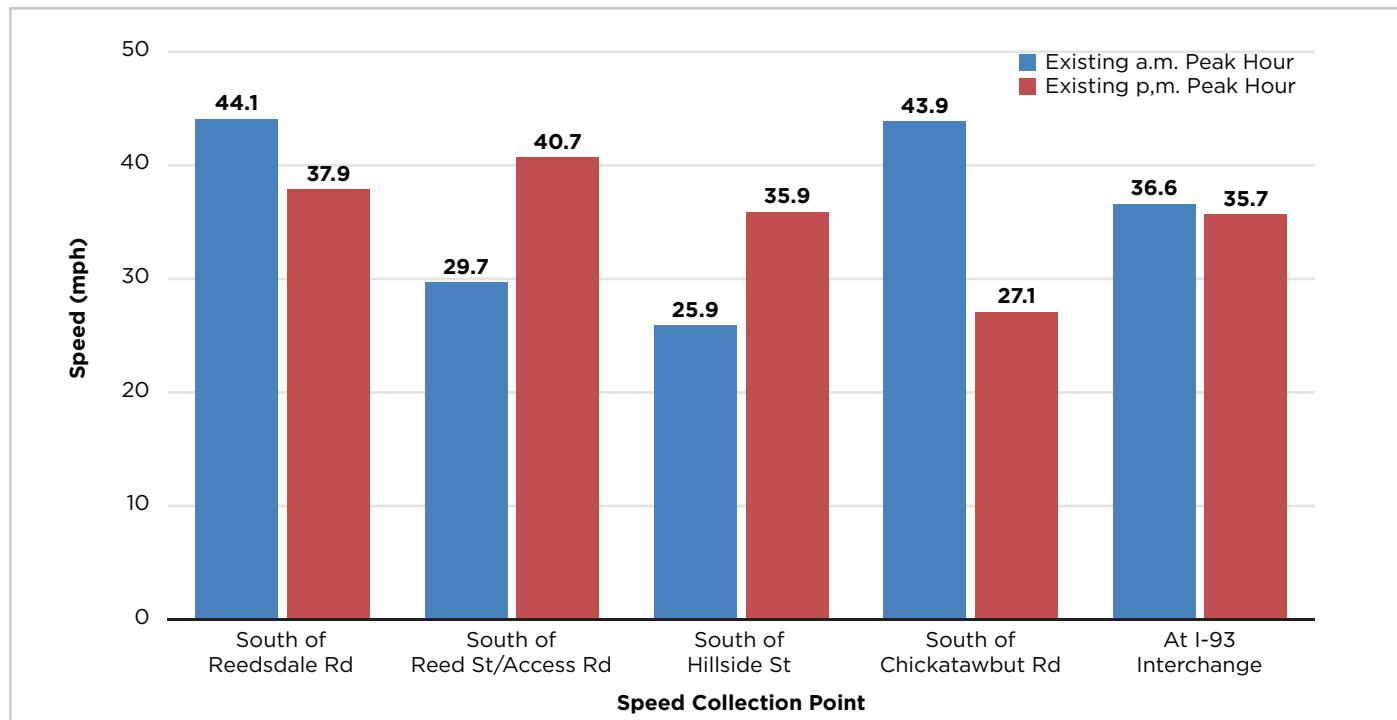


Figure 14. *Route 28 Southbound Average Speeds, Existing (2023) a.m. & p.m. Peaks*

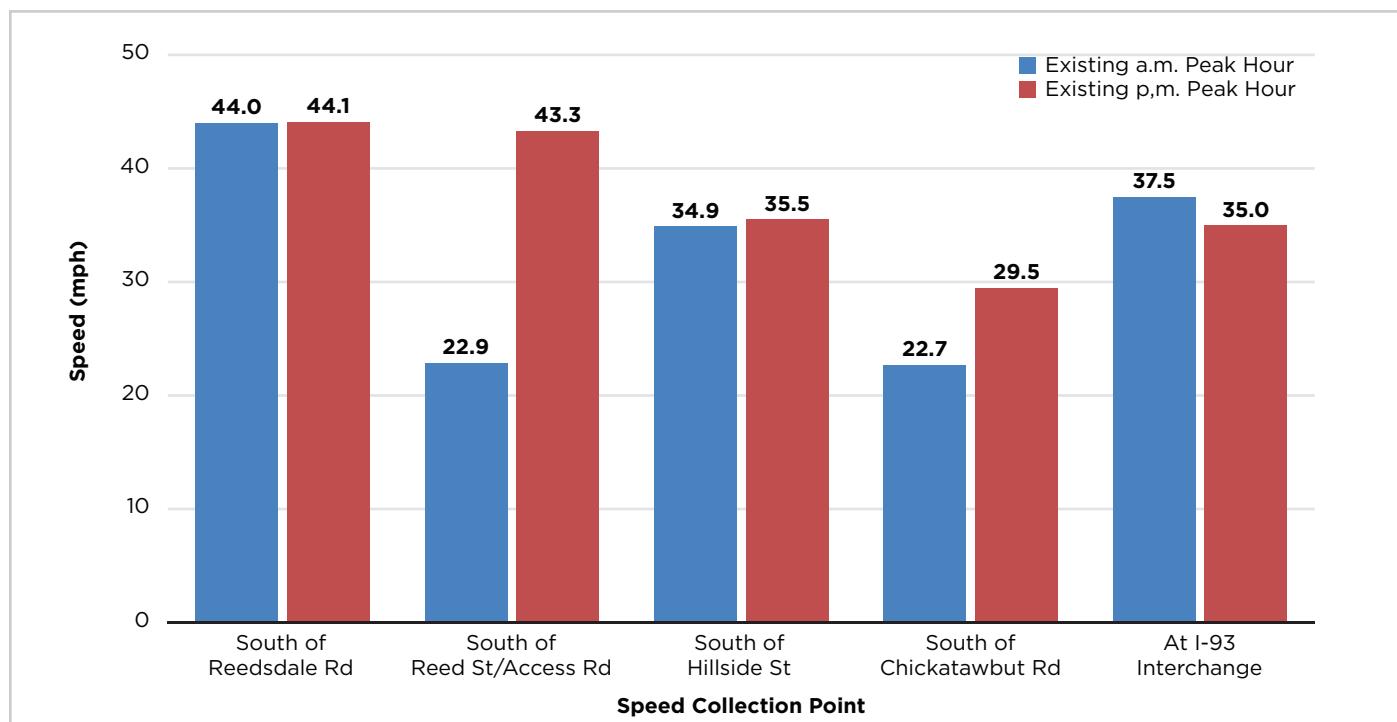




Figure 15. *Route 28 Northbound Speed Comparison of Future Alternatives*

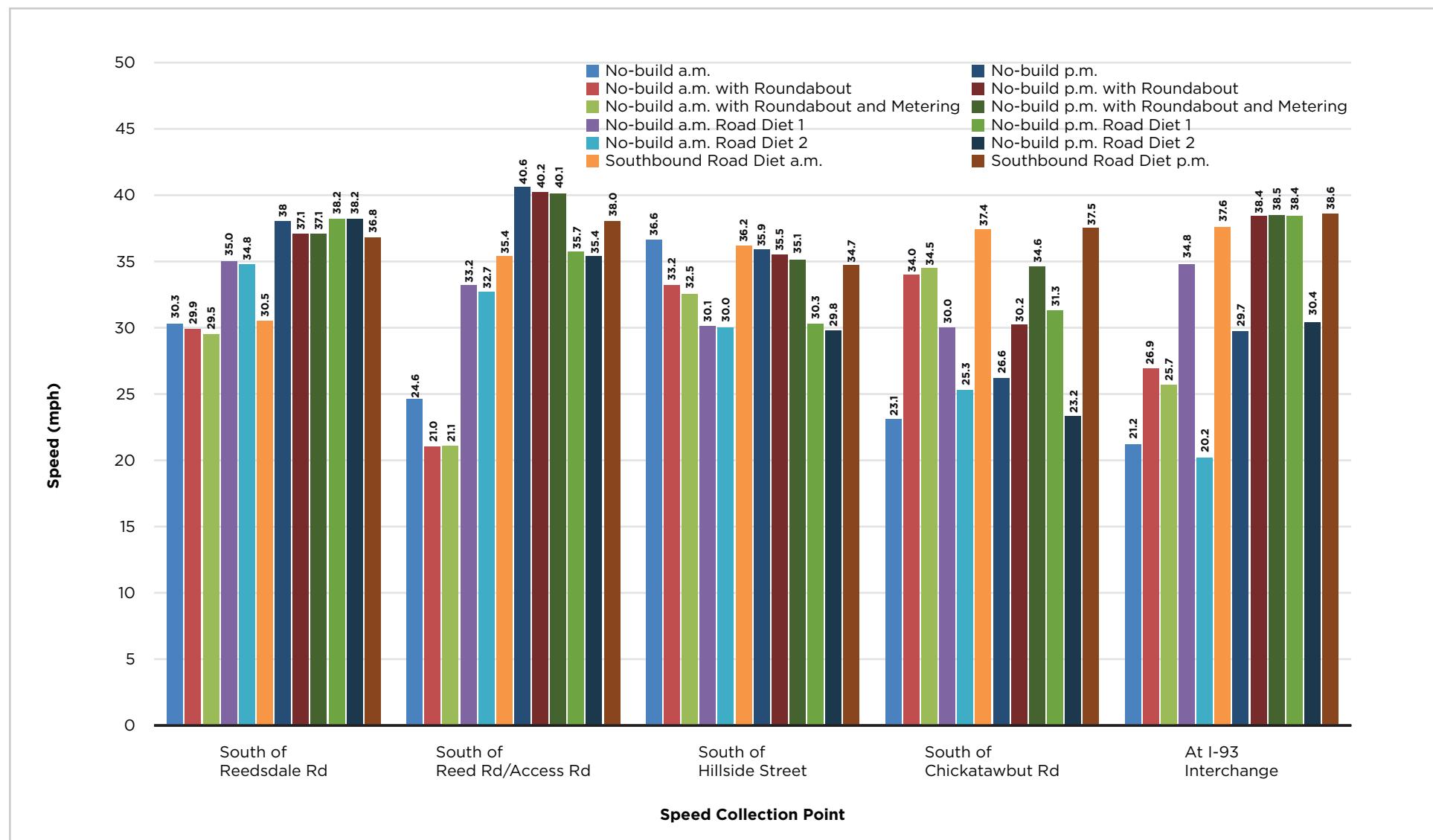
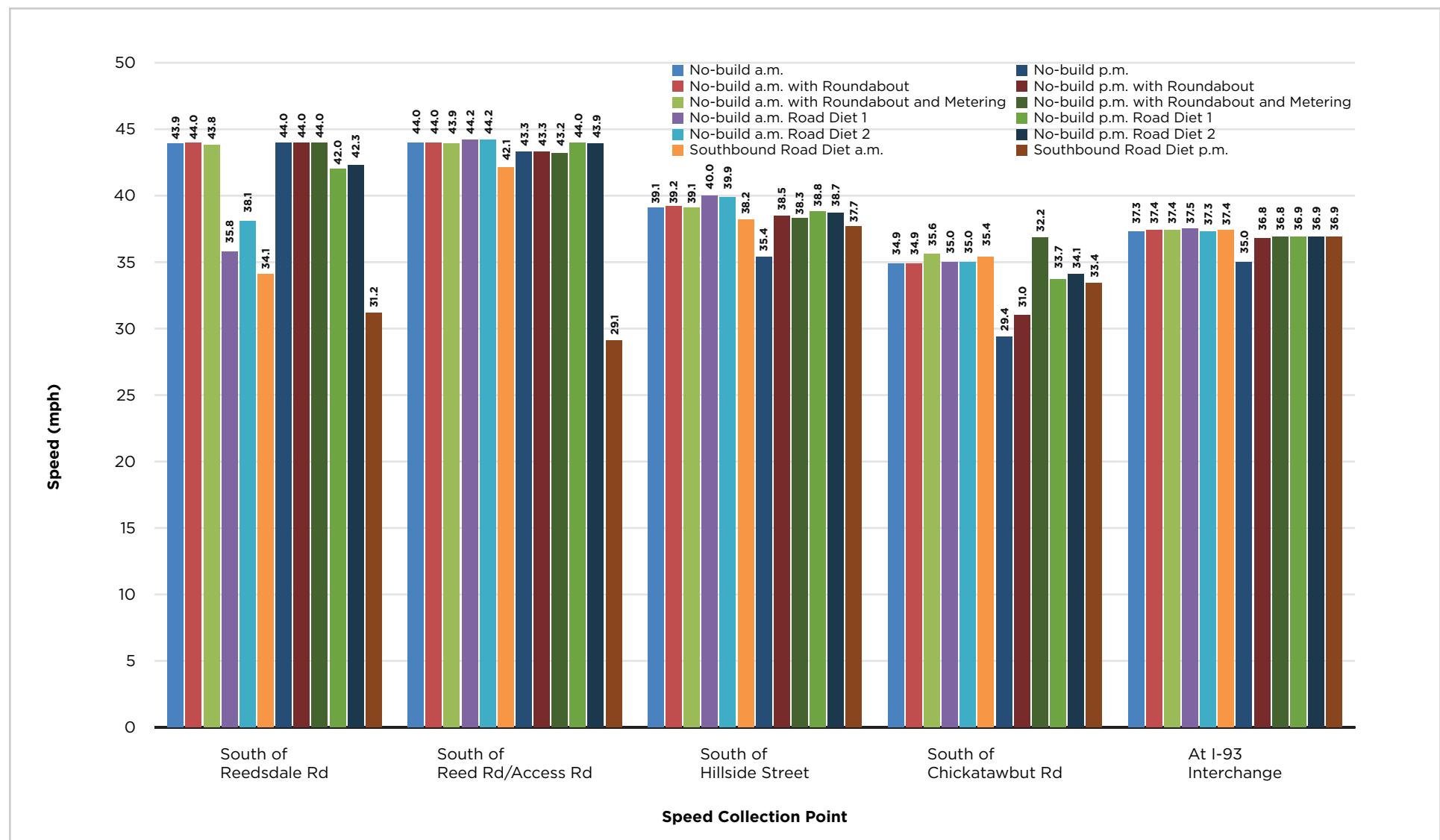




Figure 16. *Route 28 Southbound Average Speeds Comparison of Future Alternatives*





The speed charts presented previously generally show the following:

IN THE NORTHBOUND DIRECTION:

- During the a.m. peak hour, speeds throughout the corridor under Alternatives 1 through 3 vary slightly along the corridor and show an increase over No-build conditions, except for the segment between Hillside Street and Chickatawbut Road that shows a decrease in vehicle speeds; and
- During the p.m. peak hour, Alternative 1 shows a speed decrease between Reed Street/Access Road and Hillside Street, Alternative 2 shows a speed decrease between Reed Street/Access Road and Chickatawbut Road, and Alternative 3 shows a speed decrease between Reedsdale Road and Hillside Street. The remaining segments show an increase in speeds.

IN THE SOUTHBOUND DIRECTION:

- During the a.m. peak hour, Alternative 3 shows speed decreases between Reedsdale Road and Hillside Street, whereas Alternatives 1 and 2 shows speed decreases between Reedsdale Road and Reed Street/Access Road only. The remaining segments show speed increases; and
- During the p.m. peak hour, Alternative 3 shows speed decreases between Reedsdale Road and Reed Street/Access Road, whereas Alternatives 1 and 2 shows speed decreases between Reedsdale Road and Reed Street/Access Road only. The remaining segments show speed increases

DEMAND RATE/UNMET DEMAND

This metric will show two things: a) how the modeled Existing conditions compare to the observed Existing conditions, and b) the expected unmet demand, if any, of each alternative. Unmet demand in this case corresponds to the difference between the number of vehicles programmed to travel through a specific location within the study area based on the measured (or projected) volumes, and the number of vehicles making it through that location under each alternative in the Vissim model.

This comparison will be presented using a modified Chi-Squared statistic called the GEH statistic. The GEH statistic is a formula used in traffic engineering, traffic forecasting, and traffic modeling to compare two sets of traffic volumes. The GEH statistic is an empirical formula that has proven useful for a variety of traffic analysis purposes¹.

¹ "VISSIM Calibration and Validation" Technical Report, Wisconsin Department of Transportation, pg. 5-5



The formula for the GEH statistic is: $GEH = \sqrt{((M-C)^2 / (0.5 \times (M+C)))}$

Where M is the traffic volume from the Vissim model and C is the real-world traffic count. GEH values give an indication of how the model compares to the real-world conditions.

The Existing conditions Vissim model underwent this GEH statistic check to determine if the results were a good match for the observed conditions. The No-build and alternatives underwent this check to compare the results and determine if future alternatives meet the future demand.

For the purpose of the Route 28 Corridor Road Diet Feasibility, the below values will have the corresponding meaning:

- GEH < 5.0 – Vissim modeled demand closely models observed/measured demand;
- For 5 < GEH < 10 – Vissim model shows some congestion; and
- For GEH > 10 – Vissim model shows gridlock and much of the demand isn't met.

Table 1 presents the existing conditions GEH values, and **Table 2** presents the GEH values for the No-build and the alternatives and compares them against each other.



Table 1. Existing (2023) Conditions GEH

Location on Route 28	Northbound GEH	Southbound GEH
a.m. peak Hour		
South of Reedsdale Road	4.5	0.2
South of Reed Street/Access Road	4.5	0.2
South of Hillside Street	4.4	0.5
South of Chickatawbut Road	6.9	0.5
Between the I-93 inner loop ramps	2.9	0.0
p.m. peak Hour		
South of Reedsdale Road	1.4	0.8
South of Reed Street/Access Road	2.7	0.8
South of Hillside Street	2.7	0.8
South of Chickatawbut Road	3.9	2.6
Between the I-93 inner loop ramps	0.5	1.1

As can be seen by the GEH values for the Existing conditions, the southbound modeled demand is a close match to the observed demand for both peak hours. As for the northbound modeled demand, the GEH value for south of Chickatawbut Road indicates congestion, something that is experienced along this part of the corridor, during the a.m. peak hour, in the northbound direction.



Table 2. Demand Rate – No-build (2033) Conditions vs. Alternatives

Location on Route 28	Northbound Demand Rate						Southbound Demand Rate					
	No build	No build w/RBT ⁽¹⁾	No build w/RBT+MET ⁽²⁾	Alternative 1	Alternative 2	Alternative 3	No build	No build w/RBT ⁽¹⁾	No build w/RBT+MET ⁽²⁾	Alternative 1	Alternative 2	Alternative 3
a.m. peak Hour												
South of Reedsdale Road	5.0	5.2	5.3	5.2	8.2	2.2	0.4	0.4	0.3	0.3	3.6	0.6
South of Reed Street/Access Road	5.1	5.1	5.3	9.5	27.4	2.9	0.2	0.2	0.2	0.3	4.7	0.6
South of Hillside Street	4.6	2.8	2.7	9.7	17.0	3.0	0.4	0.3	0.2	0.6	3.8	0.6
South of Chickatawbut Road	7.3	3.2	3.3	6.3	18.6	3.2	0.6	0.4	0.4	0.6	2.9	0.4
Between the I-93 inner loop ramps	4.1	1.8	1.8	1.6	15.9	1.5	0.1	0.1	0.1	0.3	9.1	0.0
p.m. peak Hour												
South of Reedsdale Road	2.4	0.8	0.5	2.2	3.3	0.6	1.5	2.1	2.0	1.7	1.4	6.2
South of Reed Street/Access Road	5.1	1.8	1.3	5.2	6.7	1.0	1.1	1.5	1.5	1.3	1.6	6.8
South of Hillside Street	5.7	1.9	1.1	5.5	7.2	0.7	1.3	1.3	1.2	0.8	1.2	8.0
South of Chickatawbut Road	5.8	0.7	0.3	2.7	7.3	0.7	3.1	3.3	2.9	3.2	2.1	6.8
Between the I-93 inner loop ramps	1.5	0.2	0.3	0.2	1.9	0.4	1.8	2.0	1.7	1.5	1.3	3.6

(1) Future No-Build with Roundabout at Route 28 and Chickatawbut Road

(2) Future No-Build with Roundabout at Route 28 and Chickatawbut Road and with Metering signals on Route 28 legs



The GEH values for the No-build conditions show that conditions for the northbound direction will worsen significantly in the future, whereas the southbound direction will be able to process the increased demand.

When comparing these results, the following conclusions can be drawn:

A.M. PEAK HOUR

- Alternative 1 is expected to process the same demand with the No-build conditions in either direction of the corridor, except for the portion south of Reed Street/Access Road to south of Hillside Street and in the northbound direction only;
- Alternative 2 is expected to process less demand when compared to the No-build conditions in either direction of the corridor; and
- Alternative 3 is expected to process more demand when compared to No-build conditions in the northbound direction, and the same demand with No-build conditions in the southbound direction.

P.M. PEAK HOUR

- Alternative 1 is expected to process the same demand with the No-build conditions, in either direction of the corridor, except for the segment south of Chickatawbut Road;
- Alternative 2 is expected to process more demand than No-build conditions and in the northbound direction. In the southbound direction, Alternative 2 is expected to process demand comparable to the No-build conditions; and
- Alternative 3, in the northbound direction, is expected to process approximately all of the increased demand. However, in the southbound direction, is expected to process less demand than No-build conditions and both Alternatives 1 and 2.

If one of these road diet alternatives is chosen, vehicles are expected to reroute due to increased congestion. Based on recent Origin-Destination data pulled from MassDOT's INRIX (see 2024-04-10 Interim Improvements Presentation and related material submitted to MassDOT on April 10, 2024), assumptions can be made for what roadways vehicles may divert to in order to avoid this increased congestion. For the northbound road diet, drivers might use I-93 Northbound, which is already congested during the a.m. peak hour, but this is acceptable as I-93 should be used instead of Route 28. For the southbound road diet, drivers might use Route 138, Unquity Road, or Reedsdale Road to Pleasant Street, connecting to East Milton Square and I-93 Southbound. However, this would increase traffic on mostly residential or slow-speed roads, raising safety concerns for residents leaving their driveways.



DRIVEWAY DELAY

Concerns about impacts to traffic from the proposed Route 28 at Chickatawbut Road roundabout and the heavy traffic on Route 28 include access for properties and local side streets near the proposed roundabout. The driveway delays under No-build conditions and proposed alternatives were analyzed using Vissim, focusing on driveways between Susi Lane and Hillside Street. In No-build, No-build with Roundabout, and No-build with Roundabout and Metering conditions, the studied movement was a left turn from the driveway to Route 28 Southbound. Under the alternatives, this movement is proposed as a right turn out of the driveways and a U-turn at the signalized intersection of Route 28 and Hillside Street, the nearest intersection allowing a U-turn.

Although field observations were not conducted at these driveways, they were consistently modeled in Vissim for a fair comparison. The metric focuses on driveway delay under No-build conditions and alternatives. **Figure 17** and **Figure 18** show the driveway delay analysis results.

Tabulated data for the driveway delays can be found in **Appendix B**.



Figure 17. *Driveway Delay within Merge Area – a.m. Peak Hour*

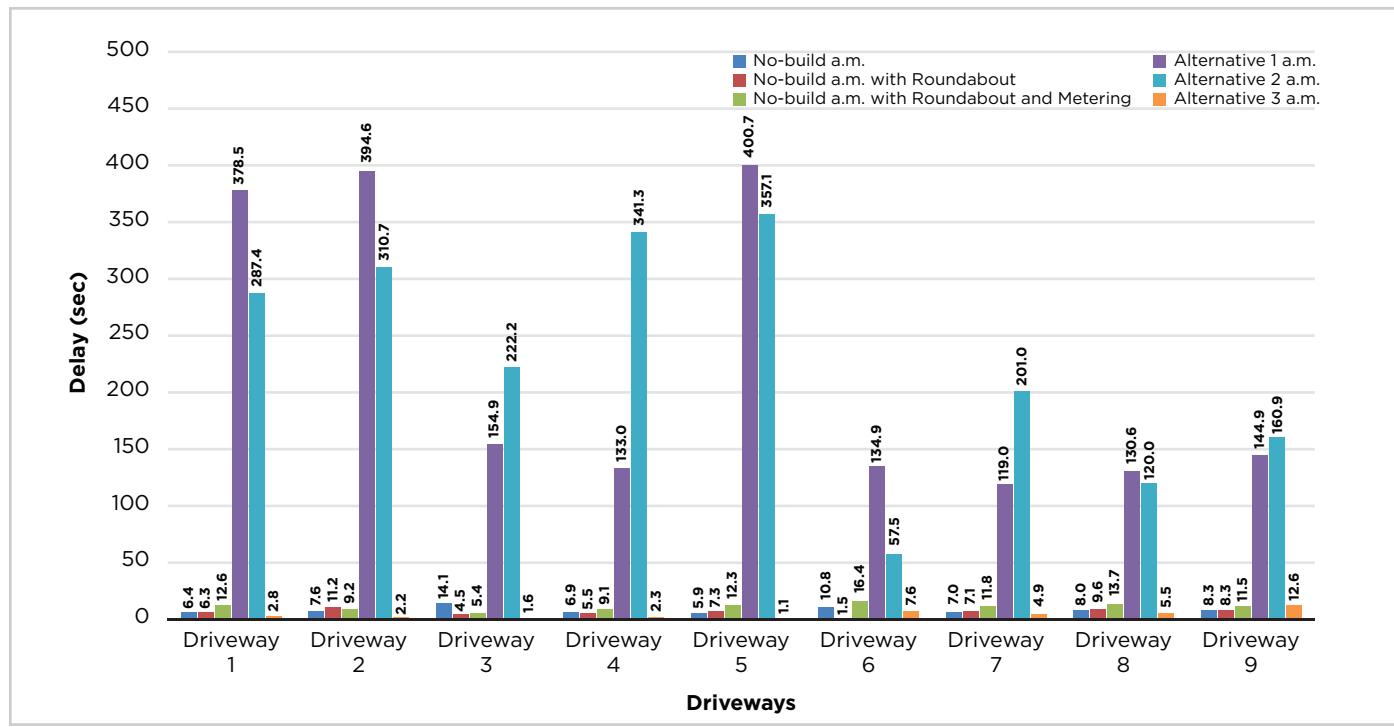
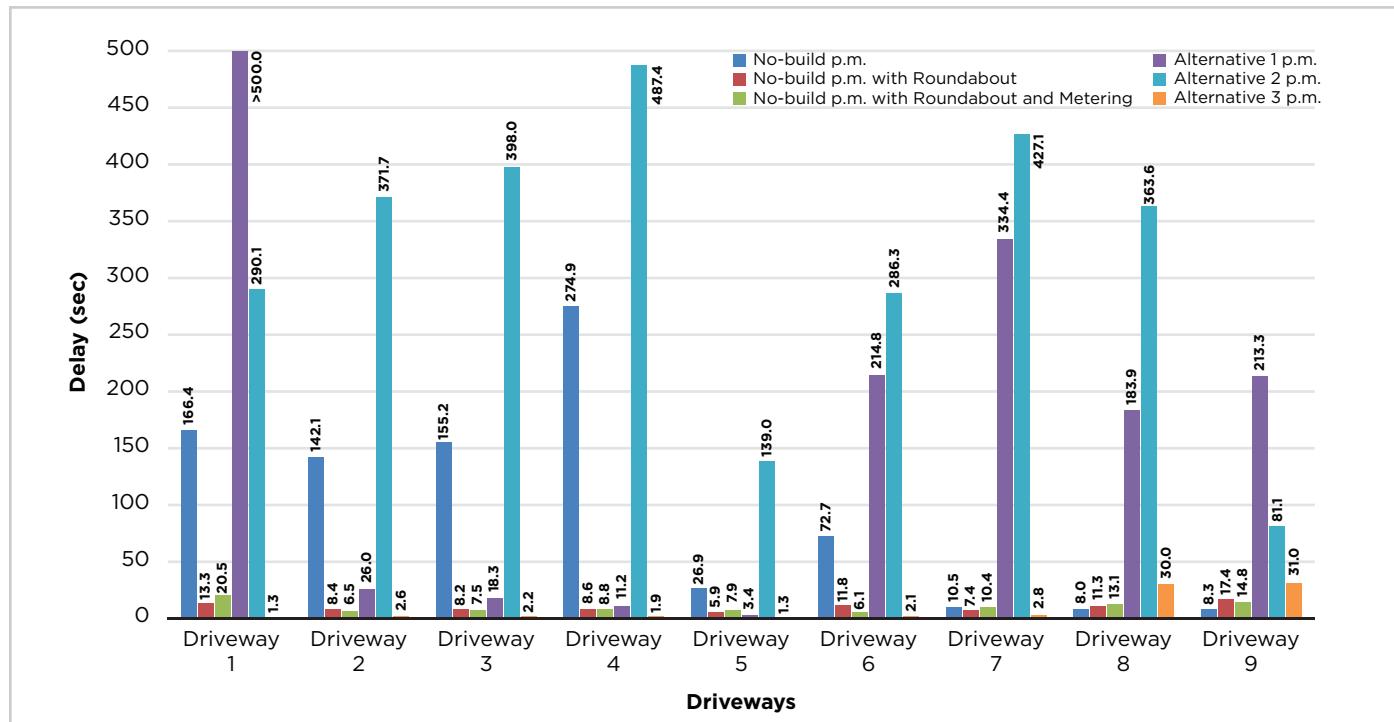


Figure 18. *Driveway Delay within Merge Area – p.m. Peak Hour*





The two driveway delay charts show that Alternative 1 and 2 are expected to increase the delay experienced by the driveways located between Susi Lane and Hillside Street, when compared to the No-build conditions and Alternative 3. On the other hand, under Alternative 3, those driveways are expected to see similar to less delay when compared to No-build conditions and the other alternatives.

QUEUES ALONG ROUTE 28 CORRIDOR

The queue information at the signalized intersections and the roundabout at Route 28 and Chickatawbut Road were also collected under this study. The focus was the queues on the Route 28 mainline.

The queues are presented in this memo to show if there are any expected queues that will be very long and spill back to adjacent intersections. The queues are presented in **Figure 19** through **Figure 22** as bar charts and, following those charts, are a discussion of the queues and specifically those that are expected to spill back to adjacent intersections.

Tabulated data for the queues can be found in **Appendix B** in the capacity analysis tables. It should be noted that where queues are spilling back beyond one or more intersections, they were added together to show the actual queue length in the charts below.



Figure 19. a.m. Peak Hour Average and Maximum Queues – Route 28 Mainline Eastbound/Southbound

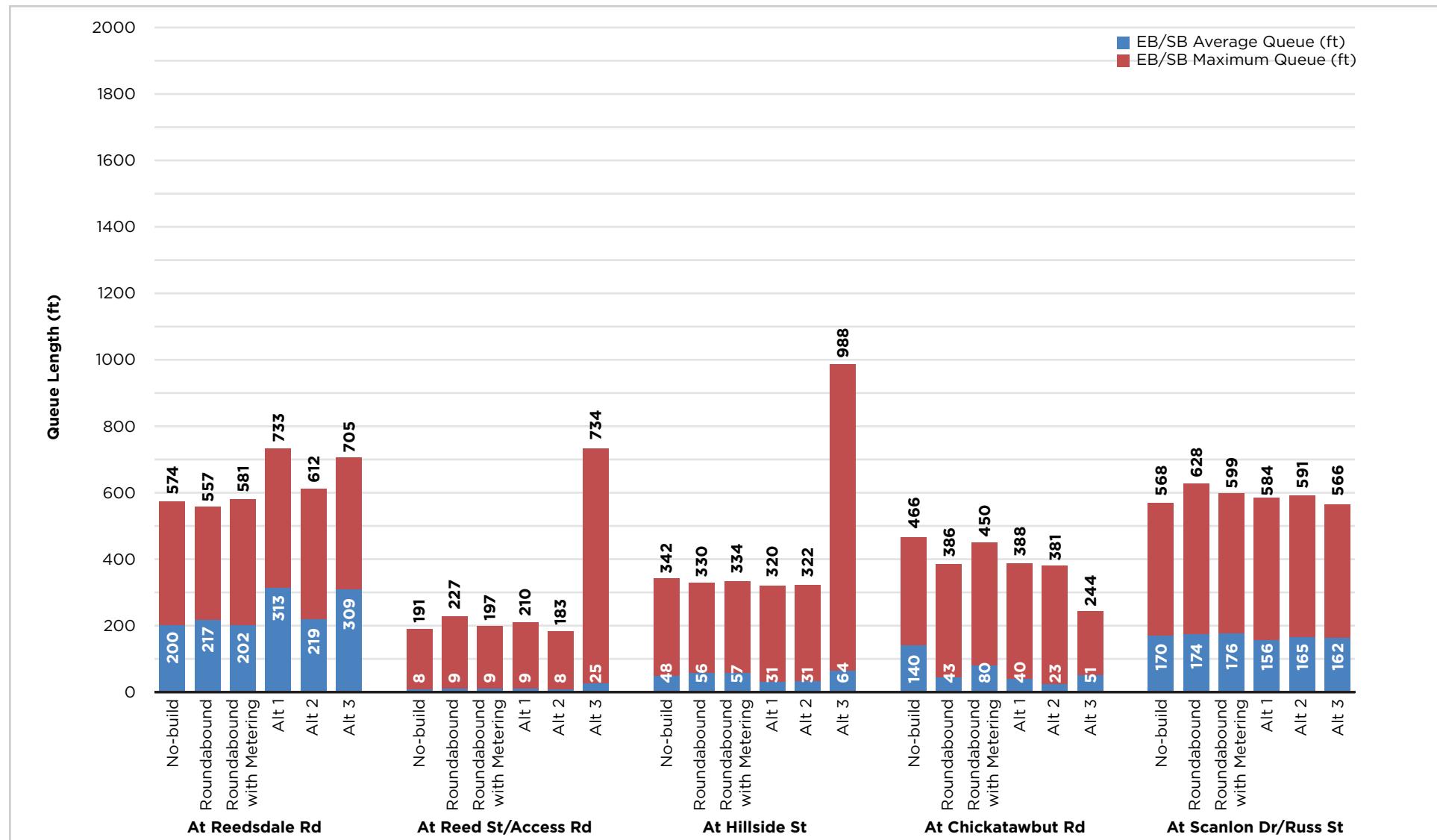




Figure 20. *p.m. Peak Hour Average and Maximum Queues – Route 28 Mainline Eastbound/Southbound*

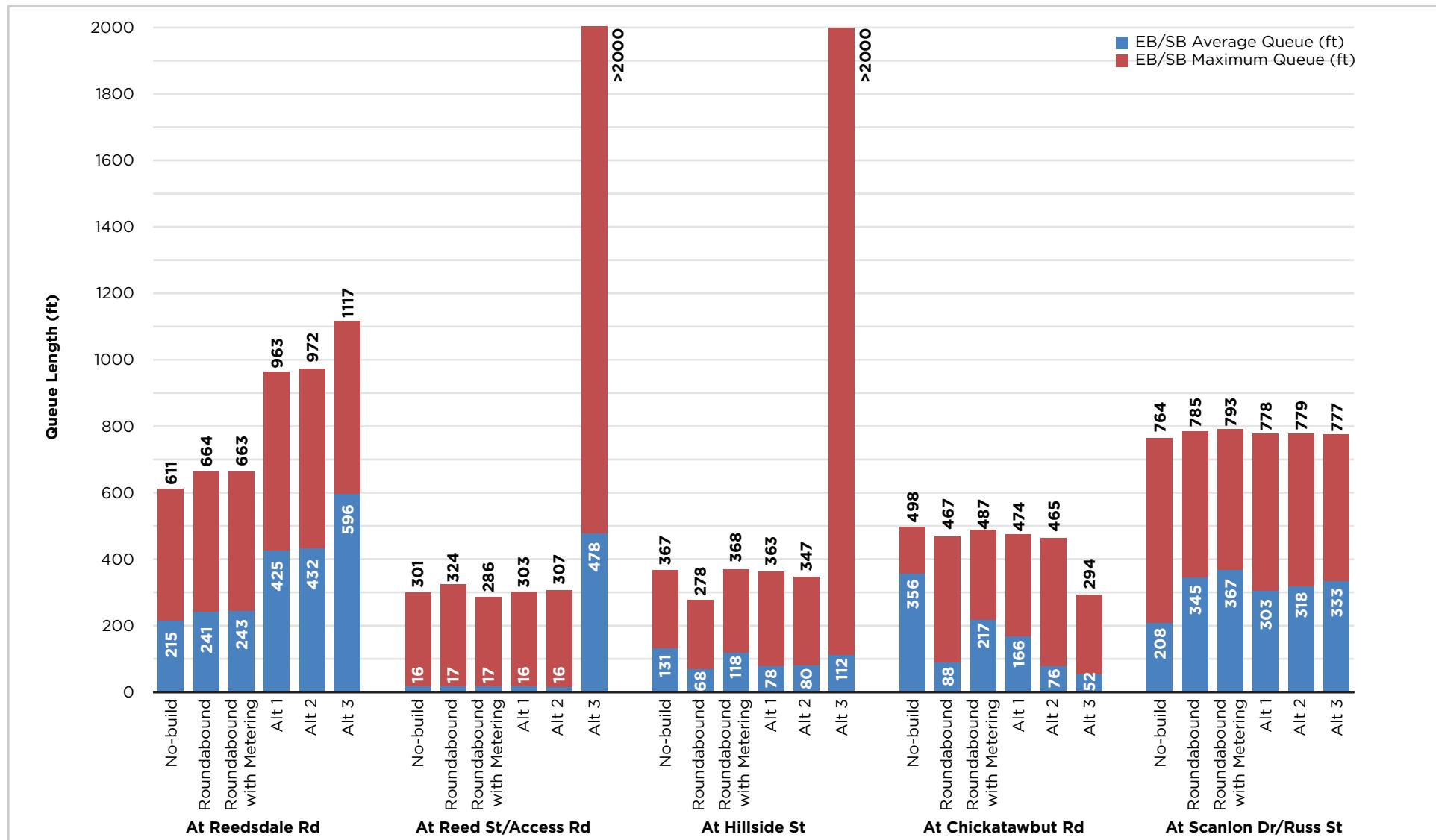




Figure 21. a.m. Peak Hour Average and Maximum Queues – Route 28 Mainline Northbound

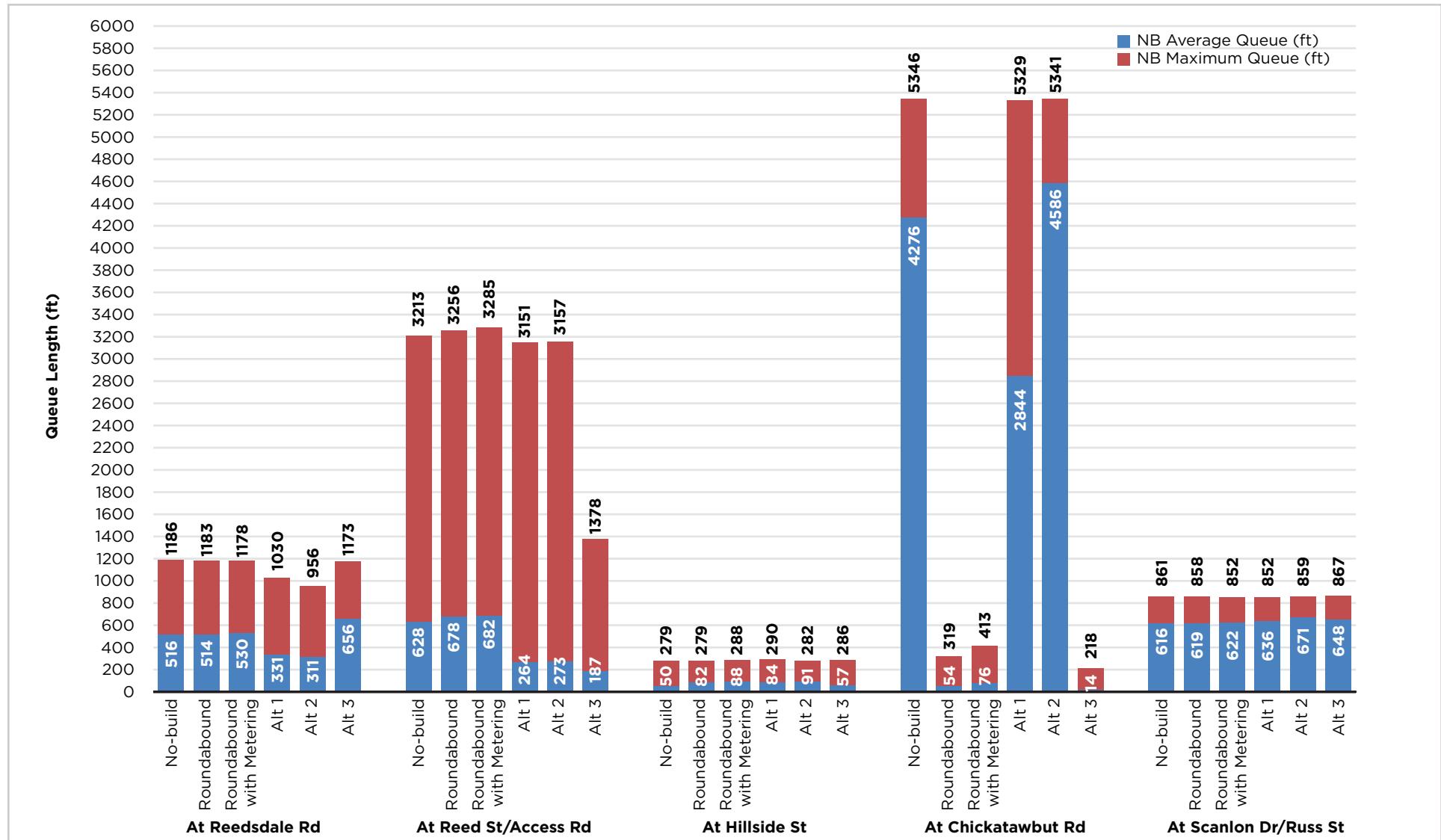
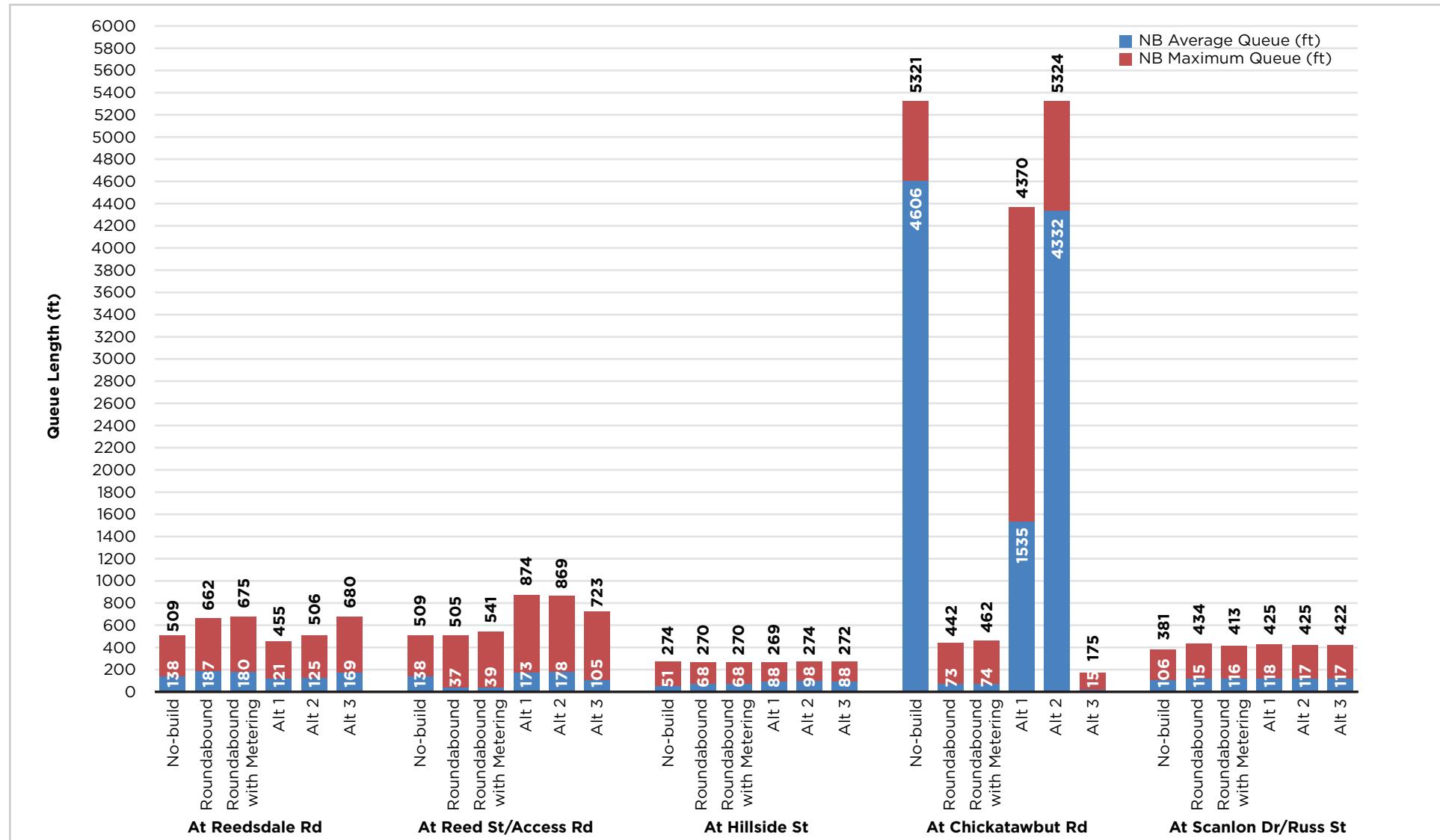




Figure 22. *p.m. Peak Hour Average and Maximum Queues – Route 28 Mainline Northbound*





As the charts show, most of the queues along the corridor and the signalized intersections are contained within the intersection and not spilling back to other intersections, except for the following:

- **Route 28 at Hillside Street** – a.m. and p.m. southbound queues will spill back to other intersections under Alternative 3. Specifically, during the a.m. peak, it is expected that the queues will extend to just south of Ridgewood Road. During the p.m. peak hour, it is expected that the southbound queues will reach just south of Reedsdale Road. Due to the length of this queue, Reedsdale Road eastbound is expected to experience queues that will reach past Clifton Street.
- **Route 28 at Reedsdale Road** – a.m. peak hour queues in the northbound direction are expected to reach just past Pleasant Street under Alternative 3.
- **Route 28 at Reed Street/Access Road** – a.m. and p.m. peak hour queues in the northbound direction, and under Alternatives 1 and 2, are expected to reach past Sassamon Avenue.
- **Route 28 at Chickatawbut Road** – a.m. and p.m. peak hour northbound queues are expected to reach near the I-93 Interchange under Alternatives 1 and 2. These lengthy queues are expected to influence queues throughout the interchange, as happens today under Existing conditions.

Conclusion

To summarize the results, when looking at the different metrics for each alternative the following results can be inferred:

- **Travel times and Vehicle-Hours of Delay:** Alternative 3 provides the better reduction in travel time and vehicle-hours of delay, only in the northbound direction, over the other alternatives and in either peak hour, whereas Alternative 2 provides the better reduction in travel time and vehicle-hours of delay in the southbound direction.
- **Average Speeds:** While the point of the improvements is not to increase speeds along the corridor, a road diet may affect the speeds as it may create or ease congestion at points throughout the corridor. For example, there is a large drop in average speed in the southbound direction and in the p.m. peak hour under Alternative 3. As the other metrics show, Alternative 3 is expected to experience long queues during the p.m. peak hour, thus slower speeds. The alternatives with the largest increases to speeds are Alternative 1 and Alternative 3 in the northbound direction and both peak hours.



- **Demand Rate:** Depending on the peak hour and the traveling direction, each alternative sees locations where the processed demand does not improve over the No-build conditions. In the a.m. peak hour and in the northbound direction, Alternatives 1 and 2 see less demand processed over the No-build. In the p.m. peak hour and in the southbound direction, Alternative 3 sees less demand processed over the No-build, whereas, in the northbound direction, Alternative 2 sees less demand processed over the No-build;
- **Driveway Delay:** Alternative 3 provides the better reduction in delay, or delays that are similar to No-build conditions, experienced by driveways near the proposed roundabout at Route 28 and Chickatawbut Road, whereas Alternatives 1 and 2 increases the delay expected at those same driveways by minutes in many cases.
- **Queues along Route 28 Corridor:** Similar to the other metrics, the queues also show areas of congestion under each alternative, depending on the peak hour and travel direction. When looking in the northbound direction and during both the a.m. and p.m. peak hours, Alternatives 1 and 2 are expected to see long northbound queues at Route 28 and Chickatawbut Road, which have the potential of impacting the Route 28 at I-93 interchange, similar to the No-build conditions. When looking at the southbound direction and the p.m. peak only, Alternative 3 is expected to see long southbound queues at Route 28 Hillside Street intersection that spill back all the way to Route 28 at Reedsdale Road intersection, much longer than seen under No-build or Alternatives 1 and 2.

In summary, the memorandum shows that a road diet along Route 28 is feasible only in the p.m. peak hour in the northbound direction and between Hillside Street and Reedsdale Road, or in the southbound direction between Hillside Street and Chickatawbut Road and only in the a.m. peak hour. If a road diet were implemented along the entire length of the Route 28 corridor, it is likely that vehicles will divert to I-93 (northbound road diet) or local streets and arterials (southbound road diet), like Route 138, Unquity Road, or Reedsdale Road to Pleasant Street that connect to East Milton Square and I-93 Southbound. A road diet can work for part of the Route 28 corridor but not the entire stretch, unless vehicles reroute to other roadways. For driveway delay, maintaining two northbound lanes reduces delays, as shown in Alternative 3, highlighting the need for two lanes up to Hillside Street to handle a.m. peak northbound demand and avoid merge issues, unless, again, Route 28 northbound vehicles reroute to I-93 northbound.

To conclude, while this memorandum focuses on comparing the future No-build conditions to the three different road diet alternatives, data on all metrics for the No-build conditions with a roundabout at Route 28 and Chickatawbut Road with the PHBs and without the PHBs but with



metering signals, are also presented. While those two conditions show similar conditions to existing/future No-build conditions, it should be noted that the only change considered under the No-build conditions with a roundabout at Route 28 and Chickatawbut Road with the PHBs and without the PHBs but with metering signals, is the roundabout at Route 28 and Chickatawbut Road and no other changes at the rest of the corridor.

HSH is available to discuss the findings of the memorandum further at the request of MassDOT.



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Appendix A

Milton – Route 28 Corridor Road Diet Feasibility Study
from Chickatawbut Road to Reedsdale Road
Supplemental Memorandum



TO: Joshua Bartus, Project Manager
MassDOT

FROM: Haralampos Stathopoulos, P.E., PTOE, HSH
Jessica Lizza, P.E., PTOE, HSH

SUBJECT: Milton – Route 28 Corridor Road Diet Feasibility Study from Chickatawbut Road to Reedsdale Road – Addendum #1

DATE: December 20, 2024
(Revised February 20, 2025)

HSH PROJECT NO.: 2021055.15

Introduction

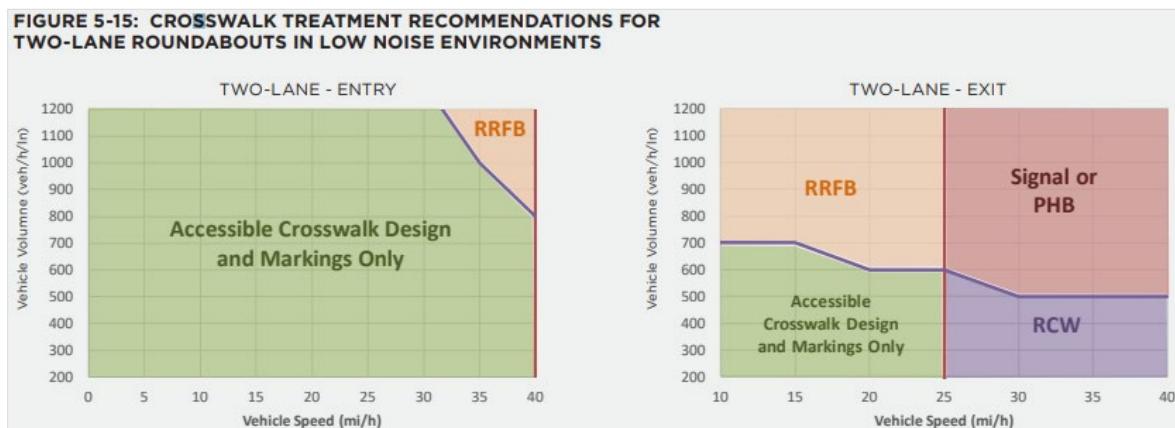
This technical memorandum is an addendum to the memorandum titled “Milton Route 28 Corridor Road Diet Feasibility Study from Chickatawbut Road to Reedsdale Road”, submitted to the Massachusetts Department of Transportation (MassDOT) by **Howard Stein Hudson (HSH)** on August 1, 2024. This memorandum focuses on delay at the driveways between Hillside Street and Chickatawbut Road, and at Eager Road and Susi Lane, as presented in the August memorandum. HSH met with MassDOT on August 13, 2024, to discuss the road diet feasibility study results. In that meeting, MassDOT requested that HSH study the impacts to the driveways and local roadways located along the part of Route 28 between the Chickatawbut Road proposed roundabout and south of the Hillside Street signalized intersection without a road diet in place, and also study what metering the proposed roundabout would do to the driveways and side streets in question; this information was not studied as part of the August memorandum.

Roundabout metering was suggested by concerned Milton residents during the design development of the project and was studied under a Roundabout Metering memorandum completed in May 2023. That study analyzed metering effects only at the roundabout and using the SIDRA software, which did not provide any input on driveway delay, just changes in operation at the proposed roundabout under metering. The May 2023 memorandum suggested more in-depth analysis to determine if roundabout metering will negatively or positively impact the concerned driveways and side streets. The additional analysis was completed under this addendum.

It should be noted that to implement roundabout metering at the proposed Chickatawbut Road roundabout, the currently proposed Pedestrian Hybrid Beacon (PHB) on the Route 28 approach and departure legs will need to be removed as they would conflict with the roundabout metering signal control. However, the MassDOT *Guidelines for the Planning and Design of Roundabouts* (March 2022) requires the PHBs be provided for the Route 28 crossings, as depicted by **Figure 1**, an excerpt from the document.



Figure 1. Crosswalk Treatment Recommendations for Two-Lane Roundabouts in Low Noise Environments



Vehicles on Route 28 currently travel with speeds above 30 miles per hour (mph); the volume in both directions of Route 28 is over 700 vehicles per hour per lane (vphpl). According to this data, the guidelines recommend a PHB for safe crossings. If the roundabout metering is implemented and the PHBs are removed, the crossings would require a different type of control to maintain the safety currently provided by the PHBs. A possible option is Rectangular Rapid Flashing Beacons (RRFBs) with raised crossings. Alternative crossings would require further investigation.

When it comes to volumes at the studied residential driveways, it was assumed that one vehicle per hour would enter Route 28 from the driveways, as no turning movement counts were conducted at the driveways, just side streets. **Table 1** and **Table 2** present the expected delays at the concerned driveways and side streets under the following conditions:

- Future No-build – Future volumes (2033), the signal at Route 28 and Chickatawbut Road is retained as it is today, and no other changes occur along the corridor;
- Future No-build with Roundabout – Future volumes, the proposed roundabout at Route 28 and Chickatawbut Road is installed, and no other changes occur along the corridor;
- Future No-build with Roundabout and Metering – Future volumes, the proposed roundabout at Route 28 and Chickatawbut Road is installed and provided with metering signals but no PHBs, and no other changes occur along the corridor; and
- Alternative 1, Alternative 2, and Alternative 3 are as described in the August 2024 Road Diet Feasibility Study memorandum.



Table 1. a.m. Peak Hour Driveway Delay Comparison – No-build vs. Alternatives

Location on Route 28	No-build Delay (sec)	No-build w/ Roundabout Delay (sec)	No-build w/ Roundabout Metering Delay (sec)	Alternative 1 Delay (sec)	Alternative 2 Delay (sec)	Alternative 3 Delay (sec)
a.m. peak Hour						
Between Eager Rd and Susi Lane						
Susi Ln EB	3.7	4.1	4.1	15.5	7.1	1.8
Susi Ln WB	8.0	7.5	7.9	34.6	42.7	8.6
Driveway #1	6.4	6.3	12.6	378.5	287.4	2.8
Driveway #2	7.6	11.2	9.2	394.6	310.7	2.2
Driveway #3	14.1	4.5	5.4	154.9	222.2	1.6
Driveway #4	6.9	5.5	9.1	133.0	341.3	2.3
Driveway #5	5.9	7.3	12.3	400.7	357.1	1.1
Between Hillside St and Eager Rd						
Eager Rd WB	10.3	12.5	8.1	127.7	66.0	13.2
Driveway #6	10.8	1.5	16.4	134.9	57.5	7.6
Driveway #7	7.0	7.1	11.8	119.0	201.0	4.9
Driveway #8	8.0	9.6	13.7	130.6	120.0	5.5
Driveway #9	8.3	8.3	11.5	144.9	160.9	12.6
Avg. Delay	8.1	7.1	10.2	180.7	181.2	5.4
Max. Delay	14.1	12.5	16.4	400.7	357.1	13.2
Min. Delay	3.7	1.5	4.1	15.5	7.1	1.1



Table 2. p.m. Peak Hour Driveway Delay Comparison – No-build vs. Alternatives

Location on Route 28	No-build Delay (sec)	No-build w/ Roundabout Delay (sec)	No-build w/ Roundabout Metering Delay (sec)	Alternative 1 Delay (sec)	Alternative 2 Delay (sec)	Alternative 3 Delay (sec)
p.m. peak Hour						
Between Eager Rd and Susi Lane						
Susi Ln EB	16	7.9	11.0	9.4	11.4	12.6
Susi Ln WB	24.4	3.7	13.4	24.1	19.5	4.0
Driveway #1	166.4	13.3	20.5	532.6	290.1	1.3
Driveway #2	142.1	8.4	6.5	26.0	371.7	2.6
Driveway #3	155.2	8.2	7.5	18.3	398.0	2.2
Driveway #4	274.9	8.6	8.8	11.2	487.4	1.9
Driveway #5	26.9	5.9	7.9	3.4	139.0	1.3
Between Hillside St and Eager Rd						
Eager Rd WB	33.1	10.2	9.7	101.3	58.5	19.5
Driveway #6	72.7	11.8	6.1	214.8	286.3	2.1
Driveway #7	10.5	7.4	10.4	334.4	427.1	2.8
Driveway #8	8	11.3	13.1	183.9	363.6	30.0
Driveway #9	8.3	17.4	14.8	213.3	81.1	31.0
Avg. Delay	96.1	10.3	10.6	170.9	316.0	8.4
Max. Delay	274.9	17.4	20.5	532.6	487.4	31.0
Min. Delay	8.0	1.5	4.1	3.4	7.1	1.1



The results in **Table 1** and **Table 2** show the following:

- During the a.m. peak hour, the Alternative 3 – Southbound Road Diet scenario is expected to see the lowest average and minimum delays and perform the best overall when it comes to the driveways, Susi Lane and Eagle Road. The No-build with Roundabout scenario is expected to see the second lowest delays, while the No-build with Roundabout and Metering option is expected to see an increase in delay compared to the No-build scenario. Alternative 1 and Alternative 2 scenarios – both Northbound Road Diet options – are expected to see substantial delay increases.
- During the p.m. peak hour, the same results as in the a.m. peak hour can be seen – Alternative 3 scenario is expected to see the lowest average and minimum delays and perform the best overall for the driveways, Susi Lane and Eagle Road, with the No-build with Roundabout seeing the second lowest delays. The No-build with Roundabout and Metering scenario is expected to see lower delays than the No-build scenario but slightly worse than the No-build with Roundabout scenario. Alternative 1 and Alternative 2 scenarios are still expected to see substantial delay increases.

While Alternative 3 is expected to see a decrease in delays for the driveways and side streets immediately to the north of the Route 28 at Chickatawbut Road proposed roundabout, when compared to the No-build and all other scenarios studied, as can be seen in the August 2024 memorandum, Alternative 3 is also expected to create heavy congestion on Route 28 southbound, especially in the p.m. peak hour, which may cause vehicles to reroute and use local streets, like Route 138, Unquity Road, Reedsdale Road, and Pleasant Street to avoid this congestion.

The next two scenarios that provide a decrease in driveway and side street delay are the No-build with Roundabout and No-build with Roundabout and Metering. The No-build with Roundabout scenario provides slightly larger decrease in delay, meaning that providing metering signals at the roundabout is not expected to provide a larger benefit than the roundabout with the PHBs, making the No-build with Roundabout scenario the preferable scenario to improve driveway and side street delay.



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Appendix B

Traffic Data, VISSIM Calibration, and Analysis Results



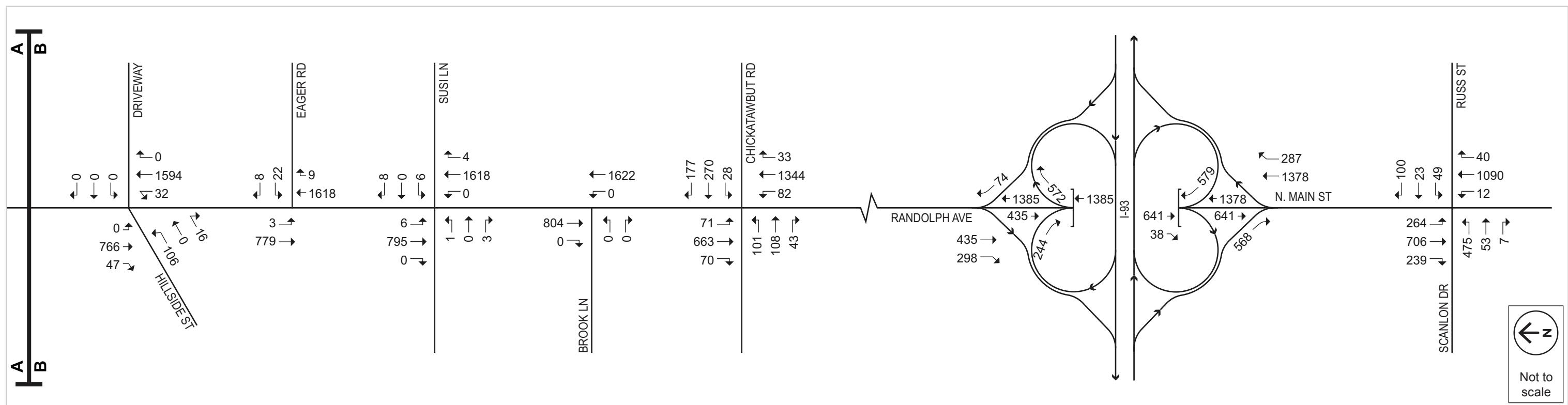
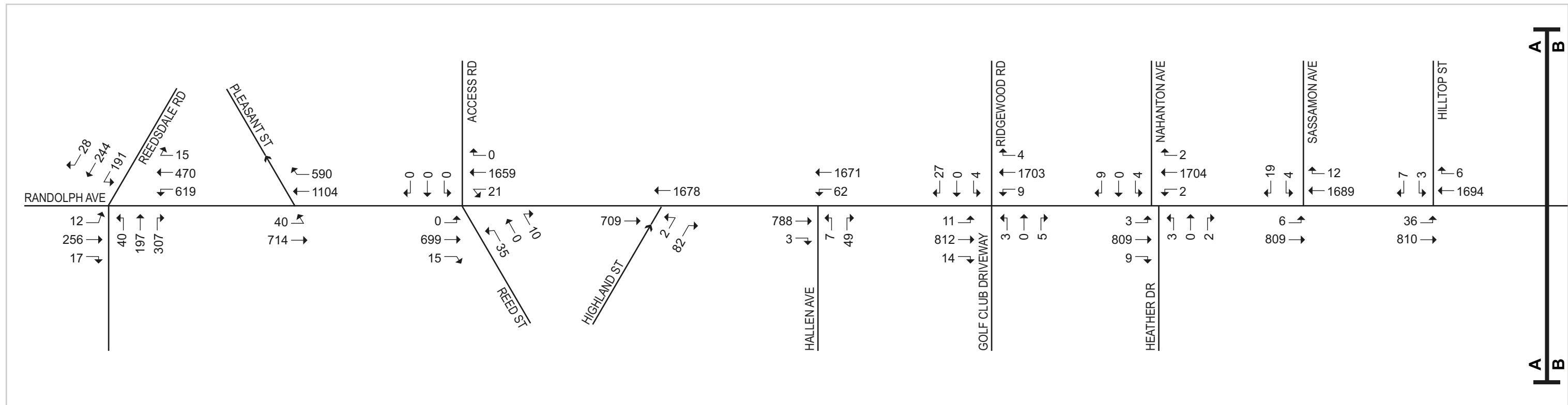
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Existing (2023) a.m. and p.m. Vehicle, Pedestrian, and Bicycle Volumes

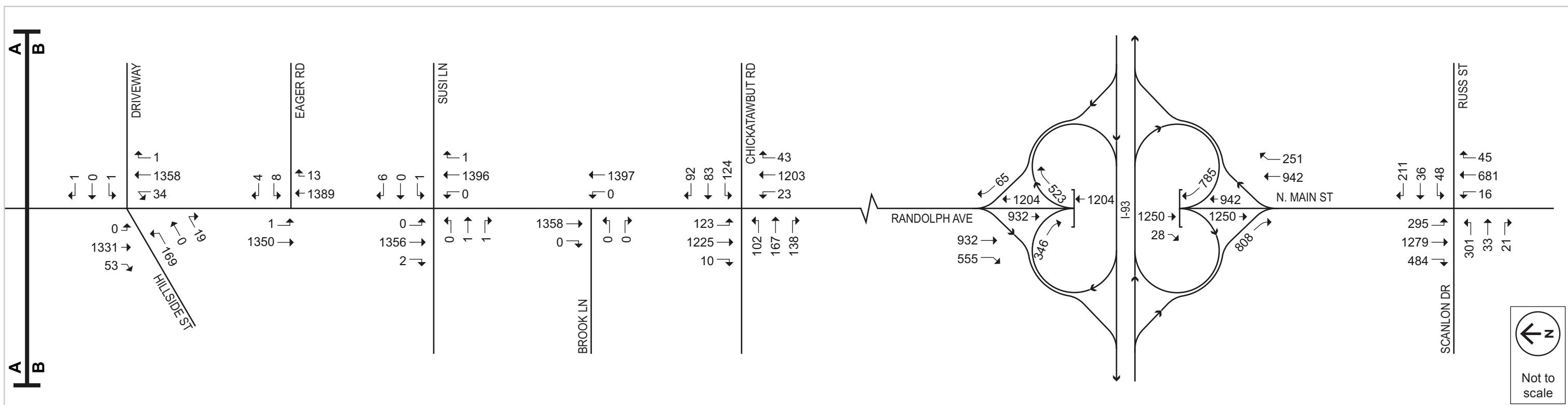
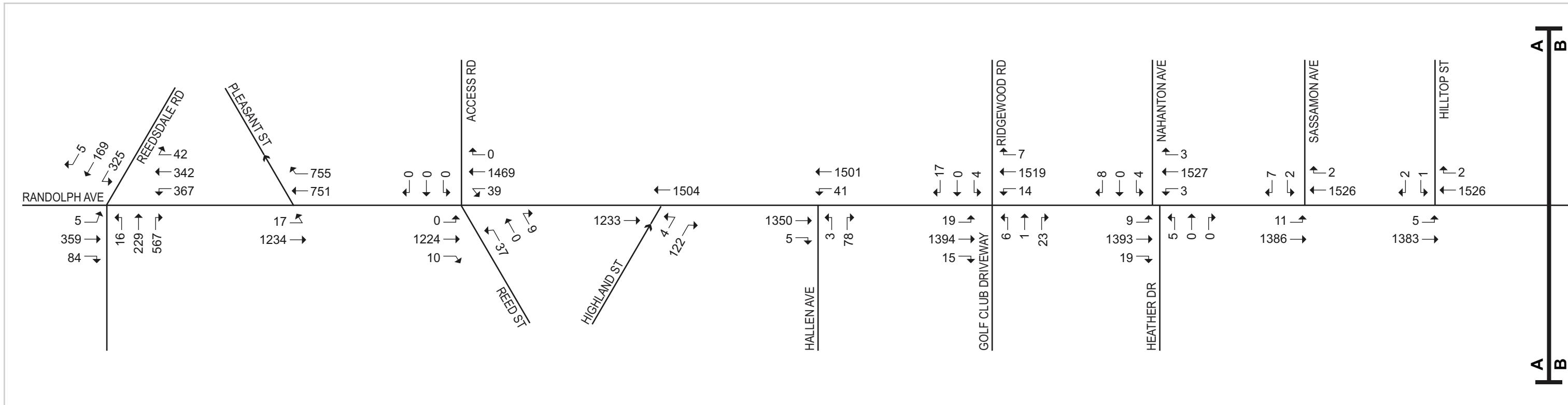


Appendix C. Existing (2023) Condition Vehicle Volumes, Weekday a.m. Peak Hour



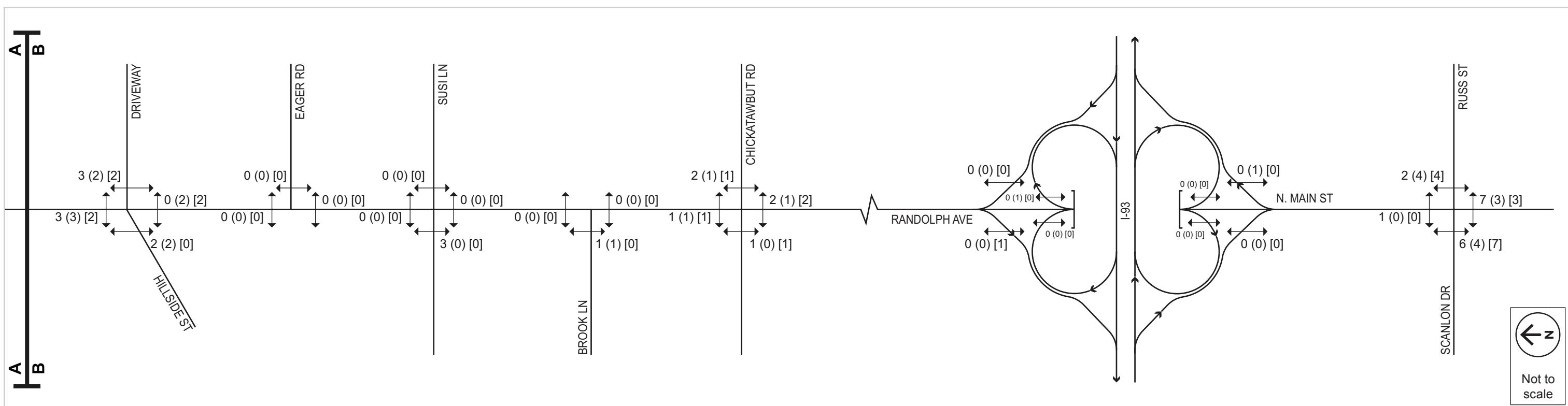
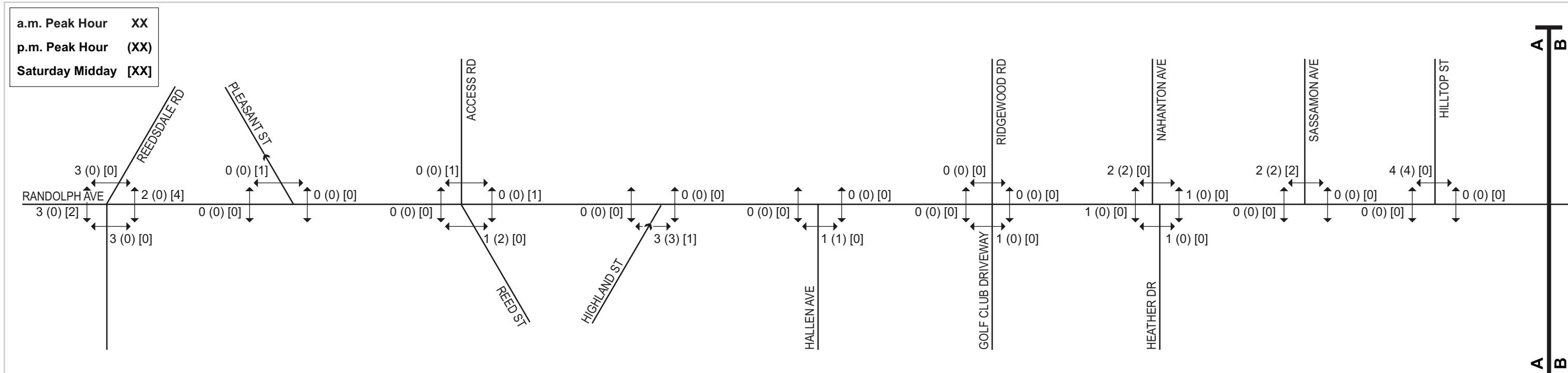


Appendix C. *Existing (2023) Condition Vehicle Volumes, Weekday p.m. Peak Hour*



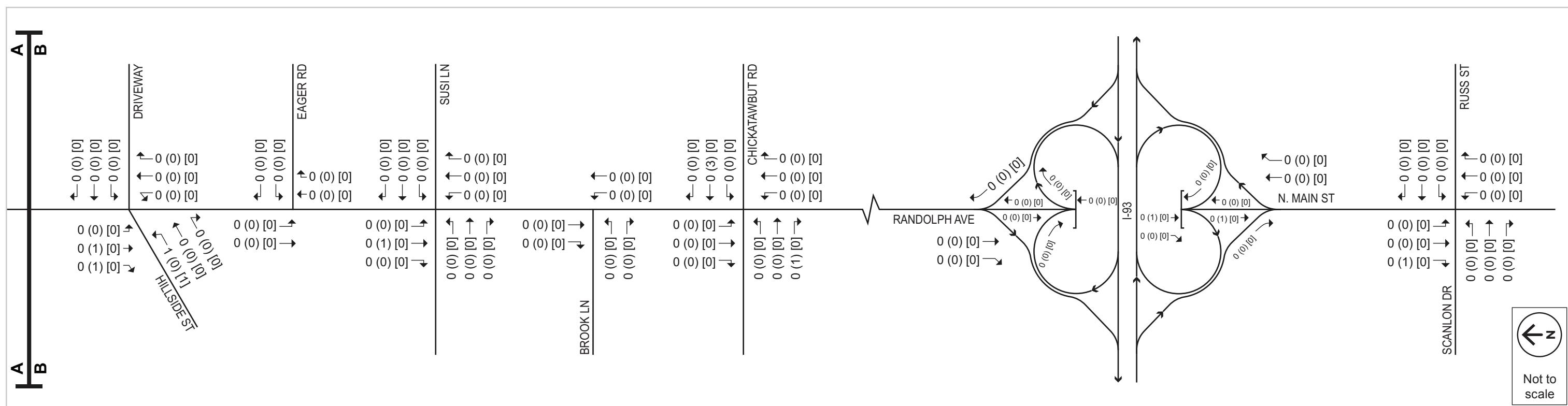
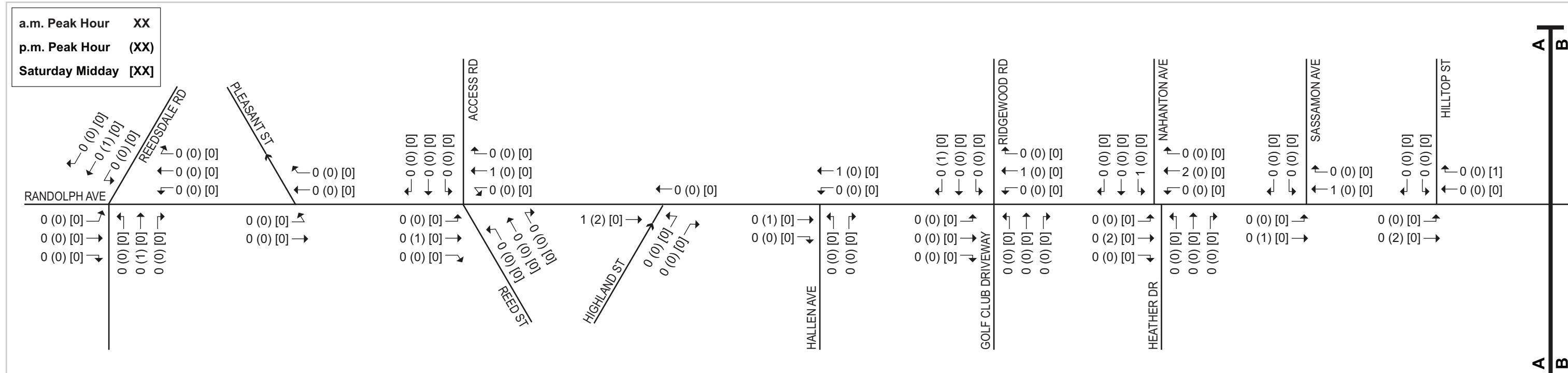


Appendix C. Existing (2023) Condition Pedestrian Volumes, Weekday a.m. and p.m. Peak Hours





Appendix C. Existing (2023) Condition Bicycle Volumes, Weekday a.m. and p.m. Peak Hours





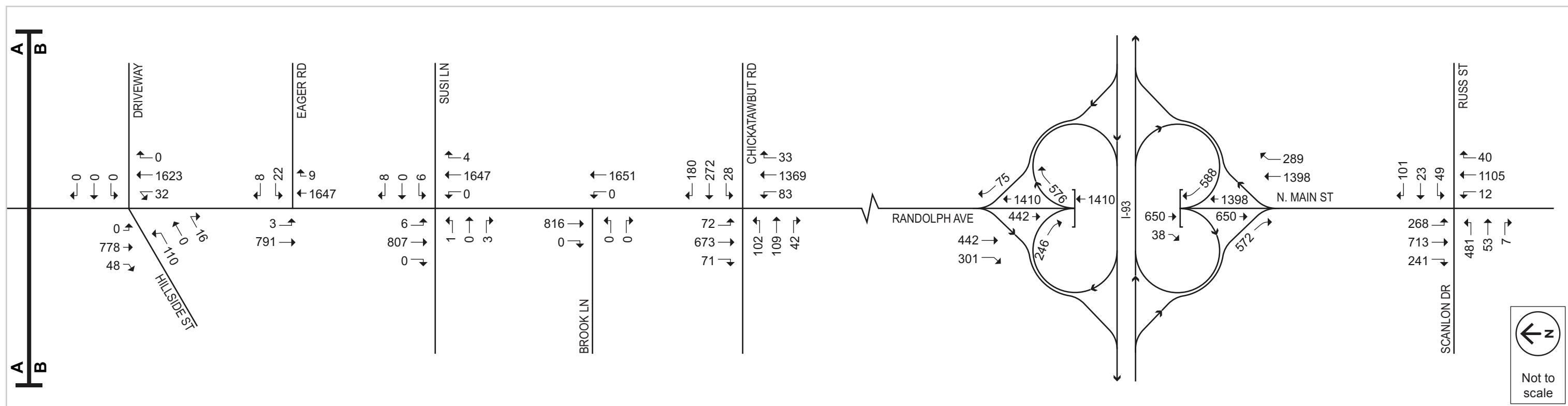
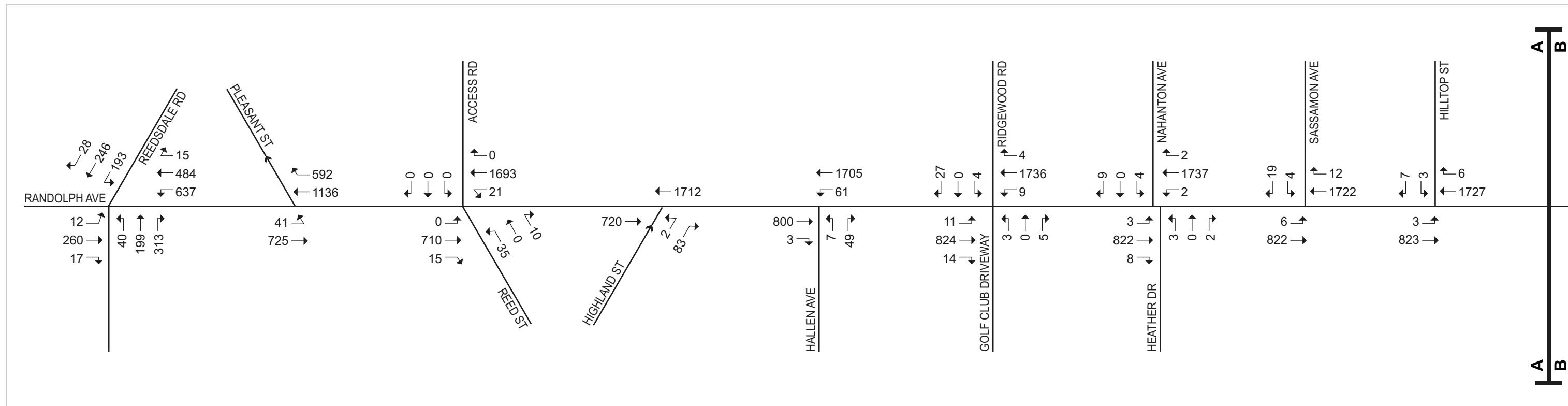
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Future (2034) a.m. and p.m. Vehicle Volumes

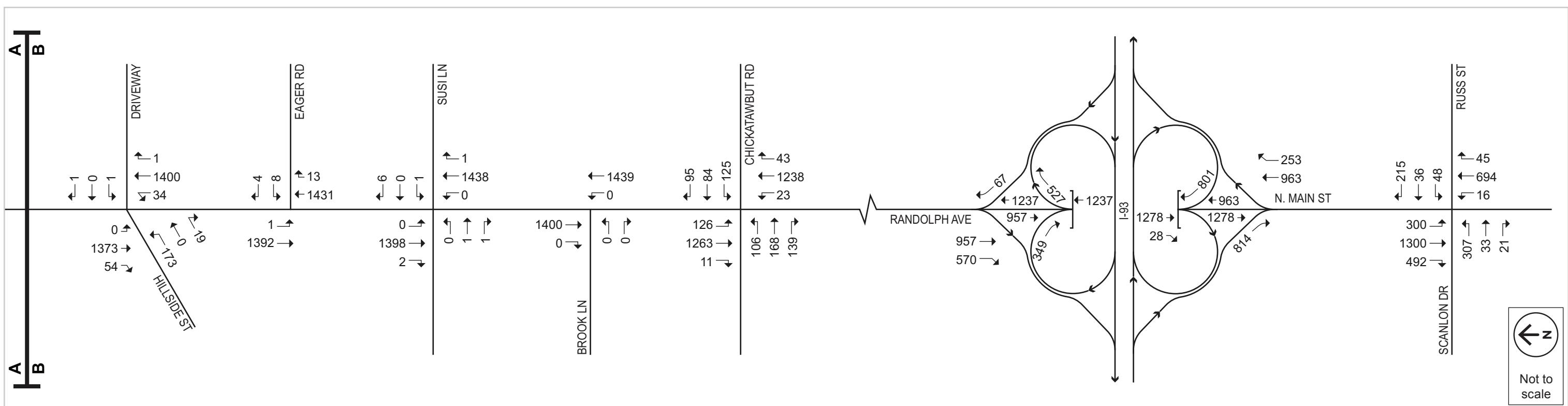
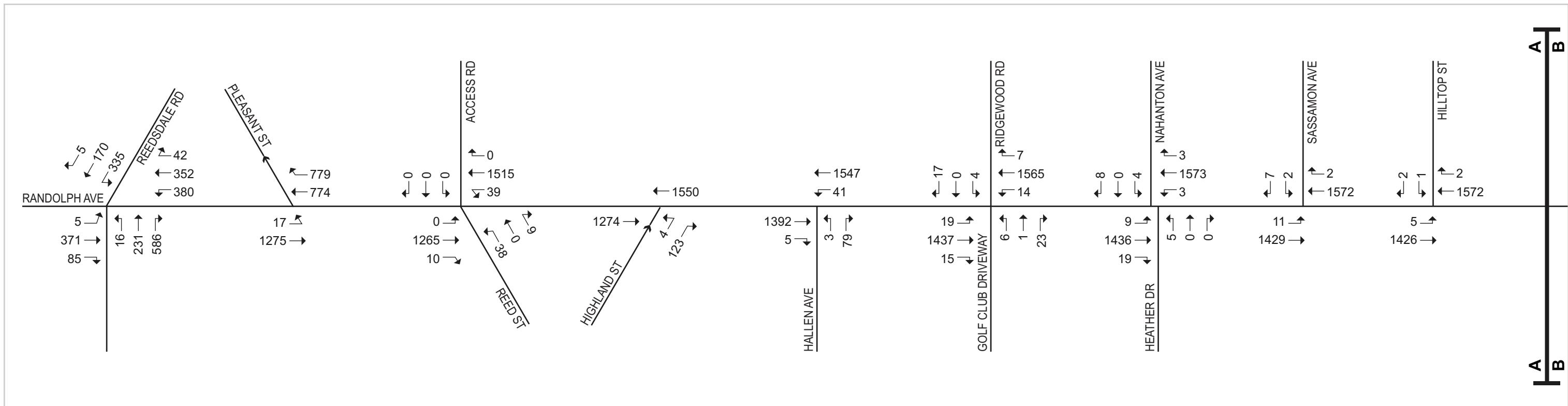


Appendix C. *Future (2034) Condition Vehicle Volumes, Weekday a.m. Peak Hour*





Appendix C. Future (2034) Condition Vehicle Volumes, Weekday p.m. Peak Hour





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VISSIM Model Calibration Notes



VISSIM PARAMETER CALIBRATIONS

Parameter	Required Calibration
	Existing and No-build Models
Driver Behavior	<ul style="list-style-type: none">■ Created a duplicate Urban Behavior where the following things changed:<ul style="list-style-type: none">– Changed Time before Diffusion from the default 60 seconds (sec) to 120 sec;– Checked on Advanced Merging;– Checked on Cooperative Lane Change;■ Created an aggressive merging behavior for links and connectors on Route 28 Northbound (NB) at and north of the I-93 Southbound (SB) off-ramp to Route 28 NB.
Connector Lane Change	<p>Changed lane change distance and emergency stop distance as described below:</p> <ul style="list-style-type: none">■ Route 28 at Chickatawbut Rd:<ul style="list-style-type: none">– SB Left Emergency Stop distance from the default 16.4 ft to 50 ft;– SB Left Lane change distance from the default 656.2 ft to 700 ft;■ Rte 28 at hillside<ul style="list-style-type: none">– NB Left Emergency stop distance to 100 ft;– NB Left Lane change distance to 1000 ft;■ Rte 28 at Reedsdale<ul style="list-style-type: none">– NB Left, Thru, and Right Emergency stop distance to 50 ft;– NB Left, Thru, and Right Lane change distance to 1000 ft;– Eastbound (EB) Thru Emergency stop distance to 50 ft;– Westbound (WB) Left Emergency stop distance to 50 ft;
Routing Decision	Placed Routing Decision point for Route 28 SB at Chickatawbut Road just south of Susi Lane, to achieve field-like conditions of travel and queueing.
Desired Speed Decision	<ul style="list-style-type: none">■ Rte 28 at Pleasant St, South of Reedsdale Rd:<ul style="list-style-type: none">– Introduced a slower speed decision that starts at 900 sec to create the backup seen in the a.m. peak hour field observations;– Adjusted that slower speed decision from 3-8mph to 4-10mph to not cause a longer NB queue than observed (observations showed it didn't go past Highland St, 3-8mph had it going past Hallen Ave);■ Route 28 NB, North of I-93 SB Off-ramp:<ul style="list-style-type: none">– Added two desired speed decisions on Rte 28 NB, one right after the merge with I-93 SB off-ramp to slow them down, and in the narrow single



Parameter	Required Calibration
	<p>lane section to get vehicles back up to the speeds experienced out in the field;</p> <ul style="list-style-type: none"> ■ Chickatawbut Rd WB – while measured 50%-ile speed was 18 miles per hour (mph), the average speed in the model was adjusted to 19.5 mph, as vehicles in the model were going too slow under uncongested conditions.
Conflict Areas	<ul style="list-style-type: none"> ■ I-93 NB Off-Ramp to Rte 28 NB <ul style="list-style-type: none"> – Changed the Merge Conflict area front and rear gap from 0.5 to 3 – Changed the VisibLink2 value from 328.1 to 550 ■ Changed I-93 SB off-ramp merge conflict area with Rte 28 NB parameters: <ul style="list-style-type: none"> – Front and Rear gap to 0.2; – Safety Distance to 1.0; ■ Changed the merge area to 3 lanes to have it act like it does today. ■ Route 28 at Chickatawbut Rd: <ul style="list-style-type: none"> – For EB Left and WB Left conflicts between them and the conflicting throughs, used a Priority rule instead of conflict area, with 1 sec Min Gap, to better match model operations with field observations.
Special Setups	<ul style="list-style-type: none"> ■ Field observations at Route 28 and Chickatawbut Rd found that the majority of thru vehicles used the outside lane to continue thru the intersection, to avoid the vehicles stopping to make a left-turn to Chickatawbut Rd WB. This was modeled by drawing a short connector in the Route 28 NB link, and routing 70% of the a.m. peak vehicles thru it, and 60% of the p.m. peak vehicles, to match observations.
Alternative 1 thru 3 Models	
General	<p>Almost all the modifications mentioned above remained for the alternatives, except for:</p> <ul style="list-style-type: none"> ■ The special connector for Route 28 NB thru at Chickatawbut Rd, as that intersection will be a roundabout in the future; ■ The priority rules for the EB and WB lefts at Route 28 NB and Chickatawbut Rd; and ■ The two desired speed decisions on Route 28 NB, north of the I-93 SB off-ramp and south of Chickatawbut Rd.



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VISSIM Roundabout Capacity Calibration Notes



TECHNICAL MEMORANDUM
Milton – Route 28 Corridor Road Diet Feasibility Study
February 2025

The tables that follow show the data and formulas used to determine the appropriate driver behavior and gap acceptance for each leg of the Route 28 at Chickatawbut Road roundabout for the VISSIM model roundabout capacity to match the calculated roundabout capacity, using the HCM 7 formulas mentioned below.

It should be noted that for some legs and circulating volume variations the 10% capacity threshold mentioned in the MassDOT guide for roundabout calibration in VISSIM could not be achieved, however, the capacity is very close to 10% and much better than what the default VISSIM behavior and gap acceptance was providing that those instances of not meeting the 10% capacity threshold were deemed acceptable and the set of behavior and gap acceptance parameter values were used for the calibrated roundabout in all VISSIM models for this study.

Route 28 NB Approach Capacity	Counts ¹	Original VISSIM ²	Alt #1 ³	Alt #2 ⁴	Alt #3 ⁵
HCM 6 Formula ^a	1098	1098	1081	1086	1080
Default VISSIM Behavior ^b	-	708	619	560	526
% Difference	-	35%	43%	48%	51%
Behavior Adjust #1 ^c	-	723	645	584	552
% Difference	-	34%	40%	46%	49%
Behavior Adjust #2 ^d	-	773	662	616	562
% Difference	-	30%	39%	43%	48%
Behavior Adjust #3 ^e	-	814	698	646	587
% Difference	-	26%	35%	41%	46%
Behavior+Conflict Adjust #3 ^f	-	965	902	780	694
% Difference	-	12%	17%	28%	36%
Behavior+Conflict Adjust #2 ^g	-	1101	994	896	794
% Difference	-	0%	8%	17%	27%
Behavior+Conflict Adjust #3 ^h	-	1106	1079	996	899
% Difference	-	-1%	0%	8%	17%
Behavior+Conflict Adjust #3 ⁱ	-	1054	1017	1050	1025
% Difference	-	4%	6%	3%	5%

TABLE 1 - Circulating Volume Variation						
	Orig (vol)	Orig (%)	Mod #1(vol)	Mod #1	Mod #2(vol)	Mod #2
Rte 28 NB L	83	6%	119	8%	119	8%
Rte 28 NB T	1369	92%	1337	90%	1307	88%
Rte 28 NB R	33	2%	30	2%	59	4%
Chicka WB L	28	6%	38	8%	38	8%
Chicka WB T	272	57%	264	55%	254	53%
Chicka WB R	180	38%	182	38%	192	40%
Rte 28 SB L	72	9%	90	11%	90	11%
Rte 28 SB T	673	82%	653	80%	636	78%
Rte 28 SB R	71	9%	73	9%	90	11%
Chicka EB L	102	40%	106	42%	106	42%
Chicka EB T	109	43%	104	41%	99	39%
Chicka EB R	42	17%	43	17%	48	19%

TABLE 2 - HCM 7 formulas for Approach capacity						
Two-Lane Entry Conflicted by One Circulating Lane						
Eq 22-2	$c_{e,pcc} = 1,420e^{(-0.91 \times 10^{-3})v_{e,pcc}}$					
One-Lane Entry Conflicted by Two Circulating Lanes	$c_{e,pcc} = 1,420e^{(-0.85 \times 10^{-3})v_{e,pcc}}$					
Eq 22-3	$c_{e,pcc} = 1,420e^{(-0.85 \times 10^{-3})v_{e,pcc}}$					
Where	$v_{e,pcc}$ Capacity of each entry lane in passenger car equivalent/hour $v_{c,pcc}$ Conflicting volume in circulating lane in passenger car equivalent/hour					

TABLE 3 - VISSIM Driver Behavior settings by Alternative							
	Avg. Standstill	Additive Part of Safety	Multiplicative Part of Safety	Safety			
	Dist	Distance	Distance	Anticipate Routing	Distance	Front Gap	Rear Gap
Default VISSIM	6.56	2	3	0%	1.5	0.5	0.5
Behavior Adjust #1	3.28	1	2	0%	1.5	0.5	0.5
Behavior Adjust #2	1.64	0.5	1	0%	1.5	0.5	0.5
Behavior Adjust #3	0.82	0.15	0.15	0%	1.5	0.5	0.5
Behavior+Conflict Adjust #1	0.82	0.15	0.15	100%	1	0.3	0.3
Behavior+Conflict Adjust #2	0.82	0.15	0.15	100%	0.5	0.1	0.1
Behavior+Conflict Adjust #3	0.82	0.15	0.15	100%	0.2	0.1	0.1
Behavior+Conflict Adjust #3-A	0.82	0.15	0.15	100%	0.2	0.1	0.1
				100%	0.1	0.1	0.1
				0%	1.8	1	1
							Rte 28 NB
							Chickatawbut WB & EB
							Rte 28 SB

TABLE 4 - Volumes from Counts						
	AM					
Route 28 NB Entering	1485					
RBT EB Circulating	283					
Chicka WB Entering	480					
RBT NB Circulating	1554					
Route 28 SB Entering	816					
RBT WB Circulating	383					
Chicka EB Entering	253					
RBT SB Circulating	773					

Route 28 SB Approach Capacity	Counts ¹	Original VISSIM ²	Alt #1 ³	Alt #2 ⁴	Alt #3 ⁵
HCM 6 Formula ^a	1002	1002	968	976	967
Default VISSIM Behavior ^b	-	894	832	787	747
% Difference	-	11%	14%	19%	23%
Behavior Adjust #1 ^c	-	948	892	860	818
% Difference	-	5%	8%	12%	15%
Behavior Adjust #2 ^d	-	996	949	909	858
% Difference	-	1%	2%	7%	11%
Behavior Adjust #3 ^e	-	1009	973	957	917
% Difference	-	-1%	-1%	2%	5%
Behavior+Conflict Adjust #1 ^f	-	956	1087	1038	957
% Difference	-	4%	-12%	-6%	1%
Behavior+Conflict Adjust #2 ^g	-	1103	1113	1088	1003
% Difference	-	-10%	-15%	-11%	-4%
Behavior+Conflict Adjust #3 ^h	-	1426	1150	1115	1013
% Difference	-	-42%	-19%	-14%	-5%
Behavior+Conflict Adjust #3 ⁱ	-	903	863	891	885
% Difference	-	10%	11%	9%	9%

Chickatawbut EB Approach Capacity	Counts ¹	Original VISSIM ²	Alt #1 ³	Alt #2 ⁴	Alt #3 ⁵
HCM 6 Formula ^a	736	736	731	741	743
Default VISSIM Behavior ^b	-	234	262	292	315
% Difference	-	68%	64%	61%	58%
Behavior Adjust #1 ^c	-	243	257	289	302
% Difference	-	67%	65%	61%	59%
Behavior Adjust #2 ^d	-	239	264	280	303
% Difference	-	68%	64%	62%	59%
Behavior Adjust #3 ^e	-	227	260	272	293
% Difference	-	69%	64%	63%	61%
Behavior+Conflict Adjust #1 ^f	-	120	276	395	447
% Difference	-	84%	62%	47%	40%
Behavior+Conflict Adjust #2 ^g	-	148	293	426	505
% Difference	-	80%	60%	43%	32%
Behavior+Conflict Adjust #3 ^h	-	269	272	431	527
% Difference	-	63%	63%	42%	29%
Behavior+Conflict Adjust #3 ⁱ	-	670	651	656	674
% Difference	-	10%	6%	10%	5%

1 - Using the counts and no modifications (see Table 4)
 2 - Using Default VISSIM settings
 3 - See Table 1 for volume changes
 4 - See Table 1 for volume changes
 5 - See Table 1 for volume changes

a - see HCM Formula in Table 2

b thru h - See Table 3

Route 28 NB Approach Capacity	Counts ^a	Original VISSIM ^b	Mod #1 ^c	Mod #2 ^d	Mod #3 ^e
HCM 6 Formula ^a	987	987	960	982	973
Default VISSIM Behavior ^b	-	846	635	611	547
% Difference	-	14%	34%	38%	44%
Behavior Adjust #1 ^c	-	857	658	645	574
% Difference	-	13%	31%	34%	41%
Behavior Adjust #2 ^d	-	868	682	670	601
% Difference	-	12%	29%	32%	38%
Behavior Adjust #3 ^e	-	899	718	701	606
% Difference	-	9%	25%	29%	38%
Behavior+Conflict Adjust #1 ^c	-	1102	932	792	706
% Difference	-	12%	3%	19%	27%
Behavior+Conflict Adjust #2 ^d	-	1142	1022	909	826
% Difference	-	16%	6%	7%	15%
Behavior+Conflict Adjust #3 ^e	-	1182	1106	1009	922
% Difference	-	20%	15%	3%	5%
Behavior+Conflict Adjust #3 ^e	-	981	945	951	937
% Difference	-	1%	2%	3%	4%

Route 28 SB Approach Capacity	Counts ^a	Original VISSIM ^b	Alt #1 ^c	Alt #2 ^d	Alt #3 ^e
HCM 6 Formula ^a	1150	1150	1119	1125	1115
Default VISSIM Behavior ^b	-	908	843	714	670
% Difference	-	21%	25%	37%	40%
Behavior Adjust #1 ^c	-	942	903	761	710
% Difference	-	18%	19%	32%	36%
Behavior Adjust #2 ^d	-	1003	949	810	753
% Difference	-	13%	15%	28%	32%
Behavior Adjust #3 ^e	-	1047	998	838	922
% Difference	-	9%	11%	26%	17%
Behavior+Conflict Adjust #1 ^c	-	1465	1108	1056	952
% Difference	-	27%	1%	6%	15%
Behavior+Conflict Adjust #2 ^d	-	1456	1131	1103	997
% Difference	-	27%	1%	2%	11%
Behavior+Conflict Adjust #3 ^e	-	1461	1151	1136	1029
% Difference	-	27%	3%	-1%	8%
Behavior+Conflict Adjust #3 ^e	-	1057	985	989	962
% Difference	-	8%	12%	12%	14%

Chickatawbut EB Approach Capacity	Counts ^a	Original VISSIM ^b	Alt #1 ^c	Alt #2 ^d	Alt #3 ^e
HCM 6 Formula ^a	394	394	398	409	416
Default VISSIM Behavior ^b	-	163	269	470	504
% Difference	-	59%	32%	-15%	-21%
Behavior Adjust #1 ^c	-	182	268	479	512
% Difference	-	54%	33%	-17%	-23%
Behavior Adjust #2 ^d	-	189	270	482	511
% Difference	-	52%	32%	-18%	-23%
Behavior Adjust #3 ^e	-	186	266	476	290
% Difference	-	53%	33%	-16%	30%
Behavior+Conflict Adjust #1 ^c	-	133	267	402	467
% Difference	-	66%	33%	2%	-12%
Behavior+Conflict Adjust #2 ^d	-	145	293	435	515
% Difference	-	63%	26%	-6%	-24%
Behavior+Conflict Adjust #3 ^e	-	145	269	431	523
% Difference	-	63%	32%	-5%	-26%
Behavior+Conflict Adjust #3 ^e	-	361	398	420	448
% Difference	-	8%	0%	-3%	-8%

Chickatawbut WB Approach Capacity	Counts ^a	Original VISSIM ^b	Alt #1 ^c	Alt #2 ^d	Alt #3 ^e
HCM 6 Formula ^a	447	447	442	458	461
Default VISSIM Behavior ^b	-	218	306	435	504
% Difference	-	51%	31%	5%	-9%
Behavior Adjust #1 ^c	-	232	312	444	514
% Difference	-	48%	29%	3%	-11%
Behavior Adjust #2 ^d	-	244	318	446	530
% Difference	-	45%	28%	3%	-15%
Behavior Adjust #3 ^e	-	244	315	454	359
% Difference	-	45%	29%	1%	22%
Behavior+Conflict Adjust #1 ^c	-	309	397	526	606
% Difference	-	31%	10%	-15%	-31%
Behavior+Conflict Adjust #2 ^d	-	328	418	530	615
% Difference	-	27%	5%	-16%	-33%
Behavior+Conflict Adjust #3 ^e	-	318	384	512	592
% Difference	-	29%	13%	-12%	-28%
Behavior+Conflict Adjust #3 ^e	-	417	435	453	473
% Difference	-	7%	2%	1%	-3%

1 - Using the counts and no modifications (see Table 4)

a - see HCM Formula in Table 2

2 - Using Default VISSIM settings

b thru h - See Table 3

3 - See Table 1 for volume changes

4 - See Table 1 for volume changes

5 - See Table 1 for volume changes

TABLE 1 - Circulating Volume Variation

Orig (vol)	Orig (%)	Mod #1 (vol)	Mod #1	Mod #2 (vol)	Mod #2	Mod #3 (vol)	Mod #3
Rte 28 NB L	23	52	4%	52	4%	65	5%
Rte 28 NB T	1231	1206	93%	1180	91%	1154	89%
Rte 28 NB R	43	39	3%	65	5%	78	6%
Chick WB L	125	119	39%	112	37%	106	35%
Chick WB T	84	91	30%	91	30%	94	31%
Chick WB R	95	94	31%	100	33%	103	34%
Rte 28 SB L	126	153	11%	153	11%	167	12%
Rte 28 SB T	1256	1226	88%	1198	86%	1170	84%
Rte 28 SB R	11	14	1%	42	3%	56	4%
Chick EB L	106	116	28%	99	24%	103	25%
Chick EB T	168	161	39%	153	37%	145	35%
Chick EB R	139	140	34%	149	36%	153	37%

TABLE 2 - HCM 7 formulas for Approach capacity

Two-Lane Entry Conflicted by One Circulating Lane

Eq 22-2 $C_{e,pce} = 1.420e^{(-0.93 \times 10^{-3})V_{e,pce}}$

One-Lane Entry Conflicted by Two Circulating Lanes

Eq 22-3 $C_{e,pce} = 1.420e^{(-0.85 \times 10^{-3})V_{e,pce}}$

Where $C_{e,pce}$ Capacity of each entry lane in passenger car equivalent/hour
 $V_{e,pce}$ Conflicting volume in circulating lane in passenger car equivalent/hour

TABLE 3 - VISSIM Driver Behavior settings by Alternative

	Avg. Standstill Distance	Additive Part of Safety Distance	Multiplicative Part of Safety Distance	Safety Anticipate Routing	Safety Distance	Front Gap	Rear Gap
Default VISSIM	6.56	2	3	0%	1.5	0.5	0.5
Behavior Adjust #1	3.28	1	2	0%	1.5	0.5	0.5
Behavior Adjust #2	1.64	0.5	1	0%	1.5	0.5	0.5
Behavior Adjust #3	0.82	0.15	0.15	0%	1.5	0.5	0.5
Behavior+Conflict Adjust #1	0.82	0.15	0.15	100%	1	0.3	0.3
Behavior+Conflict Adjust #2	0.82	0.15	0.15	100%	0.5	0.1	0.1
Behavior+Conflict Adjust #3	0.82	0.15	0.15	100%	0.2	0.1	0.1
Behavior+Conflict Adjust #3-A	1	0.15	0.23	100%	1.4	0.5	0.5
				100%	0.4	0.2	0.2
				0%	0.9	0.5	0.5
				100%	0.1	0.1	0.1
							Chickatawbut WB
							Rte 28 SB
							Chickatawbut EB

TABLE 4 - Volumes from Counts

	PM
Route 28 NB Entering	1297
RBT EB Circulating	400
Chick WB Entering	304
RBT NB Circulating	1360
Route 28 SB Entering	1393
RBT WB Circulating	232
Chick EB Entering	413
RBT SB Circulating	1507



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Existing Travel Time and Vehicle Hours of Delay



**TRAVEL TIMES AND VEHICLE HOURS OF DELAY – EXISTING (2023)
 CONDITIONS**

Segment	Volume (vehicles)	Travel Time (min)	Vehicle- Hours Traveled
a.m. peak Hour			
Route 28 Northbound – North of Scanlon Drive to South of Reedsdale Road	346	16.7	96.1
Route 28 Northbound – North of Scanlon Road to North of Chickatawbut Road	655	9.4	102.4
Route 28 Northbound –North of Chickatawbut Road to South of Reedsdale Road	757	7.6	95.7
Route 28 Southbound – South of Reedsdale Road to North of Scanlon Drive	273	6.3	28.5
Route 28 Southbound – South of Reedsdale Road to North of Chickatawbut Road	400	2.7	18.2
Route 28 Southbound – North of Chickatawbut Road to North of Scanlon Drive	513	3.5	29.8
p.m. peak Hour			
Route 28 Northbound – North of Scanlon Drive to South of Reedsdale Road	162	10.4	27.9
Route 28 Northbound – North of Scanlon Road to North of Chickatawbut Road	360	7.6	45.6
Route 28 Northbound –North of Chickatawbut Road to South of Reedsdale Road	570	3.0	28.4
Route 28 Southbound – South of Reedsdale Road to North of Scanlon Drive	545	8.6	78.5
Route 28 Southbound – South of Reedsdale Road to North of Chickatawbut Road	827	3.5	48.3
Route 28 Southbound – North of Chickatawbut Road to North of Scanlon Drive	913	5.3	80.7



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No-build and Alternatives Travel Time and Vehicle Hours of Delay



TRAVEL TIMES AND VEHICLE HOURS OF DELAY COMPARISON – NO-BUILD (2033) CONDITIONS VS. ALTERNATIVES

Segment	Volume (veh)	Travel Time (min)	Vehicle-Hours Traveled	Vehicle-Hours of delay	Travel Time (min)	Vehicle-Hours Traveled	Vehicle-Hours of delay	Travel Time (min)	Vehicle-Hours Traveled	Vehicle-Hours of delay	Travel Time (min)	Vehicle-Hours Traveled	Vehicle-Hours of delay	Travel Time (min)	Vehicle-Hours Traveled	Vehicle-Hours of delay	Travel Time (min)	Vehicle-Hours Traveled	Vehicle-Hours of delay
a.m. peak Hour																			
		No-build			No-build w/RBT			No-build w/RBT+MET			Alternative 1			Alternative 2			Alternative 3		
Route 28 Northbound – North of Scanlon Dr to South of Reedsdale Rd	359	17.1	102.5	6.4	15.5	92.6	-9.9	16.1	96.4	-6.0	12.7	75.7	-26.7	15.1	90.0	-12.5	7.7	46.3	-56.1
Route 28 Northbound – North of Scanlon Rd to North of Chickatawbut Rd	662	9.7	107.2	4.8	5.8	63.6	-43.6	5.9	65.1	-42.1	6.2	68.1	-39.1	10.4	114.5	7.3	2.9	31.7	-75.5
Route 28 Northbound – North of Chickatawbut Rd to South of Reedsdale Rd	765	7.8	99.1	3.4	10.0	127.1	28.0	10.5	133.4	34.3	7.1	91.1	-8.0	5.4	69.2	-29.8	4.9	62.0	-37.1
Route 28 Southbound – South of Reedsdale Rd to North of Scanlon Dr	282	6.3	29.7	29.7	5.8	27.5	-2.2	6.0	28.2	-1.5	5.9	28.0	-1.7	5.7	26.7	-3.0	6.4	30.1	0.4
Route 28 Southbound – South of Reedsdale Rd to North of Chickatawbut Rd	410	2.8	19.0	-9.5	2.7	18.6	-0.4	2.7	18.6	-0.4	2.7	18.6	-0.4	2.7	18.5	-0.5	2.7	18.4	-0.6
Route 28 Southbound – North of Chickatawbut Rd to North of Scanlon Dr	517	3.5	30.2	12.0	3.1	26.4	-3.8	3.2	27.8	-2.4	3.2	27.5	-2.7	2.9	25.4	-4.8	3.6	31.2	1.0
p.m. peak Hour																			
Route 28 Northbound – North of Scanlon Dr to South of Reedsdale Rd	163	11.9	32.3	4.4	6.8	18.6	-13.7	6.9	18.7	-13.6	10.5	28.4	-3.9	13.1	35.5	3.2	6.5	17.6	-14.7
Route 28 Northbound – North of Scanlon Rd to North of Chickatawbut Rd	361	9.1	54.9	9.3	3.5	21.1	-33.8	3.5	21.3	-33.6	4.6	27.6	-27.3	8.9	53.4	-1.5	2.8	16.8	-38.1
Route 28 Northbound – North of Chickatawbut Rd to South of Reedsdale Rd	556	3.0	28.1	-0.3	3.2	29.8	1.7	3.2	29.9	1.8	6.3	58.3	30.2	4.8	44.1	16.0	3.6	33.5	5.4
Route 28 Southbound – South of Reedsdale Rd to North of Scanlon Dr	559	8.5	79.7	1.2	6.7	62.7	-16.9	7.0	65.6	-14.0	6.1	57.0	-22.7	6.1	56.5	-23.1	8.9	82.7	3.0
Route 28 Southbound – South of Reedsdale Rd to North of Chickatawbut Rd	845	3.5	49.7	1.4	3.3	46.6	-3.1	3.3	46.6	-3.1	2.9	40.3	-9.4	3.0	41.7	-8.0	2.9	41.3	-8.4
Route 28 Southbound – North of Chickatawbut Rd to North of Scanlon Dr	928	5.2	80.6	-0.1	3.4	52.9	-27.7	3.7	57.8	-22.7	3.3	50.3	-30.2	3.1	47.9	-32.7	6.1	94.9	14.4

(1) – No-build with Roundabout at Route 28 and Chickatawbut Rd, (2) – No-build with Roundabout at Route 28 and Chickatawbut Rd and Metering signals on Route 28 legs



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Existing Average Speeds



ROUTE 28 NORTHBOUND AVERAGE SPEEDS – EXISTING (2023) A.M. AND P.M. PEAKS

Location on Route 28	Northbound Average Speed (mph)	Southbound Average Speed (mph)
a.m. peak Hour		
South of Reedsdale Road	44.1	40.0
South of Reed Street/Access Road	29.7	22.9
South of Hillside Street	25.9	34.9
South of Chickatawbut Road	43.9	22.7
Between the I-93 inner loop ramps	36.6	37.5
p.m. peak Hour		
South of Reedsdale Road	37.9	44.1
South of Reed Street/Access Road	40.7	43.3
South of Hillside Street	35.9	35.5
South of Chickatawbut Road	27.1	29.5
Between the I-93 inner loop ramps	35.7	35.0



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No-build and Alternatives Average Speeds



NO-BUILD AND ALTERNATIVES AVERAGE VEHICLE SPEED

Location on Route 28	Northbound Average Speed (mph)	Southbound Average Speed (mph)	Northbound Average Speed (mph)	Southbound Average Speed (mph)	Northbound Average Speed (mph)	Southbound Average Speed (mph)	Northbound Average Speed (mph)	Southbound Average Speed (mph)	Northbound Average Speed (mph)	Southbound Average Speed (mph)	Northbound Average Speed (mph)	Southbound Average Speed (mph)	
	No-Build		No-Build w/RBT ⁽¹⁾			No-Build w/RBT+MET ⁽²⁾		Northbound Road Diet		Northbound Road Diet v2		Southbound Road Diet	
a.m. peak Hour													
South of Reedsdale Road	30.3	43.9	29.9	44.0	29.5	43.8	35.0	35.8	34.8	38.1	30.5	34.1	
South of Reed Street/Access Road	24.6	44.0	21.0	44.0	21.1	43.9	33.2	44.2	32.7	44.2	35.4	42.1	
South of Hillside Street	36.6	39.1	33.2	39.2	32.5	39.1	30.1	40.0	30.0	39.9	36.2	38.2	
South of Chickatawbut Road	23.1	34.9	34.0	34.9	34.5	35.6	30.0	35.0	25.3	35.0	37.4	35.4	
Between the I-93 inner loop ramps	21.2	37.3	26.9	37.4	25.7	37.4	34.8	37.5	20.2	37.3	37.6	37.4	
p.m. peak Hour													
South of Reedsdale Road	38.0	44.0	37.1	44.0	37.1	44.0	38.2	42.0	38.2	42.3	36.8	31.2	
South of Reed Street/Access Road	40.6	43.3	40.2	43.3	40.1	43.2	35.7	44.0	35.4	43.9	38.0	29.1	
South of Hillside Street	35.9	35.4	35.5	38.5	35.1	38.3	30.3	38.8	29.8	38.7	34.7	37.7	
South of Chickatawbut Road	26.6	29.4	30.2	31.0	34.6	32.2	31.3	33.7	23.3	34.1	37.5	33.4	
Between the I-93 inner loop ramps	29.7	35.0	38.4	36.8	38.5	36.8	38.4	36.9	30.4	36.9	38.6	36.9	

(1) – No-build with Roundabout at Route 28 and Chickatawbut Rd, (2) – No-Build with Roundabout at Route 28 and Chickatawbut Rd and Metering on Route 28 legs



HOWARD STEIN HUDSON

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No-build and Alternatives Driveway Delays



DRIVEWAY DELAY – NO-BUILD VS. ALTERNATIVES

Location on Route 28	No-build Delay (sec)	No-build w/RBT Delay (sec)	No-build w/RBT+MET Delay (sec)	Alternative 1 Delay (sec)	Alternative 2 Delay (sec)	Alternative 3 Delay (sec)
a.m. peak Hour						
Between Eager Rd and Susi Lane						
Driveway #1	6.4	6.3	12.6	378.5	287.4	2.8
Driveway #2	7.6	11.2	9.2	394.6	310.7	2.2
Driveway #3	14.1	4.5	5.4	154.9	222.2	1.6
Driveway #4	6.9	5.5	9.1	133.0	341.3	2.3
Driveway #5	5.9	7.3	12.3	400.7	357.1	1.1
Between Hillside St and Eager Rd						
Driveway #6	10.8	1.5	16.4	134.9	57.5	7.6
Driveway #7	7.0	7.1	11.8	119.0	201.0	4.9
Driveway #8	8.0	9.6	13.7	130.6	120.0	5.5
Driveway #9	8.3	8.3	11.5	144.9	160.9	12.6
p.m. peak Hour						
Between Eager Rd and Susi Lane						
Driveway #1	166.4	13.3	20.5	532.6	290.1	1.3
Driveway #2	142.1	8.4	6.5	26.0	371.7	2.6
Driveway #3	155.2	8.2	7.5	18.3	398.0	2.2
Driveway #4	274.9	8.6	8.8	11.2	487.4	1.9
Driveway #5	26.9	5.9	7.9	3.4	139.0	1.3
Between Hillside St and Eager Rd						
Driveway #6	72.7	11.8	6.1	214.8	286.3	2.1
Driveway #7	10.5	7.4	10.4	334.4	427.1	2.8
Driveway #8	8.0	11.3	13.1	183.9	363.6	30.0
Driveway #9	8.3	17.4	14.8	213.3	81.1	31.0

(1) – No-build with Roundabout at Route 28 and Chickatawbut Rd,

(2) – No-build with Roundabout at Route 28 and Chickatawbut Rd and Metering on Route 28 legs



HOWARD STEIN HUDSON

Engineers + Planners

Existing Capacity Analysis



EXISTING (2023) CONDITIONS CAPACITY ANALYSIS – SIGNALIZED INTERSECTIONS

Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
a.m. peak Hour				
Route 28 at Reedsdale Rd	F	81.8	-	-
Route 28 EB left/thru	F	99.3	184	554
Route 28 EB right	C	28.2	184	554
Reedsdale WB left/thru thru/right	E	61.2	140	478
Route 28 NB left left/thru/right	F	112.0	506	1184
Route 28 SB left/thru/right	E	65.6	145	462
Route 28 at Reed Street/Access Road	D	41.9	-	-
Reed EB left/thru/right	D	45.8	17	178
Access WB left/thru/right	A	0.0	0	0
Route 28 NB left/thru thru/right	E	61.1	441	906
Route 28 SB left/thru thru/right	A	3.7	9	195
Route 28 at Hillside Street	B	12.3	-	-
Hillside EB left/thru/right	D	38.3	33	199
Driveway WB left/thru/right	A	0.0	0	0
Route 28 NB left/thru thru/right	A	8.4	50	272
Route 28 SB left/thru thru/right	B	15.1	52	326
Route 28 at Chickatawbut Road	F	117.2	-	-
Chickatawbut EB left/thru/right	D	49.9	85	362
Chickatawbut WB left/thru/right	F	99.5	436	850
Route 28 NB left/thru thru/right	F	188.1	4438	5348
Route 28 SB left/thru thru/right	D	42.4	158	489
Route 28 at Scanlon Drive/Russ Street	E	68.3	-	-
Scanlon EB left	D	43.9	101	433
Scanlon EB left/thru/right	D	43.9	101	433
Russ WB left	D	42.9	46	272
Russ WB thru/right	D	45.0	46	272
Route 28 NB left	F	98.9	648	853



Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
Route 28 NB thru thru/right	F	124.5	648	853
Route 28 SB left	F	83.0	174	616
Route 28 SB hru thru/right	B	17.7	174	616
p.m. peak Hour				
Route 28 at Reedsdale Rd	E	67.7	-	-
Route 28 EB left/thru	E	76.1	200	584
Route 28 EB right	D	33.4	200	584
Reedsdale WB left/thru thru/right	F	152.2	444	554
Route 28 NB left left/thru/right	D	43.9	144	567
Route 28 SB left/thru/right	E	64.5	230	466
Route 28 at Reed Street/Access Road	A	5.4	-	-
Reed EB left/thru/right	D	40.3	13	137
Access WB left/thru/right	A	0.0	0	0
Route 28 NB left/thru thru/right	A	5.4	29	456
Route 28 SB left/thru thru/right	A	3.9	16	299
Route 28 at Hillside Street	B	17.4	-	-
Hillside EB left/thru/right	D	41.1	53	200
Driveway WB left/thru/right	A	0.0	0	0
Route 28 NB left/thru thru/right	A	9.9	51	259
Route 28 SB left/thru thru/right	C	21.0	128	363
Route 28 at Chickatawbut Road	F	120.8	-	-
Chickatawbut EB left/thru/right	F	96.7	342	839
Chickatawbut WB left/thru/right	E	56.7	124	485
Route 28 NB left/thru thru/right	F	218.4	4407	5322
Route 28 SB left/thru thru/right	E	55.2	353	495
Route 28 at Scanlon Drive/Russ Street	C	28.0	-	-
Scanlon EB left	D	31.5	48	215
Scanlon EB left/thru/right	D	30.7	48	215
Russ WB left	D	47.2	47	394
Russ WB thru/right	D	44.3	47	394



TECHNICAL MEMORANDUM
Milton – Route 28 Corridor Road Diet Feasibility Study
February 2025

Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
Route 28 NB left	C	26.7	104	404
Route 28 NB thru thru/right	D	34.1	104	404
Route 28 SB left	D	42.6	210	747
Route 28 SB thru thru/right	C	22.7	210	747



EXISTING (2023) CONDITIONS CAPACITY ANALYSIS – UNSIGNALIZED INTERSECTIONS

Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
a.m. peak Hour				
Route 28 at Pleasant Street	D	51.9	-	-
Route 28 NB thru thru/right	E	78.2	726	1037
Route 28 SB left/thru thru/right	A	3.1	8	182
Route 28 at Highland Street	C	21.7	-	-
Highland EB left/right	A	2.0	1	79
Route 28 NB thru thru	D	33.2	240	693
Route 28 SB thru thru	A	0.8	0	58
Route 28 at Hallen Avenue	C	21.7	-	-
Hallen EB left/right	E	68.4	28	194
Route 28 NB left/thru thru	D	30.7	241	889
Route 28 SB thru thru/right	A	0.6	1	88
Route 28 at Ridgewood Road/Wollaston Golf Club	A	6.0	-	-
Wollaston Golf Club EB left/thru/right	A	3.4	0	33
Ridgewood WB left/thru/right	A	9.9	1	65
Route 28 NB left/thru thru/right	A	8.4	49	368
Route 28 SB left/thru thru/right	A	1.5	4	212
Route 28 at Nahanton Avenue	A	1.2	-	-
Nahanton WB left/right	A	5.4	0	74
Route 28 NB thru thru/right	A	1.4	21	205
Route 28 SB left/thru thru	A	0.9	1	144
Route 28 at Heather Drive	A	1.7	-	-
Heather EB left/right	B	16.6	0	29
Route 28 NB left/thru thru	A	2.6	18	203
Route 28 SB thru thru/right	A	0.1	1	146
Route 28 at Sassamon Avenue	A	3.4	-	-
Sassamon WB left/right	A	6.7	0	52



TECHNICAL MEMORANDUM
Milton – Route 28 Corridor Road Diet Feasibility Study
February 2025

Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
Route 28 NB thru thru/right	A	5.1	31	342
Route 28 SB left/thru thru	A	0.3	0	54
Route 28 at Hilltop Street	A	1.3	-	-
Hilltop WB left/right	B	14.0	2	109
Route 28 NB thru thru/right	A	1.5	9	329
Route 28 SB left/thru thru	A	0.9	0	88
Route 28 at Eager Road	A	0.5	-	-
Eager WB left/right	A	7.3	1	84
Route 28 NB thru thru/right	A	0.5	3	154
Route 28 SB left/thru thru	A	0.3	0	40
Route 28 at Susi Lane	A	0.6	-	-
Susi EB left/thru/right	A	2.4	0	29
Susi WB left/thru/right	A	6.4	1	52
Route 28 NB thru thru/right	A	0.5	3	190
Route 28 SB left/thru thru	A	0.6	4	144
Route 28 at Brook Lane	A	1.1	-	-
Brook EB left/right	A	0.0	0	0
Route 28 NB left/thru thru	A	0.4	0	0
Route 28 SB thru thru/right	A	2.3	6	232
Route 28 at I-93 SB Off-Ramp	F	171.5	-	-
I-93 SB Off-Ramp WB right	A	0.7	0	0
Route 28 NB thru thru	F	182.6	1228	1573
Route 28 at I-93 SB Off-Ramp	A	4.5	-	-
I-93 SB Off-Ramp EB right	A	0.4	0	70
Route 28 SB thru thru	A	6.9	0	0
Route 28 at I-93 NB Off-Ramp	D	35.5	-	-
I-93 NB Off-Ramp WB right	D	36.7	193	1007
Route 28 NB thru thru	D	31.7	58	165
Route 28 at I-93 NB Off-Ramp	A	1.3	-	-
I-93 NB Off-Ramp EB right	A	0.6	0	47



Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
Route 28 SB thru thru	A	2.1	7	148
p.m. peak hour				
Route 28 at Pleasant Street	A	5.0	-	-
Route 28 NB thru thru/right	A	8.4	63	574
Route 28 SB left/thru thru/right	A	1.2	2	135
Route 28 at Highland Street	A	1.0	-	-
Highland EB left/right	A	3.0	3	96
Route 28 NB thru thru	A	0.8	1	162
Route 28 SB thru thru	A	0.9	1	121
Route 28 at Hallen Avenue	A	1.8	-	-
Hallen EB left/right	A	3.1	1	70
Route 28 NB left/thru thru	A	2.5	11	345
Route 28 SB thru thru/right	A	0.8	1	144
Route 28 at Ridgewood Road/Wollaston Golf Club	A	1.7	-	-
Wollaston Golf Club EB left/thru/right	A	5.7	1	59
Ridgewood WB left/thru/right	A	6.5	1	66
Route 28 NB left/thru thru/right	A	1.2	4	252
Route 28 SB left/thru thru/right	A	2.1	9	299
Route 28 at Nahanton Avenue	A	1.3	-	-
Nahanton WB left/right	A	5.9	0	58
Route 28 NB thru thru/right	A	0.2	3	174
Route 28 SB left/thru thru	A	2.4	12	265
Route 28 at Heather Drive	A	0.5	-	-
Heather EB left/right	B	15.8	0	37
Route 28 NB left/thru thru	A	0.4	1	182
Route 28 SB thru thru/right	A	0.5	4	160
Route 28 at Sassamon Avenue	A	1.2	-	-
Sassamon WB left/right	B	13.9	0	42



TECHNICAL MEMORANDUM
Milton – Route 28 Corridor Road Diet Feasibility Study
February 2025

Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
Route 28 NB thru thru/right	A	0.8	1	159
Route 28 SB left/thru thru	A	1.5	6	133
Route 28 at Hilltop Street	A	5.7	-	-
Hilltop WB left/right	A	4.0	1	85
Route 28 NB thru thru/right	A	0.5	2	221
Route 28 SB left/thru thru	B	11.1	62	516
Route 28 at Eager Road	A	5.2	-	-
Eager WB left/right	E	64.4	6	98
Route 28 NB thru thru/right	A	0.3	2	141
Route 28 SB left/thru thru	A	9.6	45	238
Route 28 at Susi Lane	A	4.9	-	-
Susi EB left/thru/right	B	17.3	0	27
Susi WB left/thru/right	A	9.3	1	42
Route 28 NB thru thru/right	A	0.6	2	230
Route 28 SB left/thru thru	A	9.1	52	177
Route 28 at Brook Lane	B	15.9	-	-
Brook EB left/right	A	0.0	0	0
Route 28 NB left/thru thru	A	0.3	0	31
Route 28 SB thru thru/right	D	31.4	217	460
Route 28 at I-93 SB Off-Ramp	E	66.2	-	-
I-93 SB Off-Ramp WB right	A	0.4	0	0
Route 28 NB thru thru	E	70.1	387	1110
Route 28 at I-93 SB Off-Ramp	B	16.1	-	-
I-93 SB Off-Ramp EB right	A	0.9	1	114
Route 28 SB thru thru	C	22.3	0	50
Route 28 at I-93 NB Off-Ramp	A	3.3	-	-
I-93 NB Off-Ramp WB right	A	3.1	8	75
Route 28 NB thru thru	A	3.4	2	63
Route 28 at I-93 NB Off-Ramp	A	3.7	-	-



Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
I-93 NB Off-Ramp EB right	A	6.9	57	160
Route 28 SB thru thru	A	1.6	2	143



HOWARD STEIN HUDSON

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No-build and Alternatives Capacity Analysis



NO-BUILD (2033) CONDITIONS AND ALTERNATIVES CAPACITY ANALYSIS – SIGNALIZED INTERSECTIONS

Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
	No-build (2033)				No-build w/RBT ⁽¹⁾				No-build w/RBT+MET ⁽²⁾				Alternative 1 – Northbound Road Diet				Alternative 2 – Northbound Road Diet v2				Alternative 3 – Southbound Road Diet			
a.m. peak Hour																								
Route 28 at Reedsdale Rd	F	83.0	-	-	F	84.8	-	-	F	86.6	-	-	F	88.2	-	-	E	76.2	-	-	F	94.5	-	-
Route 28 EB left/thru	E	57.8	200	574	E	62.7	217	557	E	68.9	202	581	F	149.9	313	733	F	105.6	219	612	F	165.1	309	705
Route 28 EB right	F	101.2	200	574	F	110.8	217	557	F	99.8	202	581	F	138.8	296	477	D	52.9	219	612	C	25.8	309	705
Reedsdale WB left	Not under No-build												F	91.5	152	450	E	68.5	121	424	F	88.5	139	450
Reedsdale WB left/thru/right (thru/right in all alts)	E	60.9	139	534	E	68.9	162	503	E	76.5	174	511	D	42.8	152	450	D	40.5	139	424	D	41.6	136	452
Route 28 NB left left/thru/right	F	115.7	516	1186	F	111.5	514	1183	F	116.2	530	1178	E	76.2	331	1030	E	73.8	311	956	F	118.5	656	1173
Route 28 SB left/thru/right	E	63.2	139	459	E	63.9	143	459	E	61.9	141	469	F	139.4	296	477	F	118.3	254	476	F	82.2	188	467
Route 28 at Reed Street/Access Road	E	56.1	-	-	E	58.2	-	-	E	59.9	-	-	B	11.7	-	-	B	12.2	-	-	B	17.9	-	-
Reed EB left/thru/right	D	51.1	19	176	D	51.9	17	164	D	51.5	18	169	D	51.6	17	164	D	51.5	18	171	E	56.4	20	174
Access WB left/thru/right	A	0.0	0	0	A	0	0	0	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0
Route 28 NB left (Alt 1 & 2 Only)	Not under No-build												B	15.1	264	895	B	11.3	243	894	Not under this alternative			
Route 28 NB left/thru/right (thru/right in Alt 1 & 2)	F	83.4	628	913	F	86.7	678	913	F	90.4	68	913	B	14.7	264	895	B	15.7	273	889	C	22.0	187	846
Route 28 SB left/thru/right (left/thru/right in Alt 3)	A	3.3	8	191	A	0.7	0	52	A	3.6	9	197	A	3.5	9	210	A	3.3	8	183	A	5.2	25	734
Route 28 at Hillside Street	B	12.2	-	-	B	15.9	-	-	B	17.0	-	-	B	18.9	-	-	B	19.9	-	-	B	13.6	-	-
Hillside EB left/thru/right	D	40.2	36	209	D	46.4	41	206	D	50.1	48	210	F	218.9	167	229	F	201.3	163	235	F	105.4	97	209
Driveway WB left/thru/right	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0
Route 28 NB left	Not under No-build												E	61.2	84	290	E	65.8	83	280	Not under this alternative			
Route 28 NB left/thru/right (thru/right in Alt 1 & 2)	A	8.2	50	279	B	13.3	82	279	B	16.9	88	288	A	7.4	84	290	A	8.6	91	282	A	7.8	57	286
Route 28 SB left/thru/right (left/thru/right in Alt 3)	B	14.5	48	342	B	15.9	56	330	B	16.6	57	334	A	9.3	31	320	A	9.7	31	322	B	10.2	64	364
Route 28 at Chickatawbut Road	F	113.7	-	-	E	56.9	-	-	C	22.6	-	-	F	148.2	-	-	F	222.0	-	-	D	30.3	-	-
Chickatawbut EB left/thru/right	E	56.5	99	422	C	21.4	11	201	C	20.8	7	201	F	90.2	102	626	C	26.5	11	235	B	19.2	5	190
Chickatawbut WB left/thru/right	F	111.9	503	898	F	335.6	1316	2708	D	42.1	124	712	F	942.1	3493	5309	F	1528.2	4213	5309	F	123.4	496	1446
Route 28 NB left/thru/right (left/thru/right in Alt 2 only)	F	174.7	4276	5346	B	15.3	54	319	B	18.4	76	413	F	155.4	2844	5329	F	221.9	4585	5341	B	12.4	14	213
Route 28 NB right (Alt 2 only)	Not under No-build												Not under this alternative				F	202.9	4773	5340	Not under this alternative			
Route 28 SB left/thru/right	D	38.7	140	466	B	10.2	43	386	B	18.6	80	450	B	15.8	40	388	A	5.7	23	381	B	12.4	51	244
Route 28 at Scanlon Drive/Russ Street	E	64.7	-	-	E	64.8	-	-	E	64.9	-	-	E	65.3	-	-	E	79.8	-	-	E	66.9	-	-
Scanlon EB left	D	40.9	97	408	D	42.4	102	409	D	42.2	101	409	D	43.5	109	406	E	77.8	181	432	D	44.4	47	246
Scanlon EB left/thru/right	D	40.9	97	408	D	42.3	102	409	D	41.5	101	409	D	45.3	109	406	F	84.0	181	432	D	46.0	47	246
Russ WB left	D	45.0	45	239	D	43.7	44	248	D	45.1	47	259	D	45.7	45	250	D	50.7	65	311	D	46.4	47	246
Russ WB thru/right	D	42.9	45	239	D	44.6	44	248	D	46.1	47	259	D	45.9	45	250	E	66.3	65	311	D	44.5	47	246
Route 28 NB left	F	111.2	616	861	F	99.0	619	858	F	99.1	622	852	F	100.6	636	852	F	128.8	671	859	F	100.6	648	867
Route 28 NB thru/right</																								



Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
	No-build (2033)				No-build w/RBT ⁽¹⁾				No-build w/RBT+MET ⁽²⁾				Alternative 1 – Northbound Road Diet				Alternative 2 – Northbound Road Diet v2				Alternative 3 – Southbound Road Diet			
Access WB left/thru/right	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0
Route 28 NB left	Not under No-build												B	14.3	173	874	B	13.4	178	869	Not under this alternative			
Route 28 NB left/thru thru/right (thru/right in Alt 1 & 2 only)	A	5.7	30	459	A	B	10.9	178	869	7.9	39	541	A	9.9	173	874	B	10.3	161	882	B	14.3	105	723
Route 28 SB left/thru thru/right	A	4.0	16	301	A	A	3.7	16	307	3.8	17	286	A	3.8	16	303	A	3.7	15	325	D	38.4	478	999
Route 28 at Hillside Street	B	17.9	-	-	B	17.8	-	-	B	16.9	-	-	B	17.2	-	-	B	18.3	-	-	B	18.7	-	-
Hillside EB left/thru/right	D	40.9	54	200	D	42.5	56	200	D	40.9	54	200	F	88.6	114	200	F	90.9	116	200	F	97.2	126	201
Driveway WB left/thru/right	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0	F	151.1	2	68	F	251.2	2	68	A	0.0	0	0
Route 28 NB left	Not under No-Build												E	71.1	88	269	E	72.5	93	254	Not under this alternative			
Route 28 NB left/thru thru/right (thru/right in Alt 1 & 2 only)	B	10.3	51	274	B	11.5	68	278	C	20.5	68	270	A	8.8	88	269	B	10.1	98	274	B	14.4	88	272
Route 28 SB left/thru thru/right	C	21.3	131	367	C	20.4	129	362	B	19.1	118	368	B	12.9	78	363	B	13.3	80	347	B	10.7	112	369
Route 28 at Chickatawbut Road	F	132.1	-	-	D	32.6	-	-	D	36.9	-	-	F	295.5	-	-	F	122.1	-	-	B	16.2	-	-
Chickatawbut EB left/thru/right	F	114.4	410	903	F	127.7	446	1794	F	104.6	359	1643	F	216.1	764	2386	D	46.3	92	621	D	47.0	96	618
Chickatawbut WB left/thru/right	E	69.7	162	568	E	63.2	73	744	E	58.8	92	895	F	298.4	740	2399	F	262.2	589	1768	D	31.6	35	330
Route 28 NB left/thru thru/right (left/thru in Alt 2 only)	F	245.4	4606	5321	B	18.5	73	442	C	22.2	74	462	F	104.3	1535	4370	F	260.9	4332	5324	B	11.3	15	175
Route 28 NB right (Alt 2 only)	Not under No-Build												Not under this alternative				F	221.4	4698	5334	Not under this alternative			
Route 28 SB left/thru thru/right	D	54.7	356	498	B	15.9	88	467	C	29.9	217	487	C	21.5	166	474	B	12.5	76	465	A	9.1	52	294
Route 28 at Scanlon Drive/Russ Street	C	28.0	-	-	D	47.8	-	-	D	50.8	-	-	D	45.7	-	-	D	47.3	-	-	D	42.9	-	-
Scanlon EB left	C	28.6	48	244	D	34.4	53	238	D	34.7	53	238	D	38.8	59	262	D	40.0	60	253	E	79.3	166	528
Scanlon EB left/thru/right	C	22.0	53	361	D	34.2	53	238	D	33.5	53	238	D	39.1	59	262	D	38.1	60	253	E	71.9	166	528
Russ WB left	D	48.5	54	389	F	147.2	338	586	F	163.9	371	585	F	145.5	323	565	F	153.1	345	568	E	67.8	166	528
Russ WB thru/right	D	33.7	48	263	F	155.6	338	586	F	170.4	371	585	F	148.0	323	565	F	158.3	345	568	E	79.0	166	528
Route 28 NB left	C	26.4	106	381	D	49.5	115	434	D	47.8	116	413	D	52.6	118	425	E	59.3	117	425	D	48.6	117	422
Route 28 NB thru thru/right	D	34.5	106	381	D	37.4	115	434	D	38.4	116	413	D	37.9	118	425	D	37.6	117	425	D	38.3	117	422
Route 28 SB left	D	45.7	208	764	F	88.1	345	785	F	93.9	367	793	E	78.8	303	778	F	80.4	318	779	F	93.8	333	777
Route 28 SB thru thru/right	C	21.7	208	764	D	31.0	345	785	C	27.8	367	793	C	27.8	303	778	C	28.6	318	779	D	31.9	333	777

(1) – No-build with Roundabout at Route 28 and Chickatawbut Rd,

(2) – No-build with Roundabout at Route 28 and Chickatawbut Rd and Metering on Route 28 legs



NO-BUILD (2033) CONDITIONS AND ALTERNATIVES CAPACITY ANALYSIS – UNSIGNALIZED INTERSECTIONS

Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
	No-Build (2033)				No-build w/RBT ⁽¹⁾				No-build w/RBT+MET ⁽²⁾				Alternative 1 – Northbound Road Diet				Alternative 2 – Northbound Road Diet v2				Alternative 3 – Southbound Road Diet			
	a.m. peak Hour																							
Route 28 at Pleasant Street	E	58.9	-	-	E	58.4	-	-	E	59.9	-	-	C	21.4	-	-	B	17.5	-	-	D	37.8	-	-
Route 28 NB thru thru/right	F	89.8	807	1044	F	87.9	838	1042	F	91.3	841	1045	B	15.5	209	1010	B	16.4	218	1010	D	46.0	486	1026
Route 28 SB left/thru thru/right	A	2.9	7	136	A	4.7	15	231	C	21.6	14	278	D	32.5	176	759	B	19.9	91	517	B	19.7	136	1060
Route 28 at Highland Street	D	32.4	-	-	D	39.3	-	-	D	41.3	-	-	A	6.1	-	-	A	6.5	-	-	A	5.5	-	-
Highland EB left/right	A	1.5	1	71	D	30.6	17	176	F	131.6	11	158	A	4.0	3	101	A	3.4	2	78	A	4.9	3	102
Route 28 NB thru thru	D	50.1	374	756	E	59.4	466	758	E	63.3	481	755	A	9.0	130	735	B	10.1	148	745	A	7.2	56	533
Route 28 SB thru thru	A	0.6	0	29	A	0.7	0	52	A	0.7	0	58	A	0.7	0	81	A	0.5	0	23	A	1.5	2	245
Route 28 at Hallen Avenue	C	28.0	-	-	D	45.5	-	-	D	49.9	-	-	A	7.7	-	-	A	7.4	-	-	A	5.6	-	-
Hallen EB left/right	F	94.2	34	204	E	77.4	30	212	F	134.6	23	191	A	8.5	3	94	B	14.6	5	113	B	14.7	6	137
Route 28 left (Alt 1 & 2 only)	Not under No-build												B	18.9	175	758	A	10.0	155	1084	Not under this alternative			
Route 28 NB left/thru thru (thru in Alt 1 & 2)	D	40.5	326	1114	E	68.0	603	1130	E	75.0	666	1136	B	11.8	219	1102	B	11.4	198	1091	A	6.6	54	677
Route 28 SB thru thru/right	A	0.4	0	38	A	0.6	0	69	A	1.0	0	71	A	0.4	0	41	A	0.3	0	6	A	2.7	4	385
Route 28 at Ridgewood Road/Wollaston Golf Club	A	6.8	-	-	B	15.7	-	-	B	18.3	-	-	A	4.0	-	-	A	4.1	-	-	A	3.1	-	-
Wollaston Golf Club EB left/thru/right	A	4.9	0	42	A	1.4	0	37	A	2.1	1	34	A	2.0	0	42	A	2.4	1	37	A	7.7	0	28
Ridgewood WB left/thru/right	B	11.9	1	69	B	17.8	2	89	C	20.1	2	73	D	31.	2	84	C	28.9	1	73	A	9.1	2	70
Route 28 NB left/thru thru/right	A	9.9	60	430	C	23.6	156	455	C	27.7	197	480	A	5.0	48	418	A	5.2	51	421	A	1.5	7	332
Route 28 SB left/thru thru/right	A	0.9	1	145	A	1.4	4	197	B	12.0	4	169	A	1.4	3	170	A	1.4	3	146	A	6.5	32	598
Route 28 at Nahanton Avenue	A	1.3	-	-	A	3.1	-	-	A	3.8	-	-	A	1.1	-	-	A	1.2	-	-	A	1.1	-	-
Nahanton WB left/right	A	7.8	1	71	D	30.2	2	89	C	26.2	3	92	C	23.0	1	88	C	26.6	1	92	A	8.6	1	69
Route 28 NB thru thru/right	A	1.6	23	198	A	4.2	66	221	A	4.0	70	220	A	1.0	26	220	A	1.2	23	206	A	0.3	4	198
Route 28 SB left/thru thru	A	0.5	1	140	A	0.8	1	150	B	10.6	1	134	A	0.7	1	119	A	0.7	1	112	A	2.3	10	402
Route 28 at Heather Drive	A	1.9	-	-	A	5.8	-	-	A	6.9	-	-	A	1.4	-	-	A	1.3	-	-	A	0.6	-	-
Heather EB left/right	C	24.4	1	47	F	130.0	3	77	E	70.0	2	79	A	2.0	1	59	C	28.2	1	57	C	24.4	0	0
Route 28 NB left/thru thru	A	2.8	20	211	A	8.5	75	267	A	9.5	95	286	A	1.9	25	252	A	1.9	26	258	A	0.6	3	193
Route 28 SB thru thru/right	A	0.1	1	150	A	0.1	2	142	A	0.2	59	240	A	0.1	1	133	A	0.1	1	132	A	0.5	3	146
Route 28 at Sassamon Avenue	A	4.2	-	-	B	16.3	-	-	B	19.9	-	-	A	4.5	-	-	A	4.5	-	-	A	1.2	-	-
Sassamon WB left/right	A	7.9	0	71	C	25.9	2	89	C	24.0	1	83	D	34.1	2	93	C	27.1	1	79	A	7.6	1	70
Route 28 NB thru thru/right	A	6.2	40	411	C	24.8	197	659	C	28.7	251	726	A	6.5	79	674	A	6.7	84	690	A	1.1	0	108
Route 28 SB left/thru thru	A	0.3	0	64	A	0.3	0	49	B	11.6	1	79	A	0.4	0	47	A	0.4	0	25	A	1.2	4	193
Route 28 at Hilltop Street	A	1.5	-	-	A	5.2	-	-	A	6.5	-	-	A	1.8	-	-	A	2.2	-	-	A	2.3	-	-
Hilltop WB left/right	B	14.5	2	118	B	19.0	2	106	B	19.9	2	111	B	18.7	2	106	C	27.9	3	116	D	35.2	3	101
Route 28 NB thru thru/right	A	1.7	12	304	A	7.2	69	440	A	8.7	87	471	A	2.2	28	438	A	2.8	41	453	A	0.7	4	299
Route 28 SB left/thru thru	A	0.8	0	57	A	1.4	1	123	A	7.1	1	134	A	0.9	1	96	A	1.0	1	116	A	5.4	23	624
Route 28 at Eager Road	A	0.6	-	-	A	1.5	-	-	A	1.8	-	-	A	4.9	-	-	A	5.0	-	-	A	0.9	-	-
Eager WB left/right	B	10.3	2	93	B	12.5</																		



Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
No-Build (2033)				No-build w/RBT ⁽¹⁾				No-build w/RBT+MET ⁽²⁾				Alternative 1 – Northbound Road Diet				Alternative 2 – Northbound Road Diet v2				Alternative 3 – Southbound Road Diet				
Route 28 at I-93 SB Off-Ramp	F	175.7	-	-	F	124.3	-	-	F	126.6	-	-	D	48.7	-	-	F	175.4	-	-	A	3.3	-	-
I-93 SB Off-Ramp WB right	A	1.9	0	21	A	0.8	0	0	A	1.0	0	8	B	12.4	4	121	C	23.6	6	124	A	2.4	1	104
Route 28 NB thru thru	F	186.9	1289	1573	F	131.9	996	1568	F	134.3	1035	1569	D	50.9	345	1518	F	185.8	1092	1577	A	3.4	0	0
Route 28 at I-93 SB Off-Ramp	A	4.3	-	-	A	4.8	-	-	A	5.0	-	-	A	4.3	-	-	A	4.1	-	-	A	3.8	-	-
I-93 SB Off-Ramp EB right	A	0.3	0	53	A	0.4	0	71	A	0.4	0	78	A	0.3	0	55	A	0.3	0	64	A	0.3	0	56
Route 28 SB thru thru	A	6.6	0	0	A	7.3	0	0	A	7.5	0	0	A	6.7	0	0	A	6.2	0	0	A	6.0	0	0
Route 28 at I-93 NB Off-Ramp	D	34.5	-	-	B	10.8	-	-	B	12.7	-	-	A	7.7	-	-	E	68.8	-	-	A	2.0	-	-
I-93 NB Off-Ramp WB right	D	30.7	57	164	B	11.2	24	141	B	14.4	31	147	A	1.9	5	82	B	17.5	41	168	A	0.1	0	0
Route 28 NB thru thru	D	35.6	185	910	B	10.6	35	391	B	12.2	40	403	B	10.3	56	495	F	93.6	549	1379	A	2.8	0	0
Route 28 at I-93 NB Off-Ramp	A	1.2	-	-	A	1.3	-	-	A	1.3	-	-	A	1.3	-	-	A	1.3	-	-	A	1.2	-	-
I-93 NB Off-Ramp EB right	A	1.9	6	163	A	2.1	7	154	A	2.1	7	151	A	2.1	7	150	A	2.1	7	156	A	2.0	6	149
Route 28 SB thru thru	A	0.6	0	10	A	0.6	0	45	A	0.6	0	18	A	0.6	0	16	A	0.6	0	17	A	0.5	0	25
p.m. peak hour																								
Route 28 at Pleasant Street	A	4.6	-	-	A	6.5	-	-	A	6.3	-	-	A	6.4	-	-	A	6.1	-	-	D	31.9	-	-
Route 28 NB thru thru/right	A	7.8	56	607	B	10.7	99	801	B	10.2	94	728	B	10.0	110	952	A	2.1	3	120	D	30.1	316	939
Route 28 SB left/thru thru/right	A	1.2	2	142	A	1.2	2	120	B	16.5	3	129	A	2.3	4	125	A	9.8	103	941	D	34.5	485	1226
Route 28 at Highland Street	A	1.0	-	-	A	1.2	-	-	A	1.2	-	-	A	2.5	-	-	A	3.0	-	-	C	26.7	-	-
Highland EB left/right	A	2.6	2	88	A	3.1	3	96	A	4.2	3	98	A	4.0	4	125	A	3.4	3	105	F	450.5	236	326
Route 28 NB thru thru	A	0.9	1	151	A	1.2	3	244	A	1.2	2	200	A	4.1	48	717	A	5.1	61	711	A	1.2	3	232
Route 28 SB thru thru	A	0.8	0	112	A	0.9	1	119	A	1.0	1	119	A	0.6	0	29	A	0.6	0	87	D	36.7	388	917
Route 28 at Hallen Avenue	A	1.6	-	-	A	1.9	-	-	A	2.2	-	-	A	3.0	-	-	A	2.7	-	-	B	18.3	-	-
Hallen EB left/right	A	3.3	1	89	A	3.6	2	90	A	5.5	1	77	A	4.6	2	95	A	4.5	2	86	F	133.6	73	280
Route 28 left (Alt 1 & 2 only)	Not under No-Build												B	12.0	90	1061	B	11.4	73	981	Not under this alternative			
Route 28 NB left/thru thru (thru in Alt 1 & 2)	A	2.5	11	346	A	2.7	14	401	A	7.8	19	417	A	5.4	87	1050	A	4.7	67	1000	A	5.0	31	501
Route 28 SB thru thru/right	A	0.5	0	113	A	0.8	1	138	A	1.0	2	172	A	0.3	0	19	A	0.4	0	64	C	28.8	367	746
Route 28 at Ridgewood Road/Wollaston Golf Club	A	1.4	-	-	A	1.9	-	-	A	2.0	-	-	A	3.3	-	-	A	3.3	-	-	B	18.4	-	-
Wollaston Golf Club EB left/thru/right	A	3.3	1	54	A	3.8	1	60	A	3.8	1	54	A	8.3	3	82	A	8.2	3	89	D	34.3	3	88
Ridgewood WB left/thru/right	A	5.8	1	60	A	7.4	1	59	B	10.6	0	48	C	27.9	1	54	C	25.3	1	51	D	44.7	6	93
Route 28 NB left/thru thru/right	A	1.5	6	292	A	1.6	8	305	A	8.8	112	412	A	3.9	34	418	A	4.1	40	420	A	2.9	15	365
Route 28 SB left/thru thru/right	A	1.2	2	183	A	2.0	8	274	A	8.1	8	303	A	2.0	7	207	A	1.9	7	249	D	37.8	565	1065
Route 28 at Nahanton Avenue	A	0.7	-	-	A	0.8	-	-	A	0.8	-	-	A	1.0	-	-	A	1.1	-	-	A	6.1	-	-
Nahanton WB left/right	A	6.5	0	52	B	10.6	1	73	A	7.4	0	53	B	19.9	1	68	B	19.7	1	71	D	40.9	3	89
Route 28 NB thru thru/right	A	0.3	4	185	A	0.3	7	192	A	0.2	9	243	A	0.7	14	193	A	1.0	18	190	A	0.4	10	191
Route 28 SB left/thru thru	A	1.0	3	235	A	1.3	5	278	A	5.6	5	237	A	1.2	5	233	A	1.0	4	249	B	12.9	143	538
Route 28 at Heather Drive	A	0.4	-	-	A	0.4	-	-	A	0.4	-	-	A	0.9	-	-	A	0.9	-	-	A	1.4	-	-
Heather EB left/right	B	15.8	0	36	C	25.5	0	48	C	20.1	0	47	D	50.6	1	56	D	53.7	1	50	C	23.1	0	8
Route 28 NB left/thru thru	A	0.5	3	207	A	0.5	2	190	A	7.3	3	214	A	1.4	14	237	A	1.6	19	240	A	0.7	3	210
Route 28 SB thru thru/right	A	0.3	2	144	A	0.3	2	154	A	0.2	3	214	A											



Intersection and Movement	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)	LOS	Delay (sec)	Average Queue (ft)	Maximum Queue (ft)
	No-Build (2033)				No-build w/RBT ⁽¹⁾				No-build w/RBT+MET ⁽²⁾				Alternative 1 – Northbound Road Diet				Alternative 2 – Northbound Road Diet v2				Alternative 3 – Southbound Road Diet			
Route 28 at Susi Lane	A	4.6	-	-	A	0.6	-	-	A	0.9	-	-	C	26.2	-	-	A	7.7	-	-	A	1.5	-	-
Susi EB left/thru/right	B	16.0	0	28	A	7.9	0	19	B	11.0	0	26	A	9.4	0	42	B	11.4	0	39	B	12.6	0	25
Susi WB left/thru/right	C	24.4	1	46	A	3.7	0	35	B	13.4	0	40	C	24.1	1	51	B	19.5	1	47	A	4.0	0	49
Route 28 NB thru thru/right	A	0.7	4	237	A	0.4	2	175	A	0.8	2	192	D	53.0	322	425	B	15.3	160	402	A	0.4	2	206
Route 28 SB left/thru thru	A	8.2	48	176	A	0.7	6	163	A	2.2	11	183	A	1.5	6	309	A	1.0	3	268	A	2.8	30	767
Route 28 at Brook Lane	B	16.5	-	-	A	1.3	-	-	A	3.9	-	-	C	23.7	-	-	A	7.9	-	-	A	0.7	-	-
Brook EB left/right	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0	A	0.0	0	0
Route 28 NB left/thru thru	A	0.4	0	44	A	0.0	0	7	A	0.9	0	57	D	44.8	466	959	B	15.3	327	957	A	0.6	1	96
Route 28 SB thru thru/right	D	32.1	221	461	A	2.1	10	256	A	7.0	43	436	A	4.1	23	349	A	1.4	5	275	A	0.8	2	231
Route 28 at I-93 SB Off-Ramp	F	138.2	-	-	A	6.8	-	-	A	6.6	-	-	A	9.3	-	-	F	101.7	-	-	A	2.5	-	-
I-93 SB Off-Ramp WB right	A	0.9	0	2	A	0.4	0	0	A	0.4	0	0	A	4.5	1	52	B	16.9	3	84	A	1.8	0	50
Route 28 NB thru thru	F	146.9	832	1555	A	7.1	24	276	A	6.9	23	258	A	9.6	41	416	F	107.1	582	1481	A	2.5	0	0
Route 28 at I-93 SB Off-Ramp	B	16.6	-	-	B	13.5	-	-	B	13.2	-	-	A	5.4	-	-	A	5.4	-	-	A	6.7	-	-
I-93 SB Off-Ramp EB right	A	0.9	1	103	A	1.1	1	122	A	1.0	1	116	A	0.8	1	94	A	0.9	1	114	A	0.9	1	121
Route 28 SB thru thru	C	22.9	0	44	B	18.3	0	42	B	18.0	0	42	A	7.2	0	0	A	7.2	0	0	A	9.3	0	14
Route 28 at I-93 NB Off-Ramp	A	9.8	-	-	A	1.3	-	-	A	1.3	-	-	A	1.1	-	-	B	13.9	-	-	A	1.0	-	-
I-93 NB Off-Ramp WB right	B	10.2	27	144	A	0.9	0	47	A	0.9	0	29	A	0.1	0	0	A	7.0	21	111	A	0.1	0	0
Route 28 NB thru thru	A	9.6	18	314	A	1.7	0	0	A	1.6	0	0	A	1.8	0	0	B	18.9	59	516	A	1.7	0	0
Route 28 at I-93 NB Off-Ramp	A	3.7	-	-	A	5.9	-	-	A	6.2	-	-	A	4.6	-	-	A	4.9	-	-	A	5.4	-	-
I-93 NB Off-Ramp EB right	A	7.1	62	159	A	9.4	76	164	B	10.3	82	164	A	8.3	68	162	A	8.6	70	162	A	8.2	64	162
Route 28 SB thru thru	A	1.3	1	107	A	3.7	9	313	A	3.7	8	293	A	2.3	4	235	A	2.6	5	221	A	3.4	7	280

(1) – No-build with Roundabout at Route 28 and Chickatawbut Rd,

(2) – No-build with Roundabout at Route 28 and Chickatawbut Rd and Metering on Route 28 legs



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Appendix C

Route 28 at Chickatawbut Road Traffic Sensitivity
Memorandum – May 2023



TO: Joshua Bartus, Project Manager - MassDOT
James Danila, PE PTOE, State Traffic Engineer - MassDOT

FROM: Andrew Fabiszewski - Howard Stein Hudson

DATE: May 4, 2023

HSH PROJECT NO.: 2021055.15

SUBJECT: Milton Rte 28 at Chickatawbut Rd – Roundabout Metering Sensitivity Analysis

Background

The Randolph Avenue (Route 28)/Chickatawbut Road intersection is undergoing 75% design for the needed improvements to enhance safety and operations. At the Design Public Hearing (October 27, 2022), several community concerns were brought up regarding the availability of gaps for traffic on Chickatawbut Road to be able to turn onto Randolph Avenue. As a result of these concerns, HSH was asked to evaluate roundabout metering signals to be able to control traffic flows along Route 28 and provide gaps for Chickatawbut Road to enter the intersection with Route 28. Chickatawbut Road is intended to function as a Department of Conservation and Recreation (DCR) parkway providing access to environmentally sensitive parkland and recreation opportunities. However, while Chickatawbut Road serves as an important neighborhood connection for local residents, much of the traffic utilizing this road is cutting through to avoid regional congestion along I-93. The roundabout is expected to see significant queuing along Chickatawbut Road due to a lack of gaps in Route 28. This memorandum assesses the traffic that is likely to divert from Chickatawbut Road due to increased queues and performs a sensitivity analysis to assess traffic operations at the roundabout considering these potential diversions.

Data Collection and Methodology

Howard Stein Hudson (HSH) used the Massachusetts Department of Transportation's (MassDOT's) INRIX data subscription to conduct segment analyses for all movements along Chickatawbut Road approaching the Randolph Avenue intersection (eastbound/westbound lefts, throughs, and rights). The data was collected as the average of Tuesday-Thursday for 2022 during the a.m. and p.m. peak periods. The Origin-Destinations are grouped by Traffic Analysis Zones (TAZs) to show the general geographic areas of where the trips begin and end. The INRIX data maps are included in **Appendix A** to this memo.

The segment route origins were then assessed as to the likelihood of diversion by comparing the route to other potential travel routes. If an equally viable alternative route was identified, the



percentage from that route was diverted away from the Chickatawbut Road approach to Randolph Avenue. The new traffic volumes were then factored by an increase of 10% and a decrease of 10% as well as the baseline to be utilized for a sensitivity analysis on the impact in queueing and delays on Chickatawbut Road with SIDRA traffic operations analysis.

Route Alternatives

The origin and destination maps shown in **Appendix A** highlight where most drivers utilizing the segments are starting and ending their trips. For each of these movements, we identified alternative routes for the non-local drivers to utilize as follows:

- Eastbound Left
 - The relatively small number of vehicles from the further west TAZs (TAZ 1541 – Dover, MA; TAZ 1614 – Westwood, MA; and TAZ 1674/1676 – Canton, MA) can utilize I-93 eastbound and head north on Route 28.
- Eastbound Through
 - TAZ's to the North (TAZ 1071/1072/1077 – Milton, MA) have the alternative of utilizing Reedsdale Road to access Route 28 to Chickatawbut Road.
- Eastbound Right
 - Like the eastbound through movement, TAZ's to the north (TAZ 0409/0413 – Boston, MA; and TAZ 1071/1072 – Milton, MA) have the alternative of utilizing Reedsdale Road to access Route 28 to Chickatawbut Road.
- Westbound Left
 - Many vehicles are seen are coming from TAZ's north as far as Boston (TAZ 0154/0386 – Boston, MA; and TAZ 1081/1087/1099/1109/1111 – Quincy, MA), indicating that some are getting off I-93 to utilize Chickatawbut Road; these would be assumed to stay on I-93 in this re-route.
- Westbound Through
 - TAZ's to the north (TAZ 1081/1087 – Quincy, MA) have the alternative of utilizing East Milton Square to Pleasant Street to access Route 28 to Chickatawbut Road.
- Westbound Right
 - TAZ's to the southeast (TAZ 1794/797/1799 – Braintree, MA) have the alternative of utilizing I-93 to Route 28 and continuing north rather than cutting through on Chickatawbut Road.



Operations Analysis

Traffic operations analysis was conducted using SIDRA Intersection, an industry standard software for analyzing roundabout operations. The previous SIDRA traffic operations without roundabout metering and with rerouting as a result are shown in **Table 1**. Metering signals were added in SIDRA to assess the traffic operations impacts of signals stopping the mainline Route 28 traffic to provide more gaps for Chickatawbut Road traffic to utilize the roundabout. The metered signals were set to activate based on a 600 feet queue (roughly 24 vehicles) along Chickatawbut Road. It will result in a maximum of a 110-second cycle length, giving Chickatawbut Road a 10-second gap every roughly two (2) minutes. The roundabout metering will be conducted directionally depending on the peak hour, with the northbound approach metered during the a.m. peak hour and the southbound approach metered in the p.m. peak hour. **Table 2** shows the SIDRA operations analysis for the intersection with roundabout metering and rerouted traffic. The SIDRA outputs are included in **Appendix B**.



Table 1. Roundabout Traffic Operations Without Metering Analysis

Intersection/Movement	LOS	Delay (Sec)	V/C Ratio	50% Queue (ft)	95% Queue (ft)	LOS	Delay (Sec)	V/C Ratio	50% Queue (ft)	95% Queue (ft)	LOS	Delay (Sec)	V/C Ratio	50% Queue (ft)	95% Queue (ft)	LOS	Delay (Sec)	V/C Ratio	50% Queue (ft)	95% Queue (ft)
	Base Volumes					Reroute Sensitivity					+10% Reroute Sensitivity					-10% Reroute Sensitivity				
	a.m. Peak Hour																			
Rte 28/Chickatawbut Rd	D	26.4	-	-	-	C	19.2	-	-	-	C	16.0	-	-	-	C	23.7	-	-	-
Chickatawbut EB	B	10.2	0.31	13	32	A	9.1	0.24	9	23	A	8.8	0.22	8	21	A	9.4	0.26	10	26
Chickatawbut WB	F	117.9	1.12	229	570	F	74.4	0.97	99	276	F	53.8	0.87	61	171	F	102.4	1.07	172	464
Route 28 NB approach	B	13.2	0.69	100	249	B	12.2	0.67	68	161	B	12.0	0.66	59	143	B	12.5	0.68	79	190
Route 28 SB approach	B	10.6	0.53	42	105	B	10.6	0.54	43	106	B	10.2	0.52	41	101	B	10.7	0.54	43	107
p.m. Peak Hour																				
Rte 28/Chickatawbut Rd	E	41.4	-	-	-	B	13.1	-	-	-	B	14.3	-	-	-	B	12.1	-	-	-
Chickatawbut EB	F	190.5	1.28	360	895	D	30.2	0.59	31	80	E	36.0	0.66	38	99	D	25.8	0.51	25	64
Chickatawbut WB	C	15.1	0.59	44	110	B	10.3	0.39	20	51	B	11.2	0.43	24	61	A	9.5	0.35	17	42
Route 28 NB approach	A	6.4	0.32	18	45	A	6.0	0.30	17	43	A	6.1	0.31	18	44	A	5.9	0.30	17	42
Route 28 SB approach	C	21.7	0.83	204	506	B	14.9	0.73	134	340	C	15.8	0.75	145	372	B	14.1	0.71	121	304

Table 2. Roundabout With Metering Traffic Operations Comparison

Intersection/ Movement	LOS	Delay (Sec)	V/C Ratio	50% Queue (ft)	95% Queue (ft)	LOS	Delay (Sec)	V/C Ratio	50% Queue (ft)	95% Queue (ft)	LOS	Delay (Sec)	V/C Ratio	50% Queue (ft)	95% Queue (ft)	LOS	Delay (Sec)	V/C Ratio	50% Queue (ft)	95% Queue (ft)
	Base Volumes					Reroute Sensitivity					+10% Reroute Sensitivity					-10% Reroute Sensitivity				
	a.m. Peak Hour																			
Rte 28/Chickatawbut Rd	C	17.5	-	-	-	B	12.5	-	-	-	B	11.3	-	-	-	C	15.3	-	-	-
Chickatawbut EB approach	A	7.1	0.31	13	32	A	6.3	0.24	9	23	A	6.0	0.21	8	21	A	6.5	0.26	10	26
Chickatawbut WB approach	E	41.1	0.82	109	271	D	34.8	0.77	74	185	D	28.4	0.69	57	142	E	38.6	0.80	98	243
Route 28 NB approach	C	18.2	0.88	645	1053	B	10.9	0.80	611	997	B	10.5	0.79	599	978	B	14.7	0.84	637	1039
Route 28 SB approach	A	6.0	0.51	33	82	A	6.2	0.52	34	84	A	6.1	0.51	34	83	A	6.2	0.51	34	84
p.m. Peak Hour																				
Rte 28/Chickatawbut Rd	D	28.2	-	-	-	B	10.6	-	-	-	A	9.4	-	-	-	B	12.1	-	-	-
Chickatawbut EB approach	F	68.7	0.96	135	336	C	22.3	0.58	39	96	C	19.2	0.51	32	80	D	26.5	0.65	46	115
Chickatawbut WB approach	A	9.9	0.56	34	84	A	6.7	0.40	20	49	A	6.0	0.36	17	41	A	7.5	0.44	23	57
Route 28 NB approach	A	2.1	0.30	16	40	A	2.3	0.30	17	43	A	2.2	0.30	17	42	A	2.4	0.31	18	44
Route 28 SB approach	E	35.5	1.01	887	1448	B	13.1	0.84	651	1063	B	11.8	0.82	611	998	B	14.8	0.87	704	1148



Traffic Operations Summary

As shown in **Table 1**, the rerouted operations indicate that if the queueing conditions on Chickatawbut Road become poor as a result of the roundabout, there are many vehicles who are not reliant on Chickatawbut Road that have the potential to re-route and result in more acceptable levels of service. In comparing **Table 1** to **Table 2**, the traffic operations with roundabout metering are greatly improved along the Chickatawbut Road approaches compared to the previously conducted analysis. The Chickatawbut Road eastbound and westbound approaches show substantial decreases in queueing while the mainline Route 28 shows increased queueing, more like the existing condition, in the peak direction (northbound in the a.m. and southbound in the p.m.). The peak directional queueing and metering along Route 28 may also help residents who are concerned with the inability to exit their driveways along Route 28 as this will create breaks in the traffic. Were the roundabout metering option to be further pursued, a more detailed investigation with more time periods would need to be conducted to see if metering is necessary outside of the peak hours. Due to the hourly variation of traffic along Route 28 and Chickatawbut Road, it is possible that metering would only need to occur during peak periods.

However, there are potential drawbacks to consider; the roundabout metering may improve operations along Chickatawbut Road, inducing more regional traffic to utilize Chickatawbut Road, a DCR parkway through sensitive environmental areas, to avoid I-93. Were this to be the case, we would recommend coordination with DCR and investigating further changes to the queue length detection of the roundabout metering to find a proper balance of acceptable Chickatawbut Road operations with accommodating the local traffic.



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Appendix A

INRIX Data



Figure 1. *Chickatawbut Road Eastbound Left-turn Segment Analysis, a.m. Peak Period*

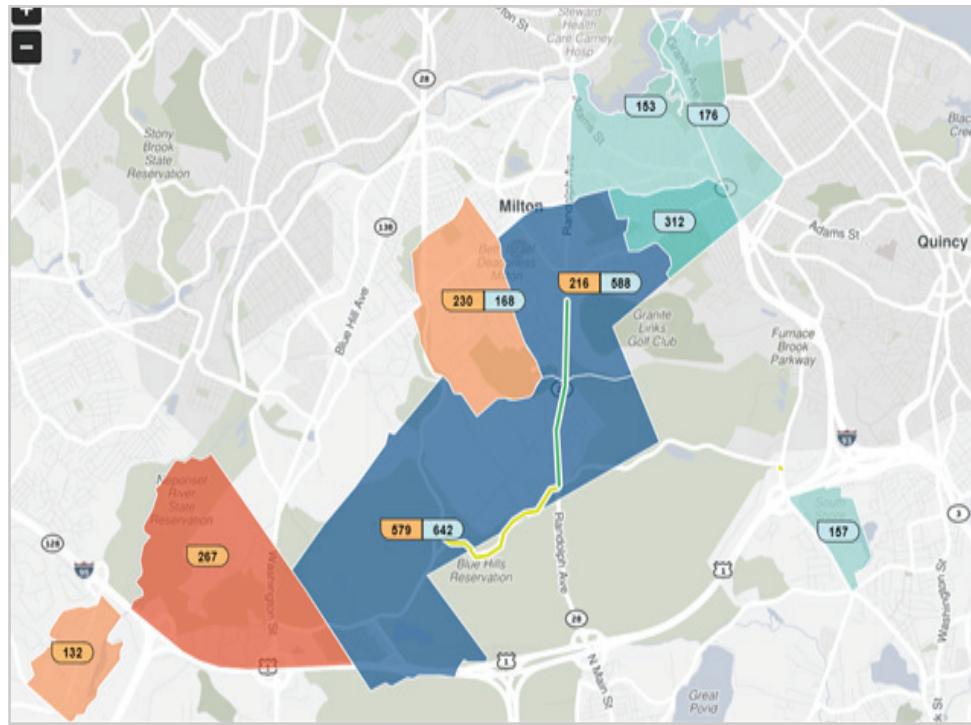


Figure 2. *Chickatawbut Road Eastbound Left-turn Segment Analysis, p.m. Peak Period*

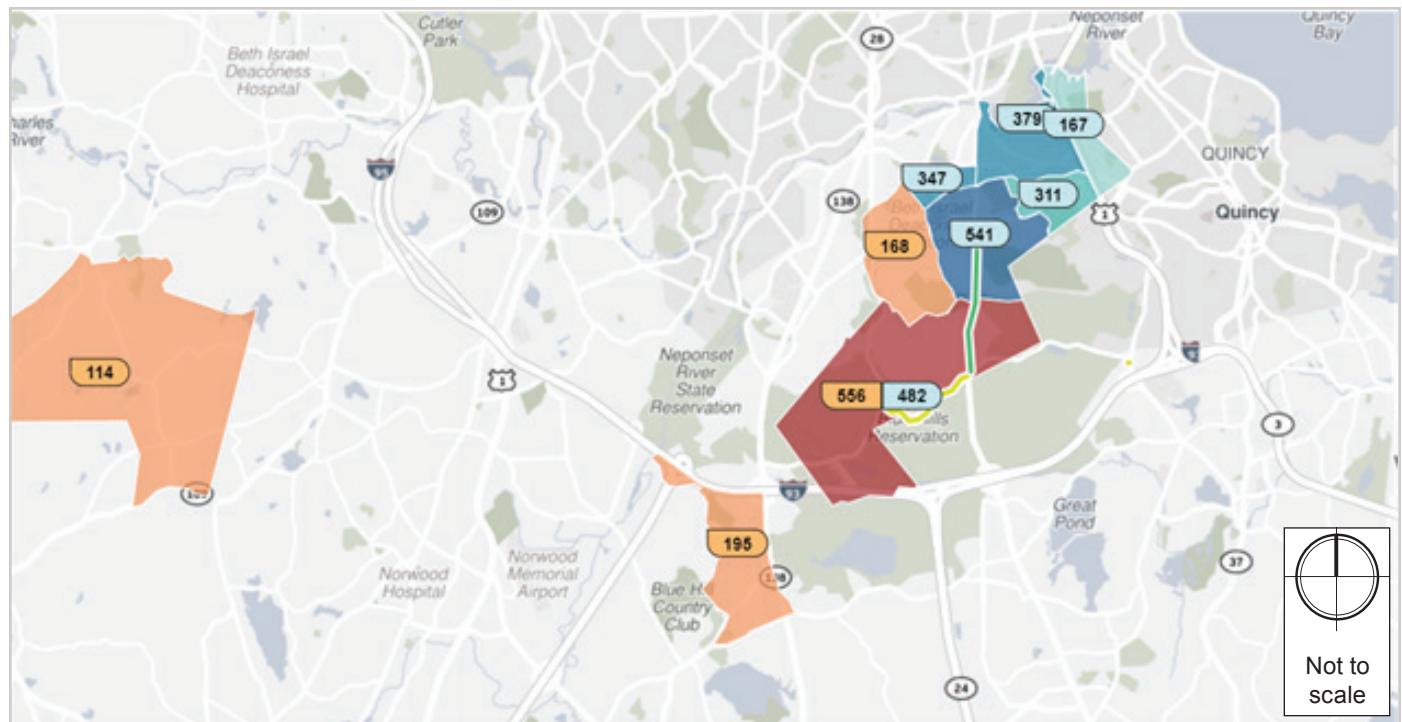




Figure 3. *Chickatawbut Road Eastbound Through Segment Analysis, a.m. Peak Period*

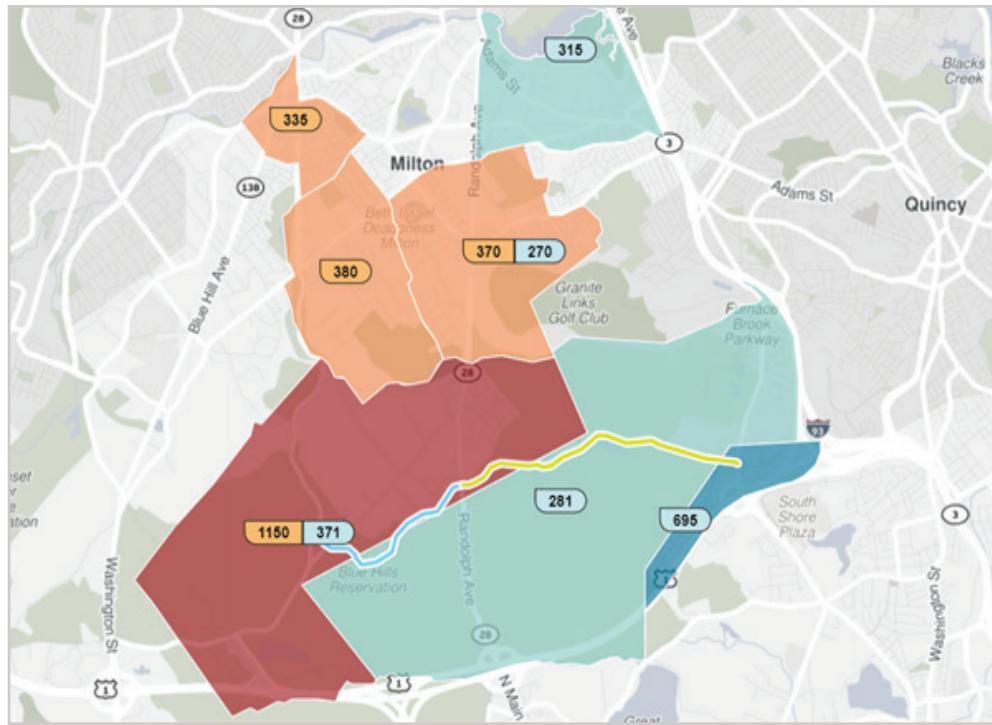


Figure 4. *Chickatawbut Road Eastbound Through Segment Analysis, p.m. Peak Period*

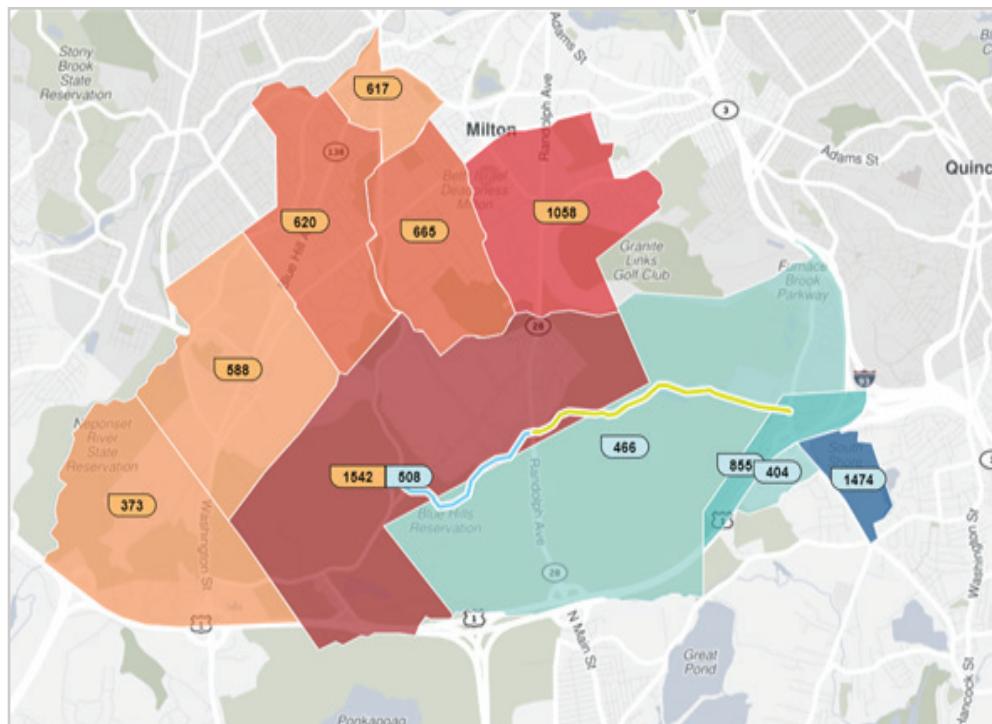




Figure 5. *Chickatawbut Road Eastbound Right-turn Segment Analysis, a.m. Peak Hour*

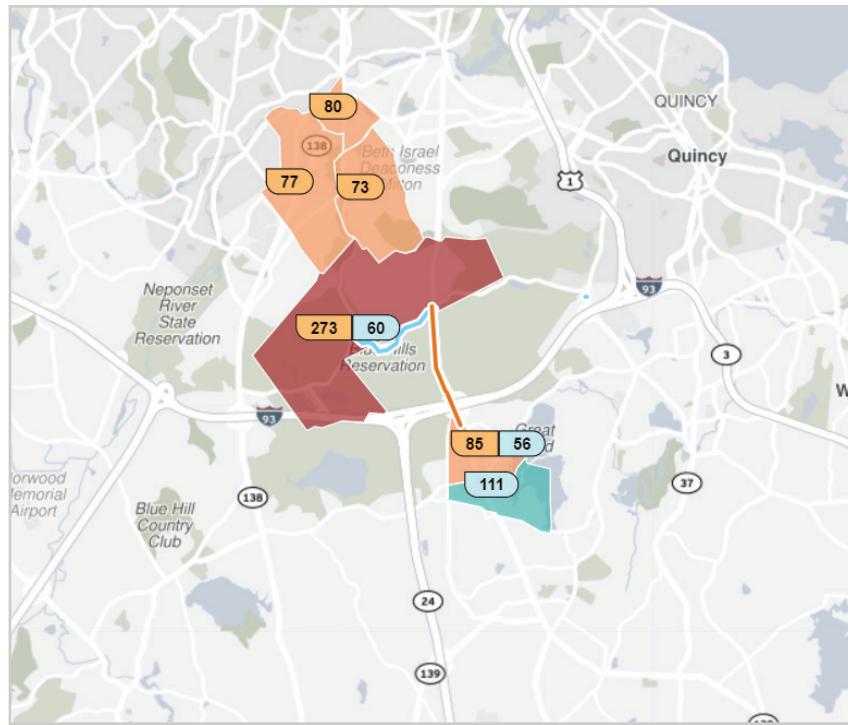


Figure 6. *Chickatawbut Road Eastbound Right-turn Segment Analysis, a.m. Peak Period*

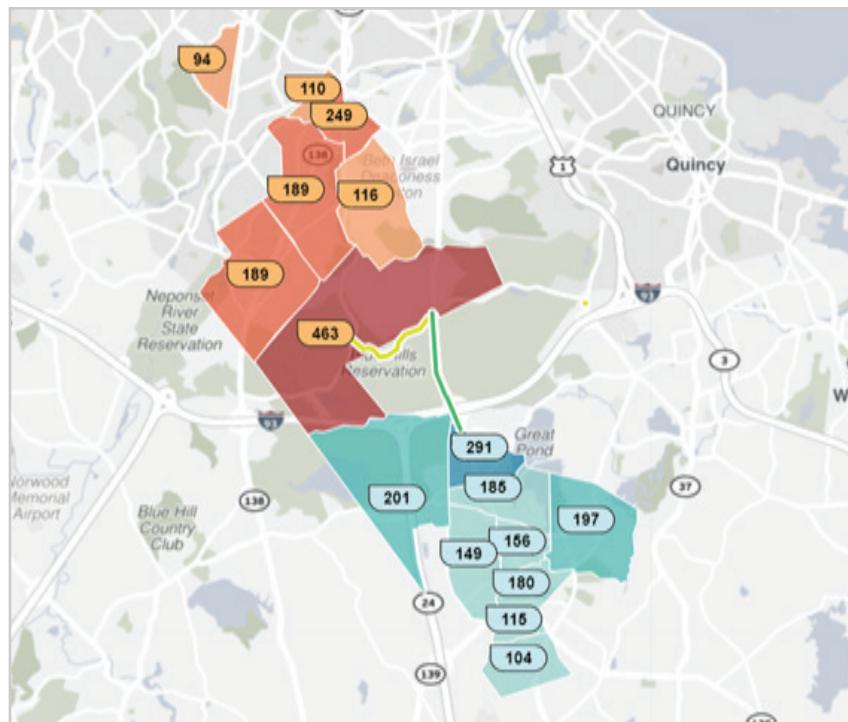




Figure 7. *Chickatawbut Road Westbound Left-turn Segment Analysis, a.m. Peak Period*

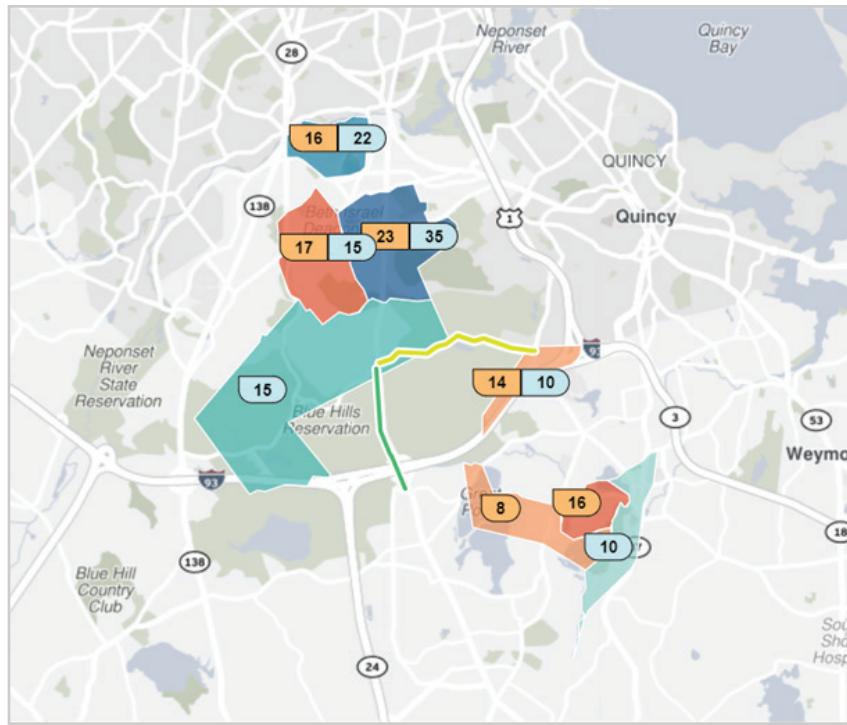


Figure 8. *Chickatawbut Road Westbound Left-turn Segment Analysis, p.m. Peak Period*

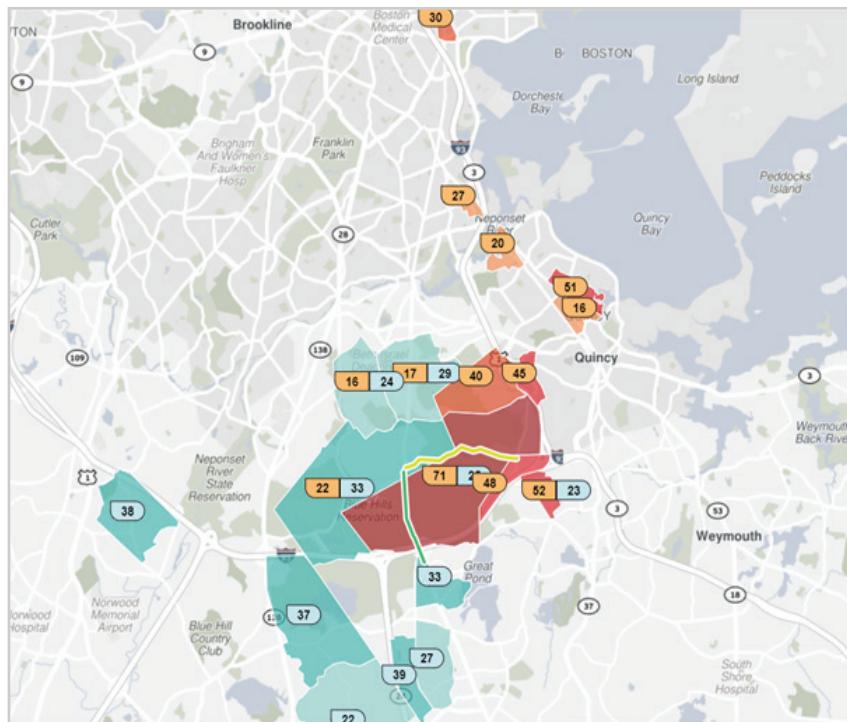




Figure 9. *Chickatawbut Road Westbound Through Segment Analysis, a.m. Peak Hour*

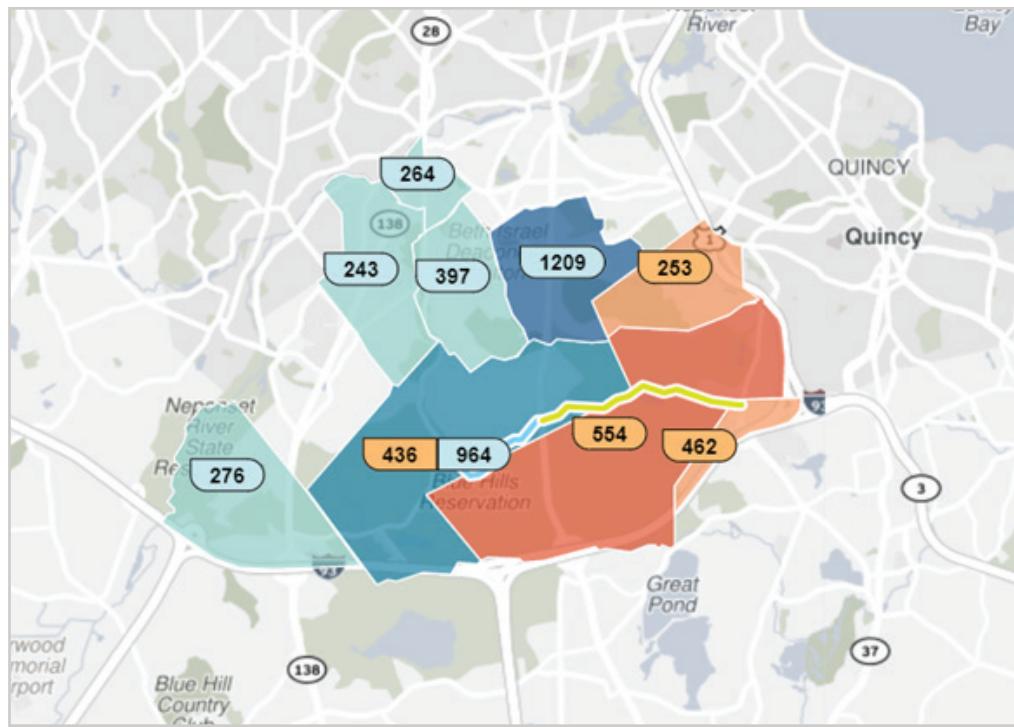


Figure 10. *Chickatawbut Road Westbound Through Segment Analysis, p.m. Peak Hour*

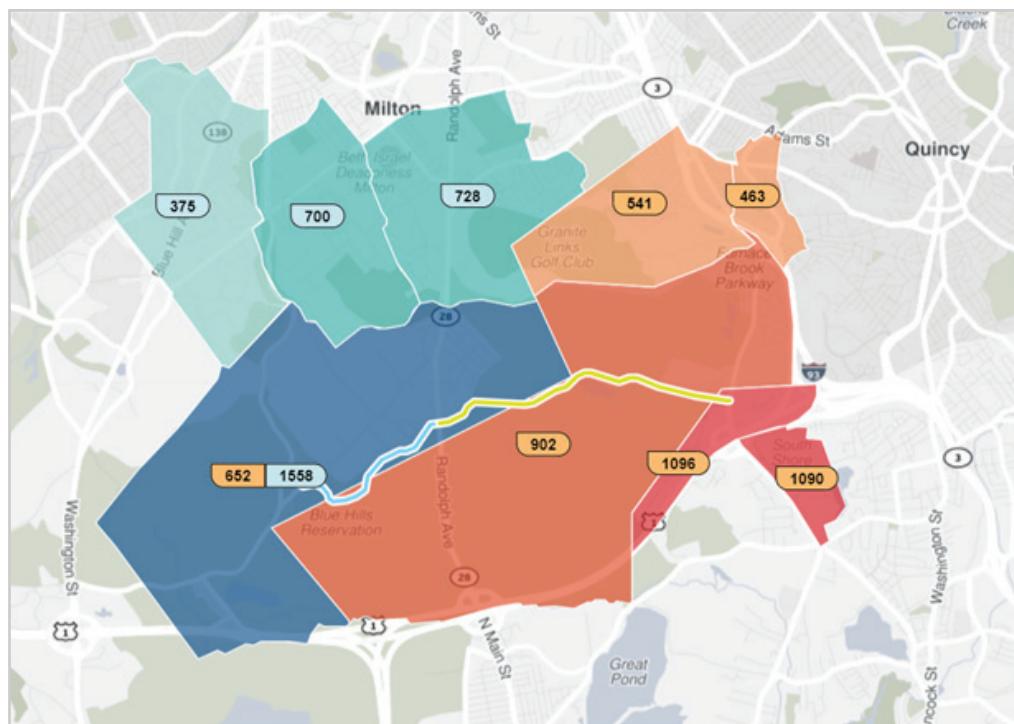




Figure 11. *Chickatawbut Road Westbound Right-turn Segment Analysis, a.m. Peak Period*

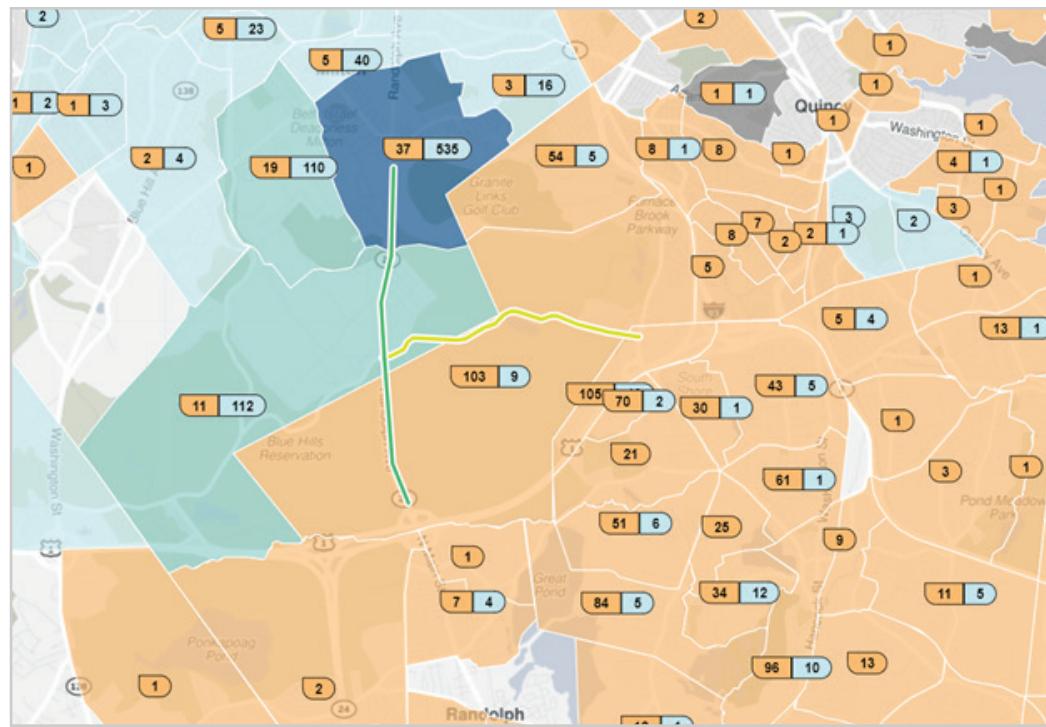
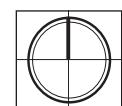
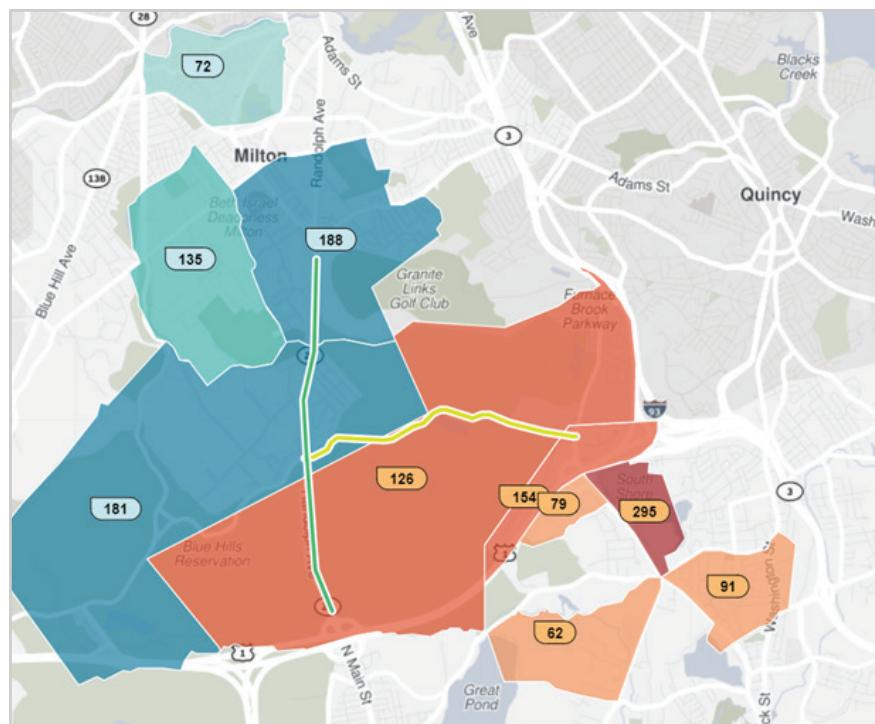


Figure 12. *Chickatawbut Road Westbound Right-turn Segment Analysis p.m. Peak Period*



Not to scale



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Appendix B

SIDRA

MOVEMENT SUMMARY

Site: 101 [Roundabout metered - AM Base (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout Metering

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	HV %	[Total veh/h]	HV %	v/c	sec		[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	202	0.0	220	0.0	0.878	18.2	LOS C	41.8	1052.7	0.98	0.95	1.42	28.4
8	T1	1232	1.3	1339	1.3	0.878	18.2	LOS C	41.8	1052.7	0.98	0.95	1.42	28.7
18	R2	37	0.0	40	0.0	0.878	18.2	LOS C	41.7	1052.3	0.98	0.95	1.42	28.1
Approach		1471	1.1	1599	1.1	0.878	18.2	LOS C	41.8	1052.7	0.98	0.95	1.42	28.6
East: Chickatawbut Rd														
1	L2	21	0.0	23	0.0	0.823	39.0	LOS E	10.8	271.3	1.00	1.49	2.52	22.2
6	T1	205	0.5	220	0.5	0.823	39.0	LOS E	10.8	271.3	1.00	1.49	2.52	22.2
16	R2	144	0.0	155	0.0	0.823	39.0	LOS E	10.8	271.3	1.00	1.49	2.52	21.9
Approach		370	0.3	398	0.3	0.823	41.1	LOS E	10.8	271.3	1.00	1.49	2.52	22.1
North: Rt 28														
7	L2	65	0.0	69	0.0	0.510	7.4	LOS A	3.2	82.1	0.66	0.60	0.71	33.9
4	T1	585	2.0	622	2.0	0.510	7.5	LOS A	3.2	82.1	0.61	0.54	0.65	34.4
14	R2	30	0.0	32	0.0	0.230	3.3	LOS A	1.0	26.2	0.51	0.41	0.51	34.7
Approach		680	1.7	723	1.7	0.510	6.0	LOS A	3.2	82.1	0.61	0.54	0.65	34.4
West: Chickatawbut Rd														
5	L2	45	0.0	49	0.0	0.312	5.9	LOS A	1.3	31.8	0.62	0.62	0.62	34.0
2	T1	85	0.0	92	0.0	0.312	5.9	LOS A	1.3	31.8	0.62	0.62	0.62	34.0
12	R2	91	0.0	99	0.0	0.312	10.2	LOS B	1.3	31.8	0.62	0.62	0.62	33.2
Approach		221	0.0	240	0.0	0.312	7.1	LOS A	1.3	31.8	0.62	0.62	0.62	33.7
All Vehicles		2742	1.0	2960	1.0	0.878	17.5	LOS C	41.8	1052.7	0.86	0.90	1.31	29.0

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 101 [Roundabout metered - AM Sensitivity (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout Metering

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	HV %	[Total veh/h]	HV %	v/c	sec		[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	202	0.0	220	0.0	0.800	10.9	LOS B	39.6	997.1	0.88	0.65	0.96	31.2
8	T1	1232	1.3	1339	1.3	0.800	10.9	LOS B	39.6	997.1	0.88	0.65	0.97	31.5
18	R2	37	0.0	40	0.0	0.800	10.9	LOS B	39.5	996.7	0.88	0.65	0.97	30.9
Approach		1471	1.1	1599	1.1	0.800	10.9	LOS B	39.6	997.1	0.88	0.65	0.97	31.5
East: Chickatawbut Rd														
1	L2	17	0.0	18	0.0	0.765	33.5	LOS D	7.4	184.9	0.94	1.28	2.05	23.7
6	T1	187	0.5	201	0.5	0.765	33.5	LOS D	7.4	184.9	0.94	1.28	2.05	23.7
16	R2	120	0.0	129	0.0	0.765	33.5	LOS D	7.4	184.9	0.94	1.28	2.05	23.3
Approach		324	0.3	348	0.3	0.765	34.8	LOS D	7.4	184.9	0.94	1.28	2.05	23.6
North: Rt 28														
7	L2	65	0.0	69	0.0	0.515	7.6	LOS A	3.3	84.0	0.67	0.61	0.73	33.8
4	T1	585	2.0	622	2.0	0.515	7.6	LOS A	3.3	84.0	0.62	0.55	0.66	34.4
14	R2	30	0.0	32	0.0	0.232	3.4	LOS A	1.1	26.6	0.51	0.42	0.51	34.7
Approach		680	1.7	723	1.7	0.515	6.2	LOS A	3.3	84.0	0.62	0.55	0.66	34.3
West: Chickatawbut Rd														
5	L2	34	0.0	37	0.0	0.237	4.9	LOS A	0.9	23.0	0.59	0.59	0.59	34.5
2	T1	63	0.0	68	0.0	0.237	4.9	LOS A	0.9	23.0	0.59	0.59	0.59	34.4
12	R2	71	0.0	77	0.0	0.237	9.0	LOS A	0.9	23.0	0.59	0.59	0.59	33.7
Approach		168	0.0	183	0.0	0.237	6.3	LOS A	0.9	23.0	0.59	0.59	0.59	34.1
All Vehicles		2643	1.1	2853	1.1	0.800	12.5	LOS B	39.6	997.1	0.80	0.70	1.00	31.0

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 101 [Roundabout metered - AM Sensitivity - (-10%) (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout Metering

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	HV %	[Total veh/h]	HV %	v/c	sec		[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	202	0.0	220	0.0	0.793	10.5	LOS B	38.8	977.6	0.86	0.61	0.92	31.4
8	T1	1232	1.3	1339	1.3	0.793	10.5	LOS B	38.8	977.6	0.87	0.61	0.93	31.8
18	R2	37	0.0	40	0.0	0.793	10.5	LOS B	38.7	977.1	0.87	0.61	0.93	31.1
Approach		1471	1.1	1599	1.1	0.793	10.5	LOS B	38.8	977.6	0.87	0.61	0.93	31.7
East: Chickatawbut Rd														
1	L2	15	0.0	16	0.0	0.685	27.1	LOS D	5.7	141.6	0.91	1.16	1.73	25.5
6	T1	168	0.5	181	0.5	0.685	27.1	LOS D	5.7	141.6	0.91	1.16	1.73	25.4
16	R2	108	0.0	116	0.0	0.685	27.1	LOS D	5.7	141.6	0.91	1.16	1.73	25.0
Approach		291	0.3	313	0.3	0.685	28.4	LOS D	5.7	141.6	0.91	1.16	1.73	25.3
North: Rt 28														
7	L2	65	0.0	69	0.0	0.513	7.5	LOS A	3.3	83.2	0.66	0.61	0.72	33.8
4	T1	585	2.0	622	2.0	0.513	7.5	LOS A	3.3	83.2	0.62	0.55	0.66	34.4
14	R2	30	0.0	32	0.0	0.231	3.4	LOS A	1.0	26.4	0.51	0.42	0.51	34.7
Approach		680	1.7	723	1.7	0.513	6.1	LOS A	3.3	83.2	0.62	0.55	0.66	34.3
West: Chickatawbut Rd														
5	L2	31	0.0	34	0.0	0.214	4.6	LOS A	0.8	20.5	0.58	0.57	0.58	34.6
2	T1	57	0.0	62	0.0	0.214	4.6	LOS A	0.8	20.5	0.58	0.57	0.58	34.6
12	R2	64	0.0	70	0.0	0.214	8.7	LOS A	0.8	20.5	0.58	0.57	0.58	33.8
Approach		152	0.0	165	0.0	0.214	6.0	LOS A	0.8	20.5	0.58	0.57	0.58	34.2
All Vehicles		2594	1.1	2800	1.1	0.793	11.3	LOS B	38.8	977.6	0.79	0.65	0.93	31.6

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 101 [Roundabout metered - AM Sensitivity - (+10%) (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout Metering

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	HV %	[Total veh/h]	HV %	v/c	sec		[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	202	0.0	220	0.0	0.844	14.7	LOS B	41.2	1038.8	0.93	0.78	1.17	29.7
8	T1	1232	1.3	1339	1.3	0.844	14.7	LOS B	41.2	1038.8	0.94	0.79	1.18	30.0
18	R2	37	0.0	40	0.0	0.844	14.7	LOS B	41.1	1038.4	0.94	0.79	1.18	29.4
Approach		1471	1.1	1599	1.1	0.844	14.7	LOS B	41.2	1038.8	0.94	0.79	1.18	29.9
East: Chickatawbut Rd														
1	L2	19	0.0	20	0.0	0.802	36.6	LOS E	9.7	242.6	0.99	1.42	2.35	22.8
6	T1	206	0.5	222	0.5	0.802	36.6	LOS E	9.7	242.6	0.99	1.42	2.35	22.8
16	R2	132	0.0	142	0.0	0.802	36.6	LOS E	9.7	242.6	0.99	1.42	2.35	22.5
Approach		357	0.3	384	0.3	0.802	38.6	LOS E	9.7	242.6	0.99	1.42	2.35	22.7
North: Rt 28														
7	L2	65	0.0	69	0.0	0.513	7.6	LOS A	3.3	84.0	0.67	0.61	0.72	33.8
4	T1	585	2.0	622	2.0	0.513	7.6	LOS A	3.3	84.0	0.62	0.55	0.66	34.4
14	R2	30	0.0	32	0.0	0.231	3.4	LOS A	1.1	26.7	0.51	0.42	0.51	34.7
Approach		680	1.7	723	1.7	0.513	6.2	LOS A	3.3	84.0	0.62	0.55	0.66	34.3
West: Chickatawbut Rd														
5	L2	37	0.0	40	0.0	0.260	5.2	LOS A	1.0	25.5	0.60	0.60	0.60	34.4
2	T1	69	0.0	75	0.0	0.260	5.2	LOS A	1.0	25.5	0.60	0.60	0.60	34.3
12	R2	78	0.0	85	0.0	0.260	9.4	LOS A	1.0	25.5	0.60	0.60	0.60	33.5
Approach		184	0.0	200	0.0	0.260	6.5	LOS A	1.0	25.5	0.60	0.60	0.60	34.0
All Vehicles		2692	1.1	2906	1.1	0.844	15.3	LOS C	41.2	1038.8	0.84	0.80	1.16	29.9

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 101 [Roundabout metered - PM Base (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout Metering

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	HV %	[Total veh/h]	HV %	v/c	sec		[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	24	0.0	24	0.0	0.299	3.3	LOS A	1.6	39.9	0.44	0.30	0.44	35.8
8	T1	632	1.8	638	1.8	0.299	3.3	LOS A	1.6	40.0	0.44	0.30	0.44	35.9
18	R2	12	0.0	12	0.0	0.299	3.3	LOS A	1.6	40.0	0.44	0.30	0.44	34.9
Approach		668	1.7	675	1.7	0.299	2.1	LOS A	1.6	40.0	0.44	0.30	0.44	35.9
East: Chickatawbut Rd														
1	L2	244	0.4	254	0.4	0.556	11.1	LOS B	3.4	84.1	0.77	0.84	0.97	31.0
6	T1	67	0.0	70	0.0	0.556	11.1	LOS B	3.4	84.1	0.77	0.84	0.97	30.9
16	R2	71	0.0	74	0.0	0.556	11.1	LOS B	3.4	84.1	0.77	0.84	0.97	30.3
Approach		382	0.3	398	0.3	0.556	9.9	LOS A	3.4	84.1	0.77	0.84	0.97	30.8
North: Rt 28														
7	L2	75	0.0	77	0.0	1.007	45.3	LOS F	57.0	1447.8	0.97	1.81	3.13	21.3
4	T1	1003	2.1	1023	2.1	1.007	35.0	LOS F	57.0	1447.8	0.91	1.42	2.36	24.4
14	R2	8	0.0	8	0.0	0.453	4.4	LOS A	6.8	174.0	0.77	0.64	0.77	33.8
Approach		1086	1.9	1108	1.9	1.007	35.5	LOS E	57.0	1447.8	0.91	1.44	2.40	24.3
West: Chickatawbut Rd														
5	L2	52	0.0	57	0.0	0.955	64.3	LOS F	13.3	335.5	1.00	1.55	2.74	18.1
2	T1	108	0.0	117	0.0	0.955	64.3	LOS F	13.3	335.5	1.00	1.55	2.74	18.1
12	R2	185	2.2	201	2.2	0.955	73.9	LOS F	13.3	335.5	1.00	1.55	2.74	17.9
Approach		345	1.2	375	1.2	0.955	68.7	LOS F	13.3	335.5	1.00	1.55	2.74	18.0
All Vehicles		2481	1.5	2556	1.5	1.007	28.2	LOS D	57.0	1447.8	0.78	1.06	1.71	26.0

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 101 [Roundabout metered - PM Sensitivity (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout Metering

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	HV %	[Total veh/h]	HV %	v/c	sec		[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	24	0.0	24	0.0	0.302	3.4	LOS A	1.7	42.5	0.47	0.32	0.47	35.7
8	T1	632	1.8	638	1.8	0.302	3.4	LOS A	1.7	42.6	0.47	0.32	0.47	35.8
18	R2	12	0.0	12	0.0	0.302	3.5	LOS A	1.7	42.6	0.47	0.32	0.47	34.8
Approach		668	1.7	675	1.7	0.302	2.3	LOS A	1.7	42.6	0.47	0.32	0.47	35.8
East: Chickatawbut Rd														
1	L2	155	0.4	161	0.4	0.397	7.5	LOS A	1.9	48.6	0.70	0.72	0.77	32.5
6	T1	55	0.0	57	0.0	0.397	7.5	LOS A	1.9	48.6	0.70	0.72	0.77	32.5
16	R2	60	0.0	63	0.0	0.397	7.5	LOS A	1.9	48.6	0.70	0.72	0.77	31.8
Approach		270	0.2	281	0.2	0.397	6.7	LOS A	1.9	48.6	0.70	0.72	0.77	32.3
North: Rt 28														
7	L2	75	0.0	77	0.0	0.843	14.2	LOS B	41.9	1063.1	0.99	0.92	1.29	30.2
4	T1	1003	2.1	1023	2.1	0.843	13.1	LOS B	41.9	1063.1	0.88	0.77	1.08	31.7
14	R2	8	0.0	8	0.0	0.380	3.4	LOS A	7.8	198.4	0.65	0.47	0.65	34.2
Approach		1086	1.9	1108	1.9	0.843	13.1	LOS B	41.9	1063.1	0.88	0.78	1.09	31.6
West: Chickatawbut Rd														
5	L2	43	0.0	47	0.0	0.578	19.7	LOS C	3.8	96.1	0.91	1.01	1.23	28.2
2	T1	80	0.0	87	0.0	0.578	19.7	LOS C	3.8	96.1	0.91	1.01	1.23	28.1
12	R2	93	2.2	101	2.2	0.578	27.0	LOS D	3.8	96.1	0.91	1.01	1.23	27.6
Approach		216	0.9	235	0.9	0.578	22.3	LOS C	3.8	96.1	0.91	1.01	1.23	27.9
All Vehicles		2240	1.6	2299	1.6	0.843	10.6	LOS B	41.9	1063.1	0.74	0.66	0.88	32.4

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 101 [Roundabout metered - PM Sensitivity - (-10%) (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout Metering

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	HV %	[Total veh/h]	HV %	v/c	sec		[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	24	0.0	24	0.0	0.298	3.3	LOS A	1.6	41.4	0.45	0.30	0.45	35.7
8	T1	632	1.8	638	1.8	0.298	3.3	LOS A	1.6	41.5	0.45	0.30	0.45	35.9
18	R2	12	0.0	12	0.0	0.298	3.3	LOS A	1.6	41.5	0.45	0.30	0.45	34.9
Approach		668	1.7	675	1.7	0.298	2.2	LOS A	1.6	41.5	0.45	0.30	0.45	35.8
East: Chickatawbut Rd														
1	L2	140	0.4	146	0.4	0.356	6.8	LOS A	1.6	41.3	0.68	0.69	0.72	32.8
6	T1	50	0.0	52	0.0	0.356	6.8	LOS A	1.6	41.3	0.68	0.69	0.72	32.8
16	R2	54	0.0	56	0.0	0.356	6.8	LOS A	1.6	41.3	0.68	0.69	0.72	32.1
Approach		244	0.2	254	0.2	0.356	6.0	LOS A	1.6	41.3	0.68	0.69	0.72	32.6
North: Rt 28														
7	L2	75	0.0	77	0.0	0.824	12.5	LOS B	39.3	997.8	0.96	0.83	1.18	30.9
4	T1	1003	2.1	1023	2.1	0.824	11.8	LOS B	39.3	997.8	0.86	0.70	1.00	32.2
14	R2	8	0.0	8	0.0	0.371	3.2	LOS A	7.7	196.2	0.64	0.44	0.64	34.3
Approach		1086	1.9	1108	1.9	0.824	11.8	LOS B	39.3	997.8	0.86	0.71	1.01	32.1
West: Chickatawbut Rd														
5	L2	39	0.0	42	0.0	0.510	16.5	LOS C	3.2	79.7	0.89	0.96	1.13	29.3
2	T1	72	0.0	78	0.0	0.510	16.5	LOS C	3.2	79.7	0.89	0.96	1.13	29.3
12	R2	84	2.2	91	2.2	0.510	23.6	LOS C	3.2	79.7	0.89	0.96	1.13	28.7
Approach		195	0.9	212	0.9	0.510	19.2	LOS C	3.2	79.7	0.89	0.96	1.13	29.0
All Vehicles		2193	1.6	2249	1.6	0.824	9.4	LOS A	39.3	997.8	0.72	0.61	0.82	32.9

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 101 [Roundabout metered - PM Sensitivity - (+10%) (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout Metering

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	HV %	[Total veh/h]	HV %	v/c	sec		[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	24	0.0	24	0.0	0.307	3.6	LOS A	1.7	43.6	0.48	0.34	0.48	35.6
8	T1	632	1.8	638	1.8	0.307	3.6	LOS A	1.7	43.7	0.48	0.34	0.48	35.7
18	R2	12	0.0	12	0.0	0.307	3.6	LOS A	1.7	43.7	0.49	0.34	0.49	34.7
Approach		668	1.7	675	1.7	0.307	2.4	LOS A	1.7	43.7	0.48	0.34	0.48	35.7
East: Chickatawbut Rd														
1	L2	171	0.4	178	0.4	0.441	8.4	LOS A	2.3	57.2	0.72	0.76	0.83	32.1
6	T1	61	0.0	64	0.0	0.441	8.4	LOS A	2.3	57.2	0.72	0.76	0.83	32.1
16	R2	66	0.0	69	0.0	0.441	8.4	LOS A	2.3	57.2	0.72	0.76	0.83	31.4
Approach		298	0.2	310	0.2	0.441	7.5	LOS A	2.3	57.2	0.72	0.76	0.83	32.0
North: Rt 28														
7	L2	75	0.0	77	0.0	0.866	16.5	LOS C	45.3	1148.4	1.00	1.01	1.43	29.3
4	T1	1003	2.1	1023	2.1	0.866	14.7	LOS B	45.3	1148.4	0.89	0.84	1.18	31.0
14	R2	8	0.0	8	0.0	0.390	3.5	LOS A	7.9	200.9	0.67	0.50	0.67	34.1
Approach		1086	1.9	1108	1.9	0.866	14.8	LOS B	45.3	1148.4	0.90	0.85	1.19	30.9
West: Chickatawbut Rd														
5	L2	47	0.0	51	0.0	0.647	23.8	LOS C	4.6	115.3	0.93	1.06	1.35	26.8
2	T1	88	0.0	96	0.0	0.647	23.8	LOS C	4.6	115.3	0.93	1.06	1.35	26.8
12	R2	102	2.2	111	2.2	0.647	31.4	LOS D	4.6	115.3	0.93	1.06	1.35	26.3
Approach		237	0.9	258	0.9	0.647	26.5	LOS D	4.6	115.3	0.93	1.06	1.35	26.6
All Vehicles		2289	1.5	2351	1.5	0.866	12.1	LOS B	45.3	1148.4	0.76	0.71	0.96	31.7

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 101v [Roundabout - AM Base (Site Folder: General)]

Rt 28/Chickatawbut Rd
Site Category: (None)
Roundabout

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	[HV %]	[Total veh/h]	[HV %]	v/c	sec		[Veh. veh]	Dist] ft				
South: Rt 28														
3	L2	202	0.0	220	0.0	0.691	13.2	LOS B	9.9	248.9	0.69	0.65	0.94	30.3
8	T1	1232	1.3	1339	1.3	0.691	13.2	LOS B	9.9	248.9	0.69	0.65	0.94	30.6
18	R2	37	0.0	40	0.0	0.691	13.2	LOS B	9.8	248.4	0.69	0.65	0.94	30.0
Approach		1471	1.1	1599	1.1	0.691	13.2	LOS B	9.9	248.9	0.69	0.65	0.94	30.5
East: Chickatawbut Rd														
1	L2	21	0.0	23	0.0	1.118	117.8	LOS F	22.7	569.7	1.00	2.36	6.29	12.6
6	T1	205	0.5	220	0.5	1.118	117.9	LOS F	22.7	569.7	1.00	2.36	6.29	12.6
16	R2	144	0.0	155	0.0	1.118	117.8	LOS F	22.7	569.7	1.00	2.36	6.29	12.5
Approach		370	0.3	398	0.3	1.118	117.9	LOS F	22.7	569.7	1.00	2.36	6.29	12.6
North: Rt 28														
7	L2	65	0.0	69	0.0	0.533	10.8	LOS B	4.2	105.4	0.67	0.75	0.94	31.5
4	T1	585	2.0	622	2.0	0.533	10.8	LOS B	4.2	105.4	0.62	0.65	0.81	32.3
14	R2	30	0.0	32	0.0	0.240	6.2	LOS A	1.0	26.0	0.52	0.45	0.52	33.0
Approach		680	1.7	723	1.7	0.533	10.6	LOS B	4.2	105.4	0.62	0.65	0.81	32.2
West: Chickatawbut Rd														
5	L2	45	0.0	49	0.0	0.313	8.4	LOS A	1.3	32.0	0.62	0.62	0.63	32.6
2	T1	85	0.0	92	0.0	0.313	8.4	LOS A	1.3	32.0	0.62	0.62	0.63	32.5
12	R2	91	0.0	99	0.0	0.313	12.7	LOS B	1.3	32.0	0.62	0.62	0.63	31.8
Approach		221	0.0	240	0.0	0.313	10.2	LOS B	1.3	32.0	0.62	0.62	0.63	32.2
All Vehicles		2742	1.0	2960	1.0	1.118	26.4	LOS D	22.7	569.7	0.71	0.88	1.60	26.0

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: J:\21\21055 - MSA Statewide Engineering Design + Review Svrs\21055.15 - Milton Rt 28 at Chickatawbut Rd\Project\SIDRA\Milton - Rt 28 at Chickatawbut Rd 2022-11.sip9

MOVEMENT SUMMARY

▼ Site: 101v [Roundabout - AM Sensitivity (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout

Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn v/c	Aver. Delay sec	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	[HV %]	[Total veh/h]	[HV %]				[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	202	0.0	220	0.0	0.669	12.2	LOS B	6.4	160.5	0.62	0.45	0.66	30.7
8	T1	1232	1.3	1339	1.3	0.669	12.2	LOS B	6.4	160.5	0.62	0.45	0.65	31.0
18	R2	37	0.0	40	0.0	0.669	12.2	LOS B	6.3	159.9	0.62	0.45	0.65	30.4
Approach		1471	1.1	1599	1.1	0.669	12.2	LOS B	6.4	160.5	0.62	0.45	0.65	30.9
East: Chickatawbut Rd														
1	L2	17	0.0	18	0.0	0.969	74.4	LOS F	11.0	276.4	0.99	1.72	3.83	16.7
6	T1	187	0.5	201	0.5	0.969	74.5	LOS F	11.0	276.4	0.99	1.72	3.83	16.7
16	R2	120	0.0	129	0.0	0.969	74.4	LOS F	11.0	276.4	0.99	1.72	3.83	16.5
Approach		324	0.3	348	0.3	0.969	74.4	LOS F	11.0	276.4	0.99	1.72	3.83	16.7
North: Rt 28														
7	L2	65	0.0	69	0.0	0.534	10.8	LOS B	4.2	105.8	0.67	0.75	0.94	31.5
4	T1	585	2.0	622	2.0	0.534	10.7	LOS B	4.2	105.8	0.62	0.66	0.81	32.2
14	R2	30	0.0	32	0.0	0.241	6.2	LOS A	1.0	26.1	0.52	0.46	0.52	33.0
Approach		680	1.7	723	1.7	0.534	10.6	LOS B	4.2	105.8	0.62	0.66	0.81	32.2
West: Chickatawbut Rd														
5	L2	34	0.0	37	0.0	0.238	7.3	LOS A	0.9	23.0	0.59	0.59	0.59	33.1
2	T1	63	0.0	68	0.0	0.238	7.3	LOS A	0.9	23.0	0.59	0.59	0.59	33.0
12	R2	71	0.0	77	0.0	0.238	11.5	LOS B	0.9	23.0	0.59	0.59	0.59	32.3
Approach		168	0.0	183	0.0	0.238	9.1	LOS A	0.9	23.0	0.59	0.59	0.59	32.7
All Vehicles		2643	1.1	2853	1.1	0.969	19.2	LOS C	11.0	276.4	0.66	0.67	1.08	28.4

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

▼ Site: 101v [Roundabout - AM Sensitivity - (-10%) (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	HV %	[Total veh/h]	HV %	v/c	sec		[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	202	0.0	220	0.0	0.663	11.9	LOS B	5.7	143.2	0.60	0.41	0.60	30.8
8	T1	1232	1.3	1339	1.3	0.663	12.0	LOS B	5.7	143.2	0.60	0.41	0.60	31.1
18	R2	37	0.0	40	0.0	0.663	12.0	LOS B	5.6	142.6	0.60	0.41	0.60	30.5
Approach		1471	1.1	1599	1.1	0.663	12.0	LOS B	5.7	143.2	0.60	0.41	0.60	31.0
East: Chickatawbut Rd														
1	L2	15	0.0	16	0.0	0.868	53.8	LOS F	6.8	171.2	0.96	1.41	2.72	19.8
6	T1	168	0.5	181	0.5	0.868	53.9	LOS F	6.8	171.2	0.96	1.41	2.72	19.7
16	R2	108	0.0	116	0.0	0.868	53.8	LOS F	6.8	171.2	0.96	1.41	2.72	19.5
Approach		291	0.3	313	0.3	0.868	53.8	LOS F	6.8	171.2	0.96	1.41	2.72	19.7
North: Rt 28														
7	L2	65	0.0	69	0.0	0.524	10.4	LOS B	4.0	100.7	0.65	0.71	0.89	31.7
4	T1	585	2.0	622	2.0	0.524	10.4	LOS B	4.0	100.7	0.61	0.62	0.77	32.4
14	R2	30	0.0	32	0.0	0.236	6.1	LOS A	1.0	25.6	0.50	0.44	0.50	33.1
Approach		680	1.7	723	1.7	0.524	10.2	LOS B	4.0	100.7	0.61	0.62	0.77	32.4
West: Chickatawbut Rd														
5	L2	31	0.0	34	0.0	0.215	7.0	LOS A	0.8	20.5	0.58	0.58	0.58	33.2
2	T1	57	0.0	62	0.0	0.215	7.0	LOS A	0.8	20.5	0.58	0.58	0.58	33.2
12	R2	64	0.0	70	0.0	0.215	11.1	LOS B	0.8	20.5	0.58	0.58	0.58	32.4
Approach		152	0.0	165	0.0	0.215	8.8	LOS A	0.8	20.5	0.58	0.58	0.58	32.9
All Vehicles		2594	1.1	2800	1.1	0.868	16.0	LOS C	6.8	171.2	0.64	0.59	0.88	29.5

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 101v [Roundabout - AM Sensitivity - (+10%) (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	HV %	[Total veh/h]	HV %	v/c	sec		[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	202	0.0	220	0.0	0.675	12.4	LOS B	7.6	190.3	0.64	0.51	0.74	30.6
8	T1	1232	1.3	1339	1.3	0.675	12.5	LOS B	7.6	190.3	0.64	0.51	0.74	30.9
18	R2	37	0.0	40	0.0	0.675	12.5	LOS B	7.5	189.7	0.64	0.51	0.74	30.3
Approach		1471	1.1	1599	1.1	0.675	12.5	LOS B	7.6	190.3	0.64	0.51	0.74	30.8
East: Chickatawbut Rd														
1	L2	19	0.0	20	0.0	1.071	102.4	LOS F	18.5	463.9	1.00	2.14	5.45	13.9
6	T1	206	0.5	222	0.5	1.071	102.4	LOS F	18.5	463.9	1.00	2.14	5.45	13.8
16	R2	132	0.0	142	0.0	1.071	102.4	LOS F	18.5	463.9	1.00	2.14	5.45	13.7
Approach		357	0.3	384	0.3	1.071	102.4	LOS F	18.5	463.9	1.00	2.14	5.45	13.8
North: Rt 28														
7	L2	65	0.0	69	0.0	0.538	10.9	LOS B	4.2	107.2	0.68	0.76	0.96	31.5
4	T1	585	2.0	622	2.0	0.538	10.9	LOS B	4.2	107.2	0.63	0.67	0.82	32.2
14	R2	30	0.0	32	0.0	0.242	6.3	LOS A	1.0	26.2	0.52	0.46	0.52	33.0
Approach		680	1.7	723	1.7	0.538	10.7	LOS B	4.2	107.2	0.63	0.67	0.82	32.2
West: Chickatawbut Rd														
5	L2	37	0.0	40	0.0	0.261	7.6	LOS A	1.0	25.6	0.60	0.60	0.60	32.9
2	T1	69	0.0	75	0.0	0.261	7.6	LOS A	1.0	25.6	0.60	0.60	0.60	32.9
12	R2	78	0.0	85	0.0	0.261	11.9	LOS B	1.0	25.6	0.60	0.60	0.60	32.2
Approach		184	0.0	200	0.0	0.261	9.4	LOS A	1.0	25.6	0.60	0.60	0.60	32.6
All Vehicles		2692	1.1	2906	1.1	1.071	23.7	LOS C	18.5	463.9	0.68	0.77	1.37	26.8

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 101v [Roundabout - PM Base (Site Folder: General)]

Rt 28/Chickatawbut Rd
Site Category: (None)
Roundabout

Vehicle Movement Performance													
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE	Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	[HV %]	[Total veh/h]	[HV %]	v/c	sec	[Veh. veh]	Dist] ft				
South: Rt 28													
3	L2	24	0.0	24	0.0	0.316	6.3	LOS A	1.8	45.2	0.47	0.33	0.47
8	T1	648	1.8	655	1.8	0.316	6.4	LOS A	1.8	45.2	0.47	0.33	0.47
18	R2	12	0.0	12	0.0	0.316	6.3	LOS A	1.8	45.2	0.47	0.33	0.47
Approach		684	1.7	691	1.7	0.316	6.4	LOS A	1.8	45.2	0.47	0.33	0.47
East: Chickatawbut Rd													
1	L2	250	0.4	260	0.4	0.586	15.2	LOS C	4.4	109.9	0.79	0.96	1.31
6	T1	68	0.0	71	0.0	0.586	15.1	LOS C	4.4	109.9	0.79	0.96	1.31
16	R2	73	0.0	76	0.0	0.586	15.1	LOS C	4.4	109.9	0.79	0.96	1.31
Approach		391	0.3	407	0.3	0.586	15.1	LOS C	4.4	109.9	0.79	0.96	1.31
North: Rt 28													
7	L2	77	0.0	79	0.0	0.833	23.7	LOS C	19.9	506.1	1.00	1.43	2.18
4	T1	1028	2.1	1049	2.1	0.833	21.6	LOS C	19.9	506.1	0.87	1.13	1.66
14	R2	8	0.0	8	0.0	0.375	7.9	LOS A	2.1	54.0	0.61	0.53	0.61
Approach		1113	1.9	1136	1.9	0.833	21.7	LOS C	19.9	506.1	0.88	1.15	1.69
West: Chickatawbut Rd													
5	L2	54	0.0	59	0.0	1.283	185.4	LOS F	35.5	894.8	1.00	2.75	7.55
2	T1	110	0.0	120	0.0	1.283	185.4	LOS F	35.5	894.8	1.00	2.75	7.55
12	R2	189	2.2	205	2.2	1.283	194.9	LOS F	35.5	894.8	1.00	2.75	7.55
Approach		353	1.2	384	1.2	1.283	190.5	LOS F	35.5	894.8	1.00	2.75	7.55
All Vehicles		2541	1.5	2618	1.5	1.283	41.4	LOS E	35.5	894.8	0.78	1.14	2.17

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: J:\21\21055 - MSA Statewide Engineering Design + Review Svrs\21055.15 - Milton Rt 28 at Chickatawbut Rd\Project\SIDRA\Milton - Rt 28 at Chickatawbut Rd 2022-11.sip9

MOVEMENT SUMMARY

Site: 101v [Roundabout - PM Sensitivity (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout

Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn v/c	Aver. Delay sec	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	[HV %]	[Total veh/h]	[HV %]				[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	24	0.0	24	0.0	0.302	6.0	LOS A	1.7	42.7	0.43	0.28	0.43	34.0
8	T1	648	1.8	655	1.8	0.302	6.0	LOS A	1.7	42.7	0.43	0.28	0.43	34.1
18	R2	12	0.0	12	0.0	0.302	6.0	LOS A	1.7	42.7	0.43	0.28	0.43	33.2
Approach		684	1.7	691	1.7	0.302	6.0	LOS A	1.7	42.7	0.43	0.28	0.43	34.0
East: Chickatawbut Rd														
1	L2	153	0.4	159	0.4	0.393	10.3	LOS B	2.0	50.9	0.70	0.75	0.86	30.9
6	T1	54	0.0	56	0.0	0.393	10.3	LOS B	2.0	50.9	0.70	0.75	0.86	30.9
16	R2	59	0.0	61	0.0	0.393	10.3	LOS B	2.0	50.9	0.70	0.75	0.86	30.2
Approach		266	0.2	277	0.2	0.393	10.3	LOS B	2.0	50.9	0.70	0.75	0.86	30.7
North: Rt 28														
7	L2	77	0.0	79	0.0	0.728	15.3	LOS C	13.4	340.4	0.83	0.89	1.29	29.7
4	T1	1028	2.1	1049	2.1	0.728	15.0	LOS B	13.4	340.4	0.72	0.72	1.03	31.0
14	R2	8	0.0	8	0.0	0.328	6.5	LOS A	1.9	47.1	0.50	0.36	0.50	32.9
Approach		1113	1.9	1136	1.9	0.728	14.9	LOS B	13.4	340.4	0.73	0.73	1.05	30.9
West: Chickatawbut Rd														
5	L2	40	0.0	43	0.0	0.586	26.6	LOS D	3.2	79.5	0.88	1.04	1.48	25.7
2	T1	63	0.0	68	0.0	0.586	26.6	LOS D	3.2	79.5	0.88	1.04	1.48	25.7
12	R2	87	2.2	95	2.2	0.586	34.3	LOS D	3.2	79.5	0.88	1.04	1.48	25.2
Approach		190	1.0	207	1.0	0.586	30.2	LOS D	3.2	79.5	0.88	1.04	1.48	25.5
All Vehicles		2253	1.6	2310	1.6	0.728	13.1	LOS B	13.4	340.4	0.65	0.63	0.88	31.1

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

▼ Site: 101v [Roundabout - PM Sensitivity - (+10%) (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout

Vehicle Movement Performance														
Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn	Aver. Delay	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	HV %	[Total veh/h]	HV %	v/c	sec		[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	24	0.0	24	0.0	0.306	6.1	LOS A	1.7	43.5	0.44	0.30	0.44	33.9
8	T1	648	1.8	655	1.8	0.306	6.1	LOS A	1.7	43.5	0.44	0.30	0.44	34.0
18	R2	12	0.0	12	0.0	0.306	6.1	LOS A	1.7	43.5	0.44	0.30	0.44	33.1
Approach		684	1.7	691	1.7	0.306	6.1	LOS A	1.7	43.5	0.44	0.30	0.44	34.0
East: Chickatawbut Rd														
1	L2	168	0.4	175	0.4	0.434	11.2	LOS B	2.4	61.0	0.72	0.79	0.95	30.5
6	T1	59	0.0	61	0.0	0.434	11.2	LOS B	2.4	61.0	0.72	0.79	0.95	30.5
16	R2	65	0.0	68	0.0	0.434	11.2	LOS B	2.4	61.0	0.72	0.79	0.95	29.9
Approach		292	0.2	304	0.2	0.434	11.2	LOS B	2.4	61.0	0.72	0.79	0.95	30.4
North: Rt 28														
7	L2	77	0.0	79	0.0	0.745	16.4	LOS C	14.6	371.6	0.87	0.99	1.45	29.3
4	T1	1028	2.1	1049	2.1	0.745	15.8	LOS C	14.6	371.6	0.76	0.80	1.14	30.6
14	R2	8	0.0	8	0.0	0.336	6.8	LOS A	1.9	48.3	0.52	0.39	0.52	32.8
Approach		1113	1.9	1136	1.9	0.745	15.8	LOS C	14.6	371.6	0.76	0.81	1.16	30.6
West: Chickatawbut Rd														
5	L2	44	0.0	48	0.0	0.664	32.3	LOS D	3.9	98.7	0.90	1.12	1.69	24.1
2	T1	69	0.0	75	0.0	0.664	32.3	LOS D	3.9	98.7	0.90	1.12	1.69	24.1
12	R2	96	2.2	104	2.2	0.664	40.3	LOS E	3.9	98.7	0.90	1.12	1.69	23.7
Approach		209	1.0	227	1.0	0.664	36.0	LOS E	3.9	98.7	0.90	1.12	1.69	23.9
All Vehicles		2298	1.6	2358	1.6	0.745	14.3	LOS B	14.6	371.6	0.68	0.69	0.97	30.6

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).

Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

▼ Site: 101v [Roundabout - PM Sensitivity - (-10%) (Site Folder: General)]

Rt 28/Chickatawbut Rd

Site Category: (None)

Roundabout

Mov ID	Turn	INPUT VOLUMES		DEMAND FLOWS		Deg. Satn v/c	Aver. Delay sec	Level of Service	95% BACK OF QUEUE		Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver. Speed mph
		[Total veh/h]	[HV %]	[Total veh/h]	[HV %]				[Veh. veh]	Dist ft				
South: Rt 28														
3	L2	24	0.0	24	0.0	0.298	5.9	LOS A	1.7	42.0	0.41	0.27	0.41	34.0
8	T1	648	1.8	655	1.8	0.298	5.9	LOS A	1.7	42.0	0.41	0.27	0.41	34.1
18	R2	12	0.0	12	0.0	0.298	5.9	LOS A	1.7	41.9	0.41	0.27	0.41	33.2
Approach		684	1.7	691	1.7	0.298	5.9	LOS A	1.7	42.0	0.41	0.27	0.41	34.1
East: Chickatawbut Rd														
1	L2	138	0.4	144	0.4	0.352	9.6	LOS A	1.7	41.8	0.68	0.70	0.76	31.2
6	T1	49	0.0	51	0.0	0.352	9.5	LOS A	1.7	41.8	0.68	0.70	0.76	31.2
16	R2	53	0.0	55	0.0	0.352	9.5	LOS A	1.7	41.8	0.68	0.70	0.76	30.6
Approach		240	0.2	250	0.2	0.352	9.6	LOS A	1.7	41.8	0.68	0.70	0.76	31.1
North: Rt 28														
7	L2	77	0.0	79	0.0	0.711	14.4	LOS B	12.0	304.4	0.79	0.78	1.13	30.1
4	T1	1028	2.1	1049	2.1	0.711	14.2	LOS B	12.0	304.4	0.69	0.63	0.92	31.3
14	R2	8	0.0	8	0.0	0.320	6.3	LOS A	1.8	46.0	0.47	0.33	0.47	33.0
Approach		1113	1.9	1136	1.9	0.711	14.1	LOS B	12.0	304.4	0.69	0.64	0.93	31.2
West: Chickatawbut Rd														
5	L2	36	0.0	39	0.0	0.512	22.4	LOS C	2.6	64.4	0.86	0.98	1.32	27.0
2	T1	57	0.0	62	0.0	0.512	22.4	LOS C	2.6	64.4	0.86	0.98	1.32	27.0
12	R2	78	2.2	85	2.2	0.512	29.9	LOS D	2.6	64.4	0.86	0.98	1.32	26.5
Approach		171	1.0	186	1.0	0.512	25.8	LOS D	2.6	64.4	0.86	0.98	1.32	26.8
All Vehicles		2208	1.6	2262	1.6	0.711	12.1	LOS B	12.0	304.4	0.62	0.56	0.78	31.6

Site Level of Service (LOS) Method: Delay & v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.

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Roundabout Capacity Model: US HCM 6.

Delay Model: HCM Delay Formula (Geometric Delay is not included).

Queue Model: HCM Queue Formula.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.



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